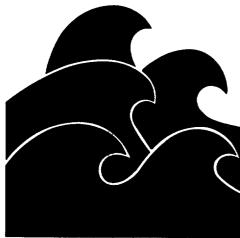
W1125.7 R299 No.224

Report 224

Occurrence, Quantity, and Quality of Ground Water in Taylor County, Texas



TEXAS DEPARTMENT OF WATER RESOURCES

October 1978

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for REPORT 224

OCCURRENCE, QUANTITY, AND QUALITY OF GROUND WATER IN TAYLOR COUNTY, TEXAS

(Published by the Texas Department of Water Resources October 1978)

The following table replaces the one on page 13.

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Table 1.--Geologic Units and Their Water-Bearing Properties in Taylor County

SYSTEM	SERIES	GROUP	FORMATION	MEMBER	APPROXIMATE MAXIMUM THICKNESS (ft)	LITHOLOGIC CHARACTER	WATER-BEARING CHARACTERISTICS
	Recent		Allavium		30	Cross bedded sandstones, gravel, fine silts, and sancy clays occurring in and bordsring most of the stream channels in the county.	Yields fresh to moderately seline water in small to moderate quantities to wells mostly in the eastern two thirds of the county.
		- Unconformity	Undivided surf	ficial deposits	10	Residual so is of caliche and lag gravels capping many of the low-lying hills in the northern half of the county.	Known to yield small quantities of fresh to slightly saline water to one well and one spring in the northern half of the county.
Quaternary	Pleistocene		Seymour		40	Contains fine grained, white, light tan to red sands and sits, redish-orange and gray clay; and white to buff nodules of catiche (usually near surface). Lower portion of the formation is coarse gravels or conglomerates containing well rounded pebbles of ouartz, quartite, ligneous crystalline rocks, bone fragments, patrilled wood, scattred water worn Cretaceous fossis, and cobbles and pebbles of fourscone	Known to vield small quantities of water to three wells along the county line north of Merkel in the northwest part of the county. Water in one well was fresh.
			Edwards Limestone			Gray to near white, dense to fine crystalline, thin to thick bedded limestone with thin irregular layers and nodules of dark bluish-gray chert.	Yields fresh water in small quantities to scattered wells and springs in the southern part of the county.
		Fredericksburg	Comanche Peak Limestone		100	Gray, thin to rregular, wavy bedded, fossiliterous limestone with thin interbedded clay.	
Cretaceous	Comanche		Walnut			Marly, laminated, light gray to yellowish clay: some thin semi-crystalline limestone lenses locally.	
		Trinity	Antiers		200	Lower and upper parts chiefly stand, middle part manniy clay. Sand is crean to near white, fine to medium grained, incorrelative to well parted, warthers built to locally varigated, some cross hedding, argillacteos in the upper part, locally conglommarie in the lower part. Middle part Chiefly red to aint, buryle, locally caston green clay, sity, with occasional bade of hard calcarecos sits tone. Conglomerate in lower part made up of chert and surfact pebbles.	Vields fresh water in small quantities to wells and springs in the southern part of the county.
		Passe River	San Angelo		200	Cross bacded sandstone, greenish grav, usvaly well consolidated, medium grained, sub-angular to well condided near top of unit: lower portion is clay bells, sandstone as labore interbeddeff with cherty conglomerates, gypsum nodules, sreaks of "satin spar" gypsum, and red and green shales. Weathers dark red.	Yields fresh to moderately saline water in avail to moderate quantities to wells along the extreme western edges of the county.
			Choza	Merkei Dolomite	5	The gray Merical dolomite, at or near the top of this formation, is near believed to be present bouther of the second second to the 20 and about 1.5 miles as to firent. The remainder of the formation consists of semi persuent bads of gray dolomite and anhydrite intergoread in red shales and, locally, thin goorly developed sandstone lenses.	Vields freeh to moderately seline water in small to moderate quantities to wells in the western part of the county.
Permian	Leonard	Clear Fork	Vale	Builwagon Dolomite	10 550	Upper portion of the formation is comprised of many thin back of gray dolomits and aniyotric instabeddad with some clay, but manily red shales. Losver portion of unit is dominately red shale with thin stringers of odomite and a few thin lenticular shaley sandstones. This lower red shale with this of the west.	Yields fresh to moderately saline water in small quantities to a few wells in the eastern half of the county.
			Arroya	Standpipe Limestone Kirby Lake Limestone Lytle Limestone Rainy Limestone	250	White, cream colored, bull and brown, thin bedded and poorly developed investores, dolomites, and maris interbedded with tock haley and do nes. Antydrin is present, tocally, near the base of the tormation in the Lytle and Rainy Limestone Members.	Vields fresh to slightly saline water in small quantities to a few scattered wells in the eastern part of the county.
		Wichita	Lueders		80	Thin bedilet, gray to buff, tossilferous limitscone interbedded with argificecous limitscone and gray to greenst gray shales. Unit grades into dolomite westward in the subsurface.	Yields slightly to moderately seline water in small quantities to a few scattered wells in the eastern part of the county.

Yield of Wells: Small, less than 100 gpm (galions per minute); moderate, 100-1,000 gpm, large, more than 1,000 gpm.



Aerial View of Abilene, Looking Southwest. Courtesy of the Abilene Reporter News.



TEXAS DEPARTMENT OF WATER RESOURCES

REPORT 224

OCCURRENCE, QUANTITY, AND QUALITY OF GROUND WATER IN TAYLOR COUNTY, TEXAS

Bу

Howard D. Taylor, Geologist Texas Department of Water Resources

TEXAS DEPARTMENT OF WATER RESOURCES

Harvey Davis, Executive Director

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FOREWORD

> Effective September 1, 1977, Texas three water resources agencies, the Texas Water Rights Commission, the Texas Water Development Board, and the Texas Water Quality Board, were consolidated to form the Texas Department of Water Resources. A number of publications prepared under the auspices of the predecessor agencies are being published by the TDWR. To effect as little delay as possible in production of these publications, references to these predecessor agencies will not be altered except on their covers and title pages.

Lancy Mavis

Harvey Davis Executive Director

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OCCURENCE, QUANTITY, AND QUALITY OF

GROUND WATER IN

TAYLOR COUNTY, TEXAS

ABSTRACT

Taylor County covers an area of 913 square miles in west-central Texas. The 1970 population was 97,853, most cf which was concentrated in the county seat of Abilene. The climate is warm and semi-arid to subhumid, and the average annual rainfall is about 25 inches. The northern two-thirds of the county is drained by the Brazos River drainage system and the southern one-third by the Colorado River system. The economy of the county is derived from three main sources: manufacturing; mineral extractions, which include surface mining of stone, gravel, and clay as well as oil and gas production; and agriculture.

The surface of Taylor County is comprised of geological formations of the Permian, Cretaceous, and Quaternary Systems. The gently west-northwestward dipping Permian rocks are exposed in narrow, successively younger belts from east to west across the county. Cretaceous sedimentary units, which dip almost imperceptably to the southeast, form northward facing, steep-walled mesas and buttes across a large part of the southern one-half of the county. Unconsolidated sands and gravels of the Quaternary System are found as alluvium and terrace deposits along and between the major drainage tributaries. These are concentrated mostly in the eastern one-half of the county.

Significant amounts of fresh to moderately saline ground water occur in aquifers of the Permian, Cretaceous, and Quaternary Systems. The principal aquifers are: the Choza Formation, particularly in the area from the Taylor-Jones county line just north of Merkel southward to the Cretaceous hills west of the community of View, and the San Angelo Formation, both of Permian age; the Antlers Formation of Cretaceous age; and the alluvium of Quaternary age, primarily that along Jim Ned and East Jim Ned Creek in the Tuscola area, and that along Elm Creek from Lake Abilene northward through Abilene. Minor amounts of fresh to moderately saline ground water are also known to occur in the Lueders, Arroyo, and Vale Formations of the Permian age; the Fredericksburg Group of Cretaceous age; and the Seymour Formation of Quaternary age.

The ground water in Taylor County is used for irrigation, industrial, public supply, domestic, and livestock purposes. The alluvium yields water that is used for irrigation along Jim Ned and Elm Creeks; for public supply in the communities of Tuscola, Buffalo Gap, and Ovalo; for industrial purposes at a gas plant west of Tuscola; and for domestic and livestock supplies in these and other areas scattered across the county. Water from the Antlers Formation is used almost exclusively for livestock and domestic purposes, except in one local area along Elm Creek west of U.S. Highway 277 where a limited amount has been used for irrigation. Water from the Choza Formation is used mostly for irrigation and domestic purposes in the Merkel area and, to a lesser extent, for livestock consumption in this and other areas along the outcrop. Ground water from the Choza and that from the Vale Formation is used at a small mining operation about 7 miles southeast of Merkel. Prior to 1955, ground water from the Choza, and probably the Bullwagon Dolomite Member of the Vale Formation, was used for municipal supply for the town of Merkel. Water from the San Angelo Formation is used primarily for domestic and livestock purposes; however, 16 wells were found in use at a commercial feedlot northeast of Trent. The use of water from all other water-bearing units is principally for domestic and livestock purposes.

The chemical quality of the ground water varies widely. In general, the water from all water-bearing units is very hard. Waters in the Cretaceous rocks are the least mineralized of any in the county. Chemical concentrations in the waters from all the water-bearing units indicate that natural alteration, to one degree or another, has occurred. In some individual wells with high nitrate concentrations, the probable sources for organic contamination, such as nearby barnyards, stock pens, or septic tanks, were apparent. In other wells with equally high nitrate concentrations, the cause or causes could not be readily determined. About 65 percent of the alluvium ground-water samples in the Tuscola area contained nitrate concentrations ranging from 47 to 326 mg/l. Sewage disposal in Tuscola is by septic tanks, which may account for some of the nitrate. There is slight evidence from five wells inventoried in previous years that, historically, nitrate concentrations have been higher in this area than others. High concentrations of sodium and chloride in ground water are fairly common over the county and, along with small scattered vegetative-kill areas, may be evidence of ground-water contamination by oil-field brines.

Reported information from a few "old timers" and some historical data indicate that, in general, there has been a long-term net rise in water levels, but the data are insufficient to say just how much in any area.

OCCURRENCE, QUANTITY, AND QUALITY OF

GROUND WATER IN

TAYLOR COUNTY, TEXAS

INTRODUCTION

Location and Extent of the Study Area

Taylor County is located in west-central Texas between 99° 38' and 100° 09' west longitude and 32° 05' and 32° 31' north latitude. It is bounded on the north by Jones County, on the east and west by Callahan and Nolan Counties, respectively, and on the south by Runnels and Coleman Counties (Figure 1). The county seat is Abilene which is in the northeast corner of the county along Interstate Highway 20. The county is comprised of approximately 913 square miles.

Purpose and Scope of the Investigation

Generally, the purpose of the study, conducted from September 1, 1969 to September 1, 1971, was to determine the occurrence, quantity, and quality of the ground-water resources of the county. Emphasis was placed on determining the sources of water suitable for domestic, livestock, public supply, industrial, and irrigational uses. Areas and possible sources of present or potential ground-water contamination were determined.

The general scope of this study included the collection, compilation, and analysis of data pertaining to the distribution and quality of ground water in Taylor County.

Methods of Investigation

The following methods were used in conducting this study:

An inventory was compiled of all industrial, irrigation, and public supply wells, as well as all springs and selected domestic and stock wells (Table 5). Water levels in the wells were measured where possible.

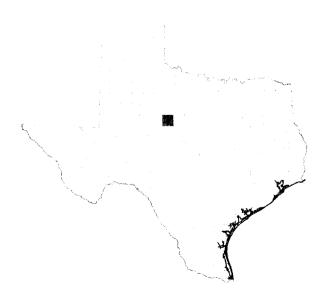


Figure 1.-Location of Taylor County

Available well data were gathered including well depths and construction, date drilled, driller, water yielding zones, and water quantities. Surface elevations of inventoried wells and springs were determined from topographic maps and electric logs.

Water samples were collected from all springs and selected wells for chemical analysis.

Surface and subsurface geologic data were collected and compiled with emphasis placed on their relationship to ground water.

Additional data were collected and compiled on ground-water pumpage, aquifer characteristics, apparent and potential contamination, oil-field brine analysis and disposal, climate, and areas of recharge and discharge.

Previous Investigations

Several general geological reports that include Taylor County have been published prior to this investigation. They are cited in the selected references.

H. A. Smith (1940) obtained data on 126 wells, springs, and oil tests, 105 test holes, and 15 earthen tanks in the county.

The U.S. Geological Survey in cooperation with the Texas Water Commission conducted a reconnaissance investigation of the ground-water resources of the Brazos River basin (Cronin and others, 1963); and the Texas Water Development Board in cooperation with the U.S. Geological Survey conducted a reconnaissance investigation of ground-water resources of the Colorado River basin (Mount and others, 1967).

Well-Numbering System

The system used in numbering the wells and springs in this report was developed and is used statewide by the Texas Water Development Board. It was designed to identify each well or spring and also to designate its geographical location within the State.

The well number consists of a two-letter county prefix followed by a seven-digit number. The numbers are derived from the system of division and subdivision of the State into quadrangles of degrees and minutes of latitude and longitude (Figure 2). The largest division, a one-degree quadrangle, is subdivided into sixty-four 7 1/2-minute quadrangles which are further subdivided into nine 2 1/2-minute quadrangles. Each quadrangle has an assigned number for identification. The first two digits in the well number identify the one-degree quadrangle, the third and fourth digits the 7 1/2-minute quadrangle, and the fifth digit the 2 1/2-minute quadrangle. The sixth and seventh digits identify the individual well or spring within the 2 1/2-minute quadrangle.

The two-letter prefix for Taylor County is XW, and the county falls within the one-degree quadrangles numbered 29 and 30.

Data are included in this report for a few wells in bordering counties. The two-letter prefix for Callahan County is BX; for Jones County, PY; Nolan County, UA; and Runnels County, WP.

Acknowledgements

Grateful acknowledgement is extended to the many landowners, farmers, water-well drillers, oil operators, and city and county officials who aided in the collection of data for this report by allowing access to files and various information and by granting permission to test water wells. Appreciation is also expressed to the Taylor Electric Co-Op, Inc., the State Department of Highways and Public Transportation, and the Soil Conservation Service of the U.S. Department of Agriculture. Particular thanks are given Mr. K. C. Roberson, Agriculture Stabilization and Conservation County Committee of the U.S. Department of Agriculture, for time and information given concerning water conditions in the county.

GEOGRAPHY

Topography and Drainage

Taylor County lies along the border between the Central Lowland physiographic province to the north and the Great Plains province to the south and west. In the southern part of the county is a moderately high plateau area with steep northward facing walls and rolling hills to the south. This plateau rises above an otherwise gently rolling to near-level surface in the remainder of the county. The surface elevation varies from near 1,600 to just under 2,500 feet for a relief of approximately 850 feet.

Farming is dominant in the northern one-half and extreme southern parts of the county where the topography is favorable. In the ranch country of the plateau area, vegetation consists mainly of grasses and scattered to locally heavy cedar tree coverage.

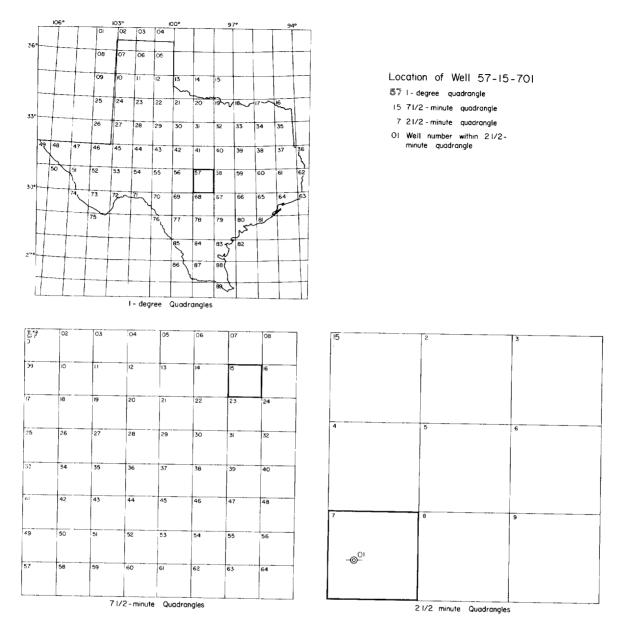


Figure 2.-Well-Numbering System

About the northern two-thirds of Taylor County is drained to the north and east by several minor tributaries of the Brazos River drainage system. The more important ones are Mulberry Creek, Little Elm Creek, Elm Creek, Cedar Creek, and Lytle Creek. The southern one-third of the county is drained by minor tributaries of the Colorado River drainage system. Jim Ned Creek is the most important of these (Figure 5). The physiographic feature which separates the two drainage systems is called the Callahan Divide.

There are several small reservoirs located along the drainage tributaries. Three of these are probably the

most important from a standpoint of size and use. Kirby Lake is located within the southern extension of the city limits of Abilene, along the east side of U.S. Highway 83-84. When full it impounds about 7,600 acre-feet of water. The lake is a source of supply for Abilene. Lake Abilene is located along the north side of Farm Road 89 approximately 20 miles south-southwest of Abilene. At full capacity it impounds about 7,900 acre-feet of water, and it is also a source of supply for Abilene. Lytle Lake is located in the southeastern part of Abilene about one-quarter mile south of State Highway 36. This lake holds about 1,200 acre-feet at full capacity.

Climate

Generally, the climate of Taylor County is warm and semi-arid to subhumid (Figure 3). The mean annual precipitation at Abilene is 24.32 inches over the period 1886-1970 (Figure 4). During the same time interval, the maximum official annual precipitation was 48.77 inches recorded in 1941 while the minimum was 9.78 inches in 1956 (Figure 4). The maximum average monthly precipitation of slightly over 4 inches occurs in May and the minimum of slightly under 1 inch in January (Figure 3). The highest officially recorded precipitation for one month was 10.88 inches in October 1941.

The average annual temperature is near 65° F, with high average monthly temperatures being in July and August and the minimum average being in January (Figure 3). Average monthly gross and net lake-surface evaporation amounts for the Taylor County area are shown in Figure 3. The measured monthly precipitation during the period of this investigation is shown in Figure 15.

History, Population, and Economy

Taylor County was created in 1858 from Bexar and Travis Counties. It was organized with the present boundaries in 1878. It is generally accepted that Taylor County was named after Edward Taylor, one of three brothers who were defenders of the Alamo. The first county seat was Buffalo Gap. However, with the completion of the Texas and Pacific railroad through the county in 1882, the present city of Abilene was "born" and the county seat was moved there from Buffalo Gap in 1882. After the coming of the railroad, the rate at which settling in the county was taking place increased and a transition from free range stock raising to crop production and stock raising on fenced lands began.

The population of the county has grown from only a few people in the mid-1800's to slightly under 100,000 in 1970. Nearly 90 percent of the county's residents are concentrated in the city of Abilene and Dyess Air Force Base. Approximately 2 percent live in the small towns of Lawn, Merkel, Trent, and Tuscola with the remaining 8 percent classified as rural.

Taylor County is served by four railroads, the Fort Worth and Denver, the Texas and Pacific, the Santa Fe, and the Abilene Southern. All are freight carriers only. There are five motor freight carriers and one air express carrier operating in the county. Public transportation is furnished by one airline and six bus lines. A network of one interstate, three federal, two state, and numerous other all-weather roads is found in the county.

In 1970 there was in excess of \$276 million on deposit in banks and savings and loan institutions in Taylor County.

The basic economy is derived from three main sources. These are agriculture, extraction of minerals, and manufacturing. Total 1970 income from these sources was slightly in excess of \$92 million. Agriculture income in 1970 was approximately 23 percent of the total. About 70 percent of the agricultural income came from ranching, principally the raising of cattle and sheep. Crop farming, primarily cotton and grain sorghums and to a lesser extent wheat, peanuts, and hay, produced the remaining 30 percent of the agricultural income.

The extraction of minerals in 1970 amounted to about 32 percent of the total basic income. The production of oil and gas plus the associated refining industry accounted for almost 62 percent of this income, while the mining of stone, sand, gravel, and clay made up the remainder.

Manufacturing income for 1970 was 45 percent of the total basic income. Apparel, aircraft components, appliances, musical instruments, watches, hardware, and food products were the main items produced.

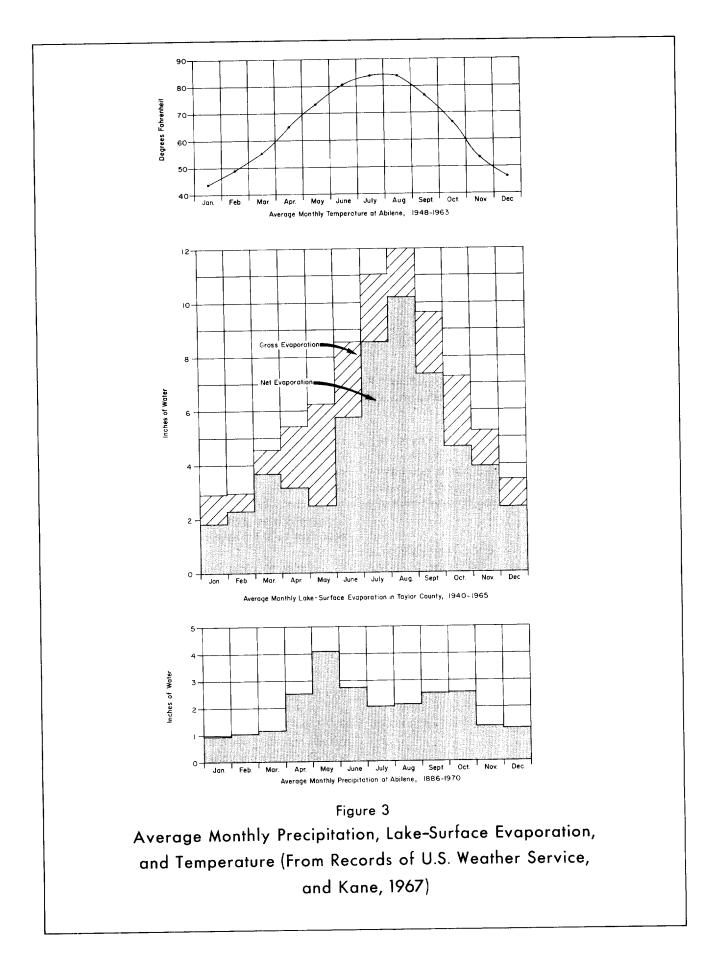
A United States Air Force base, a State school for mental retardation, a United States Post Office sectional mail center, and a district office of the State Department of Highways and Public Transportation, all located in or adjacent to Abilene, with combined annual payrolls of over \$50 million also contribute to the general economy of the county.

GENERAL GEOLOGY

Geologic History

In ascending order, rocks of the Precambrian, Cambrian, Ordovician, Mississippian, and Pennsylvanian Systems are present in the subsurface in Taylor County; sediments of the Permian, Cretaceous, and Quaternary are exposed at the surface (Figures 26, 27, and 28).

Available data suggest that deposition of late Cambrian through Mississippian sediments occurred in



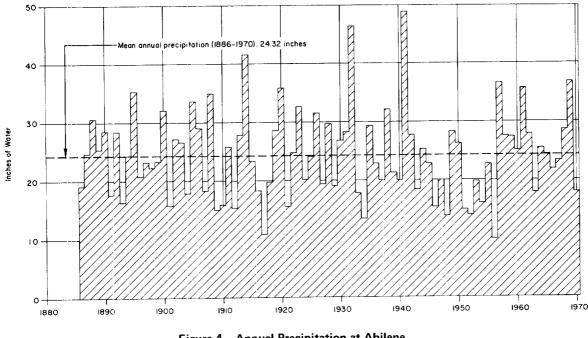


Figure 4.—Annual Precipitation at Abilene (From records of U.S. Weather Service)

broad, relatively shallow seas in this area. Absence of some Cambrian and Ordovician, all Silurian and Devonian rocks, and some Mississippian beds, due either to non-deposition or removal by erosion, is ample evidence of the repeated advance and retreat of the seas during this vast time period.

By late Mississippian or early Pennsylvanian, epeirogenic movement had begun. The nature of early Pennsylvanian deposits is indicitive of shifting environmental conditions and apparently continuous disposition. Evidence points to sea-level changes and subsequent widespread erosion toward the end of early Pennsylvanian time. A general subsidence began at this time and continued, with some interruptions, through the Permian. Evidence of this is the thick sequences of Middle and Upper Pennsylvanian and Permian deposits found in the Taylor County area. A westward recession of the seas occurred in this area toward the end of the Permian.

There are no Triassic or Jurassic deposits in Taylor County; however, structural and stratigraphic evidence indicates that land tilting and drainage changed by late Jurassic time from a previously westerly or northwesterly direction to a southerly or southeasterly direction. Regional tilt and drainage in this area has remained in this direction since that time.

The Lower Cretaceous sea advanced from the southeast across a somewhat unevenly eroded Permian

surface in Taylor County. The Antlers Formation, which is the marginal or shoreward facies of the Trinity Group, was laid down by this sea. As the sea transgressed farther upon the land, the offshore, or seaward, sediments of the Fredericksburg Group were deposited. Although late Cretaceous seas probably covered this area, the rocks deposited by them have since been removed by erosion.

Cenezoic rocks through Pliocene time are not present in this area. However, Van Siclen (1957, p. 56-57) states that the area just to the north was eroded to a near-flat plain sloping gently eastward prior to Pleistocene time with removal of all sediments younger than Permian.

Gravel deposits of probable Pleistocene age form a thin mantle covering scattered parts of the northern half of Taylor County (Figure 5). These deposits, some as lag gravel and some with a calcareous cement, are believed to have been laid down as a continuous sheet across the area. They were controlled by terrestrial alluviation and erosion caused by repeated climatic changes associated with the advance and retreat of the great glaciers to the north during this period of time. Much of these sediments have since been removed from the area by stream erosion so that today only isolated remnants of the once near-continuous sheet are found capping the low gently rolling hills.

Recent alluvial deposits are found along many of the main drainage tributaries in Taylor County,

particularly in the eastern one-half of the county. Much of these sediments was derived from Cretaceous rocks along the Callahan Divide (Figure 5). Also, some of the material of the alluvium undoubtedly was derived from the older Pleistocene gravels and from dissected beds of Permian age.

Stratigraphy of the Water-Bearing Formations

Pre-Permian Systems

In the Taylor County area, rocks of Precambrian age are composed primarily of granite, and to a lesser magn tude of schist and gneiss. Cambrian sediments contain mostly dolomitic limestone with some sandstone. Deposits of the Ordovician and Mississippian consist mainly of dolomite, dolomitic limestone, and limestone, with some chert and shale. The rocks of the Mississippian System are very thin compared to the other systems. The Pennsylvanian contains sands, limestones, and thick sequences of shales. Locally, these limestones are quite thick due to reefing (Figure 27).

In Taylor County, all water in rocks from the Cambrian to the Upper Permian (Lueders Formation), so far as known, contain only brine (over 35,000 parts per million total dissolved solids).

Permian System

Permian sediments of the Lueders, Arroyo, Vale, Choza, and San Angelo Formations, in ascending order, occur at the surface in Taylor County. These rocks attain a total thickness of about 1,600 feet and form a part or all of the Wichita, Clear Fork, and Pease River Groups (Table 1 and Figure 5) which are present in the county.

Wichita Group

The Wichita Group, including those rocks older than the Lueders, ranges from slightly less than 800 to a little over 900 feet in thickness in Taylor County.

The Lueders Formation contains the only known potable water in this group and outcrops in the extreme eastern part of the county. It is about 80 feet thick and consists of alternating thin beds of gray limestone and shale.

Clear Fork Group

The Arroyo, Vale, and Choza Formations, from oldest to youngest, comprise the Clear Fork Group.

These rocks range in thickness from zero at the updip wedge-out in the eastern part of the county to slightly over 1,300 feet in the western part.

The Arroyo Formation is made up primarily of red and gray shales with thin shaley limestones alternating throughout. It is about 250 feet thick and is exposed in the eastern part of the county. Thin persistent limestone members of the Arroyo are, in ascending order, the Rainy Limestone, Lytle Limestone, Kirby Lake Limestone, and Standpipe Limestone.

The Vale Formation consists principally of red shales with thin scattered lenticular red and gray sandstones in the lower part and many thin interbedded dolomite and shale stringers in the upper part. The Bullwagon Dolomite Member occurs near the top of the formation. The Vale outcrops in the central part of the county and averages about 550 feet thick.

The Choza Formation contains mostly red shales, locally some gray shale, with thin carbonate beds in the lower part and, occasionally, thin shaley sandstones in the lower and middle part. This unit is exposed in the western part of the county and is about 510 feet thick. The thin Merkel Dolomite Member is at or near the top of the formation.

Pease River Group

The San Angelo Formation is the lone representative of this group in Taylor County. Exposures are found in the extreme western part of the county. It is about 200 feet thick and consists mainly of cross-bedded gray sandstone, with chert conglomerates and some shale in the lower part. It is dominantly non-marine and weathers to a red color at the outcrop.

Cretaceous System

The Cretaceous deposits of the county are composed of two groups, the Trinity and the overlying Fredericksburg. They are believed to attain a combined maximum thickness of about 300 feet.

Trinity Group

The Trinity Group in Taylor County is comprised entirely of the Antlers Formation. This marginal representative of the Trinity consists of light-colored sandstone in the upper part, well sorted and locally cross-bedded; primarily silty sandstone with pink to purple clay in the middle unit; and dominantly light-colored sandstone with some conglomerate in the

Table 1.-Geologic Units and Their Water-Bearing Properties in Taylor County

					APPROXIMATE		
					MAXIMUM		
SYSTEM	SERIES	GROUP	FORMATION	MEMBER	(ft)	LITHOLOGIC CHARACTER	WATER-BEARING CHARACTERISTICS
	Recent	Unconformity	Alluvium NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN	MAAAAAAAAA	30	Cross-bedded sandstones, gravel, fine silts, and sandy clays occurring in and bordering most of the stream channels in the county.	Yields fresh to moderately saline water in small to moderate quantities to wells mostly in the eastern two-thirds of the county.
			Undivided sur	ficial deposits	10	Residual soils of caliche and lag gravels capping many of the low-lying hills in the northern half of the county	Known to yield small quantities of fresh to slightly saline water to one well and one spring in the northern half of the county.
Quaternary	Pleistocene		Seymour		40	Contains fine grained, white, light tan to red sands and silts; reddish-orange and gray clay, and white to buff nodules of caliche (usually near surface). Lower portion of the formation is coarse gravels or conglomerates containing well rounded pebbles of quartz, quartzite, igneous crystalline rocks, bone fragments, petrified wood, scattered water-worn Cretaceous fossils, and cobbles and pebbles of limestone.	Known to yield small quantities of water to three wells along the county line north of Merkel in the northwest part of the county. Water in one well was fresh.
		mmmmm	20000000000000000000000000000000000000	unnnu		Gray to near-white, dense to fine crystalline, thin to thick-bedded limestone with thin irregular layers and nodules of dark bluish-gray chert.	Yields fresh water in small quantities to scattered wells and springs in the southern part of the county.
		Fredericksburg	Comanche Peak Limestone		100	Gray, thin to irregular, wavy-bedded, fossiliferous limestone with thin interbedded clay.	
Cretaceous	Comanche		Walnut			Marly, laminated, light gray to yellowish clay; some thin semi-crystalline limestone lenses locally.	
40.0000000.00	0000 000000	Trinity	Antiers	020000000000000000000000000000000000000	200	Lower and upper parts chiefly sand, middle part mainly clay. Sand is cream to near white, fine to medium grained, moderately to well sorted, weathers buff to locally varigated, some cross-bedding, argillaceous in the upper part. locally conglomeratic in the lower part. Middle part chiefly red to pink, purple, locally gray and green clay, silty, with occasional beds of hard calcareous siltstone. Conglomerate in lower part made up of chert and quartzite pebbles.	Yields fresh water in small quantities to wells and springs in the southern part of the county.
		Pease River	San Angelo		200	Cross bedded sandstone, green sh gray, usually well consolidated, medium-grained, sub-angular to well-rounded near top of unit, lower portion is clay balls, sandstone as above interbedded with cherty conglomerates, gypsum nodules, streaks of "satin spar" gypsum, and red and green shales.	Yields fresh to moderately saline water in small to moderate quantities to wells along the extreme western edges of the county.
			Choza	Merkel Dolomite	510	The gray Merkel dolomite, at or near the top of this formation, is not believed to be present southward from a point just south of Interstate 20 and about 1.5 miles east of Trent. The remainder of the formation consists of semi-parsistent beds of gray dolomite and anhydrite interspersed in red shales and, locally, thin poorly developed sandstone lenses.	Yields fresh to moderately saline water in small to moderate quantities to wells in the western part of the county.
Permian	Leonard	Clear Fork	Vale	Bullwagon Dolomite	10 550	Upper portion of the formation is comprised of many thin beds of gray dolomite and anhydrite interbedded with some clay, but mainly red shales. Lower portion of unit is dominately red shale with thin stringers of dolomite and a few thin lenticular shaley sandstones. This lower red shale unit thins to the west.	Yields fresh to moderately saline water in small quantities to a few wells in the eastern half of the county.
			Αττογο	Standpipe Limestone Kirby Lake Limestone Lytie Limestone Rainy Limestone	250	White, cream-colored, buff and brown, thin bedded and poorly developed limestones, dolomites, and marls interbedded with thick gray and red shales and lenticular shaley sandstones. Anhydrite is present, locally, near the base of the formation in the Lytle and Rainy Limestone Members.	Yields fresh to slightly saline water in small quantities to a few scattered wells in the eastern part of the county.
		Wichita	Lueders		80	Thin bedded, gray to buff, fossiliferous limestone interbedded with arguilaceous limestone and gray to greenish gray shales. Unit grades into colomite westward in the subsurface.	Yields slightly to moderately saline water in small quantities to a few scattered wells in the eastern part of the county.

Yield of Wells: Small, less than 100 gpm (gallons per minute); moderate, 100–1,000 gpm; large, more than 1,000 gpm.

basal section. Its outcrop forms the lower slopes of the mesas and buttes in southern Taylor County. The Antlers is believed to reach a maximum of about 200 feet in thickness.

Fredericksburg Group

This group is made up of, in ascending order, the Walnut Formation, Comanche Peak Limestone, and Edwards Limestone. These formations form the mesas and buttes which rise above the surrounding land surface in the southern part of the county. The Walnut Formation is composed of marly yellow clay which grades into shaley limestone locally. The Comanche Peak Limestone consists of gray, nodular, marly limestone. It contains a thin, carbonate detrital zone near the middle. The Edwards Limestone is a cream to gray, crystalline limestone with considerable chert which occurs as thin beds or nodules. In this report, the Fredericksburg Group will be treated as a single unit. The combined thickness of these beds in Taylor County is about 100 feet.

Quaternary System

Pleistocene Series

Sand, silt, and gravel, with varying amounts of clay, form a thin mantle which rests unconformably on Permian beds in much of the northern half of Taylor County. Many of these deposits near the Taylor-Jones county line are assigned to the Seymour Formation, whereas others are believed to be younger Pleistocene and, at least in part, derived from the Seymour. Locally the Seymour deposits may be as much as 40 feet thick.

Recent Series

Alluvial deposits composed of fine sand, silt, clay, and gravel occur in and bordering many of the streambeds of the county. These stream deposits are derived from older Pleistocene sediments as well as Cretaceous and Permian rocks. The thickness of the alluvium is believed to be no greater than 30 feet. Figure 11 depicts the approximate saturated thickness of the alluvium along Jim Ned and East Jim Ned Creeks near the communities of Tuscola and Lawn.

Regional Structure

The major subsurface structural features of central and north-central Texas are shown on Figure 6. Taylor County is located on the west flank of the Bend Flexure. This feature probably had its beginning in late Pennsylvanian or early Permian times as a result of westward land subsidence and regional tilting. This movement continued through the Permian and probably into early Mesozoic time. Regional dip of the Permian strata is to the west-northwest at about 40 feet per mile. The beds crop out in irregular belts having a north-south trend and becoming successively younger from east to west across the county.

The Cretaceous deposits of Taylor County overlie the Permian with a marked unconformity caused by post-Permian, pre-Cretaceous uplift, erosion, and tilting to the south and east. Regional dip on these strata is to the southeast at rates up to 25 feet per mile (Farris et al., 1963).

Quaternary deposits lie unconformably on Permian rocks and generally assume an attitude equivalent in rate and direction to local topography.

Geomorphology

The low-relief structure in the Taylor County area has little effect on land forms. In the area surrounding the Cretaceous outcrops, the main controlling factor is the differential erosion of the Permian age rocks forming the surface. These forms, called cuestas, are many times accentuated by a Pleistocene sand and/or gravel remnant capping the elevated areas. Local relief is usually less than 50 feet. The front slope or scarp of the cuestas face in an eastward direction.

The mesas and buttes, with prominent northward facing scarps which rise quickly above the rolling to near-level surface, mark the Cretaceous deposits. These features are outliers or erosional remains of the once more-extensive Edwards Plateau. They are found in a broken east-west line extending across southern Taylor County. Relief in their immediate area is as much as 400 feet. These broken plateau remnants lie along a belt commonly called the Callahan Divide. This belt divides the Colorado River drainage system to the south from the Brazos River drainage system to the north.

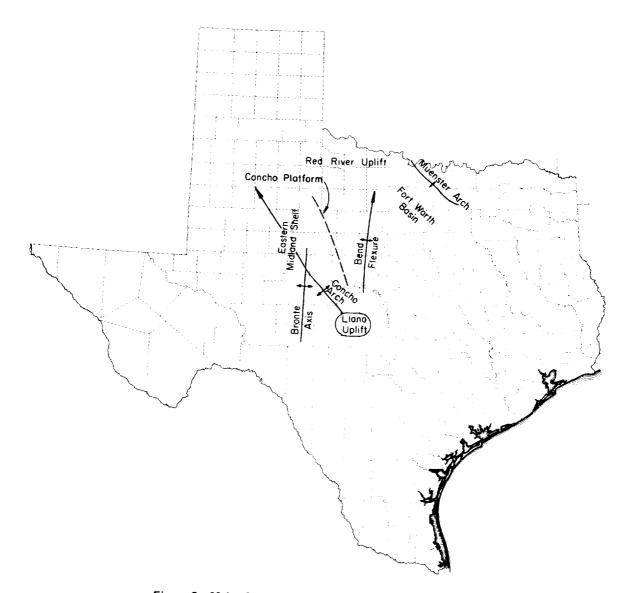


Figure 6.—Major Structural Features in North-Central Texas

GENERAL GROUND-WATER HYDROLOGY

Hydrologic Cycle

Figure 7 illustrates the circulation system of water on the earth. It shows the continued movement of water from the oceans, by evaporation, to the land where it is released as precipitation, and finally its return, either directly or indirectly, to the oceans. This system is called the hydrologic cycle.

Ground water, or phreatic water, is that part of the returning water which has moved downward through void spaces, or pores, in the various soils and rocks making up the crust or outer shell of the earth, and entered the water table. The water table is the upper surface of the zone of saturation in which all void spaces in the rocks or sediments are completely filled with water. From time to time some of the subsurface water, on its downward percolation, will encounter impermeable beds above the normal water table. This water is trapped and forms a *perched water table*.

That subsurface water which does not reach the water table but remains in the *zone of aeration*, in which some of the void spaces of the sediments are filled with air and some with water, is known as *vadose* or *suspended subsurface water* (Meinzer, 1923, p. 22).

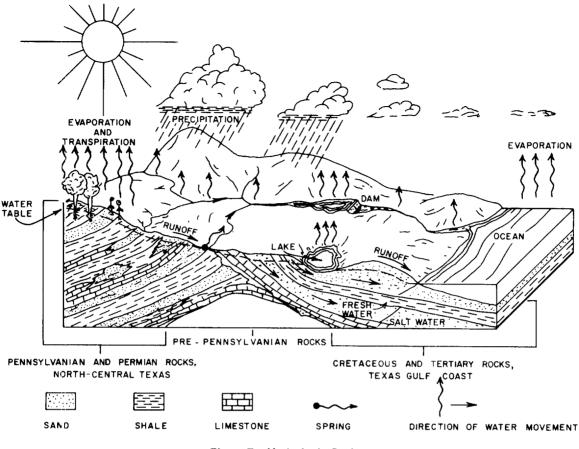


Figure 7.—Hydrologic Cycle

Source and Occurrence of Ground Water

The source of all fresh ground water is precipitation; however, only a small percentage of the the precipitation ultimately becomes ground water.

A working knowledge of the geologic history of an area is most beneficial in understanding the occurrence and movement of ground water. Ground water occurs as accumulations of water in geologic formations. If the formation or formations will yield water in significant or usable quantities it is termed an *aquifer*. The sizes of aquifers may vary from a few to thousands of square miles.

There are two types of aquifers, unconfined and confined. An *unconfined aquifer* is one in which water-table conditions exist; that is, the upper surface of the zone of saturation is unconfined and under atmospheric pressure. Under these conditions, mapping of the water table reveals that it will usually take on the configuration of the topography of the land surface. A *confined aquifer* is one in which its water is restricted and under pressure due to the aquifer dipping under the land surface below non-porous beds. These waters are said to be under artesian conditions. The mapped surface under these conditions is one of pressure, called the *piezometric surface*. It is an imaginary surface representing the elevation to which water will rise when the aquifer is penetrated.

In aquifers containing relatively unconsolidated deposits, such as sand and gravel, water is found in the spaces between individual particles. In aquifers made up of more compact or well-cemented rocks, such as limestones, dolomites, and others, the water occurs mostly in cracks or fractures caused by force of earth movement or in spaces such as vugs, caverns, or channels caused by the dissolving action of water.

Recharge, Discharge, and Movement of Ground Water

Recharge is the process by which water is added to an aquifer. Natural recharge is accomplished by precipitation directly on the exposed surface of an aquifer or seepage from surface streams, lakes, ponds and the like which are in direct contact with the aquifer. An aquifer may also receive natural recharge by leakage when in hydraulic contact with another aquifer. The discharge of water onto the surface outcrop of an aquifer or pumping of water into an aquifer effects artificial recharge.

Factors that limit recharge of an aquifer are the amount and frequency of precipitation, the area and extent of the outcrop, topography, the type and amount of vegetation on and in the vicinity of the recharge area, the condition of the soils, the permeability of the aquifer, and its capacity to accept recharge.

Discharge is the process by which water is removed from an aquifer. Natural discharge occurs as spring flow, effluent seepage or flow of water from an aquifer into a stream caused by the water table being at a higher elevation than the stream channel, leakage of water from one aquifer into another, transpiration by vegetation, and by evaporation. Artificial discharge is accomplished through withdrawal from wells and by ditching.

The rate of movement of ground water is usually very slow, being in the magnitude of a few feet to a few hundred feet per year. This movement is from areas of recharge to areas of discharge or from points of higher hydraulic head to those of lower hydraylic head. The movement is in the direction of the hydraulic gradient just as in the case of surface-water flow. Under normal artesian conditions, ground-water movement is usually in the direction of regional dip of the aquifer. Under water-table conditions, the slope of the water table and consequently the direction of movement of the ground water is closely related to the slope of the land surface. However, under either condition, local anomalies are developed in areas of pumping and some water moves toward the points of artificial discharge.

Hydraulic Properties of Aquifers

The capacity of an aquifer to yield water to wells depends on the ability of that aquifer to transmit and store water, which in turn is dependent upon the permeability and porosity of the sediments which make up the aquifer. *Permeability* is the ability of rock to transmit fluid whereas *porosity* is the measure of the amount of its void space expressed as a percentage of the total volume of the rock. Differences in capacities between aquifers, as well as within a single aquifer, are caused by variations in permeability and porosity which depend largely on rock composition.

The hydraulic gradient of an aquifer, at a given place in a given direction, is the rate of change of

pressure head per unit of distance at that place and in that direction. (Meinzer, 1923, p. 38).

The coefficient of permeability of an aquifer is expressed as the number of gallons of water per day moving through a cross-sectional area of 1 square foot under a hydraulic gradient of 1 foot per foot $(45^{\circ} \text{ slope})$ at a temperature of 60° F (Kazmann, 1965, p. 135). In the field the adjustment to standard temperature is usually ignored and the permeability is commonly understood to be a field coefficient at the prevailing water temperature.

The coefficient of transmissibility is a measure of the capability of an aquifer to transmit water. It is defined as the number of gallons of water per day that will flow through a vertical section of the aquifer 1 foot wide and having a height equal to the full thickness of the aquifer, at a hydraulic gradient of 1 foot per foot (After Theis, 1938, p. 889-902). The coefficient of transmissibility is an important characteristic of an aquifer in the calculation of the amount of water available on a continuing use basis. It is the product of the coefficient of permeability and aquifer thickness.

The coefficient of storage is a measure of the water-yielding capacity of an aquifer. It is the volume of water an aquifer releases from or takes into storage per unit horizontal surface area of the aquifer per unit change in the component of the head normal to that surface (Todd, 1959, p. 31). Under water-table conditions, the coefficient of storage is equal to the specific yield or the quantity of water that the saturated material will yield under the influence of gravity. Under artesian conditions, the coefficient of storage is a measure of the aquifer's ability to yield water by compression of its sediments and the expansion of the water as the piezometric surface is lowered. The coefficient of storage is usually much smaller in aquifers under artesian conditions. As a result, a water well producing under artesian conditions will develop a large cone of depression over a wide area in a very short time, while a comparable well producing from an aquifer under water-table conditions will develop a small cone of depression in a much longer period of time, the difference being in the storage capabilities of the two types of aquifers.

Development of Ground Water

Irrigation

Ground water for use as irrigation water must be available in relatively large amounts which can be supplied in fairly short periods of time.

In Taylor County ground water for irrigation use is restricted due to small aquifers and, generally, small yields of wells. In some cases, the water quality has deteriorated to such a degree that it can no longer be used for irrigation.

The main areas of development of ground water for irrigation are in the southeastern part of the county, along Jim Ned Creek between Tuscola and Lawn; in and around Merkel in the northwestern part of the county; and in the east-central part of the county, along Elm Creek, between Buffalo Gap and Abilene (Figures 5 and 25).

The first known use of ground water for irrigation was in the middle 1940's. Although significant amounts of ground water are still used for irrigation purposes, it is probable that its use for this purpose reached a peak in the late 1950's and early to mid-1960's.

Public Supply

Ground water for use as public-supply water must also be available in relatively large amounts although these can be supplied, generally, over longer periods of time than for irrigation purposes. Dependability of supply is of prime importance in development of ground water for public supply.

The only known public-supply wells in use at the time of this study were those supplying the communities of Buffalo Gap, Tuscola, and Ovalo. The first known public-supply wells for use by towns were drilled in the 1920's and the last known were drilled in the 1960's. The towns of Lawn, Merkel, and Trent at one time depended on wells for water supply but have since abandoned them for surface water. In years past some rural schools used ground water.

Industrial

Demands on ground water for industrial purposes can vary widely, but it generally must be of good quality.

Ground water has been used in industry in the county since at least as far back as 1939. Limited records indicate use of ground water in the ginning of cotton at one time. It also was used by an electric company for a few years. Water from wells has been used, and still is, in small amounts for building and maintaining highways. Records show that fresh to slightly saline ground water has been used in the past in the drilling of oil tests and in water-flood operations but, as far as is known, as of 1971 it is used only in one small gas plant operation in the county.

The use of ground water for mining limestone for highway road metal has more than doubled each year from about 1965 through 1970. A feedlot operation in the county has increased use of ground water by about 25 percent each year since 1967.

Domestic and Livestock

In many semiarid and arid regions, ground water is essential for domestic and livestock uses. In some areas the ground water available may determine man's existence. Its presence will bear on the kind of existence man leads in any particular area where water is in short supply. Taylor County lies near to semiarid to arid regions to the west and its people have depended to some extent on ground water since shortly after the first settlers arrived in the mid-1800's.

The oldest wells inventoried during this study were developed in the late 1880's. By the early 1900's every farm house in the county probably was served by one or more wells if ground water was available. As the small farms were abandoned some of the wells were also abandoned but many were maintained for livestock use. In recent years new wells drilled primarily for small-scale livestock and/or irrigation use have increased in the areas surrounding larger towns due to more and more families moving to these areas. These wells supply water for a few livestock and for irrigation on small tracts used to grow feed for the livestock.

Changes in Water Levels

In wells, measurements of the depth to the water, of the water level, indicate the position of the water table or of the piezometric surface of the aquifer, as the case may be. Changes in the amount of water in storage in a given aquifer are reflected by water-level fluctuations, and these changes may be on a local or regional basis. A rise of the water level indicates an increase in storage whereas a lowering of the water level indicates a decrease in storage. Water-level changes may occur also as a result of earthquakes or tidal forces. More commonly, minor fluctuations occur due to atmospheric pressure changes or small withdrawals from wells. Greater water-level changes occur in areas of irrigation where heavy pumping by many wells over longer periods of time takes place.

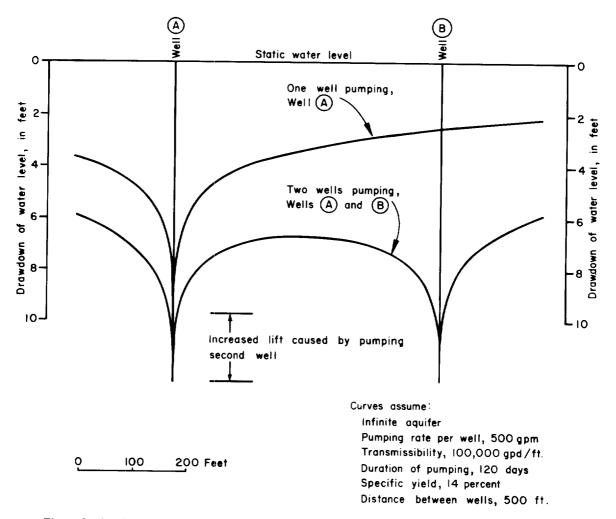


Figure 8.—Idealized Cross Section Showing Drawdown Interference Between Two Pumping Wells

Pumping water from a well will cause a *cone of depression* to be formed in the water table or piezometric surface around the well bore. It is so called because its shape is that of an inverted cone with the apex at the well bore (Figure 8, well A). As pumping continues this cone will expand and continue to do so until sufficient sources of water are encountered to satisfy the withdrawal demand or it meets the cone of depression of another well. When a number of these cones of depression meet and combine, a regional cone of depression is formed (Figure 8, well A + B).

Limited historical data indicate that water levels, in general, have risen since 1939 in Taylor County (Table 5).

GENERAL CHEMICAL QUALITY OF GROUND WATER

All ground water contains dissolved minerals. The kind and concentration of these minerals, or the chemical composition of the ground water, depends upon the movement and source of the ground water, and of greatest importance, the soil and rock through which it has moved. In general, the concentrations of dissolved minerals in water increase with depth and are greater in rock units where ground-water circulation is restricted.

Table 7 is a tabulation of chemical analyses of water from selected wells and springs in Taylor County and adjacent areas. Figure 9 shows the concentrations of some of the more important chemical constituents for this area. These data were obtained from chemical analyses of water samples collected from selected wells. The various well symbols shown on Figure 9 represent the water-bearing formations in the county.

Relationship of Water Quality to Use

Uncontaminated ground water is very desirable for many uses due to its relatively constant chemical quality and temperature as compared to surface water.

For many purposes the dissolved-solids content is a major limitation on the use of water. A general classification of water by Winslow and Kister (1956, p. 5), based on dissolved-solids content, is as follows:

DESCRIPTION	DISSOLVED- SOLIDS CONTENT (mg/l)*
Fresh	Less than 1,000
Slightly saline	1,000 to 3,000
Moderately saline	3,000 to 10,000
Very saline	10,000 to 35,000
Brine	More than 35,000

*Milligrams per liter (mg/l) is considered equivalent to parts per million (ppm) for water containing less than 7,000 mg/l dissolved solids.

The principal mineral constituents found in ground water are calcium, magnesium, sodium, potassium, bicarbonate, sulfate, chloride, silica, iron, manganese, nitrate, fluoride, and boron.

Water used for municipal or public supply, as well as for domestic purposes, should be colorless, odorless, and palatable. It should be chemically as well as bacteriologically safe for consumption. The standard test for bacteriologic quality is the determination of coliform bacteria concentration. Chemically, the mineral content of water should be within the limits recommended by the U.S. Public Health Service (1962). The limits on some of these chemical constitutents, reported in milligrams per liter, are as follows:

SUBSTANCE	CONCENTRATION (mg/l)
Chloride (C)	250
Fluoride (F)	1.0*
Iron (Fe)	0.3

SUBSTANCE	CONCENTRATION (mg/l)
Manganese (Mn)	0.05
Nitrate (NO ₃)	45
Sulfate (SO ₄)	250
Dissolved solids	500

*Recommended upper limit of concentration of fluoride for Taylor County based on annual average maximum daily air temperature of 76.3°F. Lower limit recommendation--0.7 mg/l, optimum--0.8 mg/l.

Water supplies with mineral concentrations greater than the above, out of necessity, have been and are being used in Taylor County with no apparent ill effects. Smith et al. (1942, p. 15) stated that some livestock have been known to survive on water containing as much as 10,000 ppm dissolved solids, although much better quality is necessary for maximum growth and reproduction. Some objections to water with mineral contents exceeding those recommended by the U.S. Public Health Service are explained in Table 2.

Hardness of water, expressed in milligrams per liter as calcium carbonate, is an important factor in water for industrial use as well as domestic and public supply. The principal constituents causing hardness of water are calcium and magnesium. Increasing hardness causes an increase of soap consumption in washing and laundering processes. It also causes formation of scale in boilers and other equipment. A generalized classification for hardness (Durfor and Becker, 1964, p. 29), useful as an index to the analyses of water, is as follows:

CONCENTRATION (mg/l)	CLASSIFICATION
Less than 60	Soft
61 to 120	Moderately hard
121 to 180	Hard
More than 180	Very hard

Excessive amounts of silica, calcium, and magnesium in water cause scale deposits. Too much manganese and iron cause staining of laundered goods and affect the taste of the water.

There are a number of factors involved in determining the suitability of water for irrigation

Table 2.—Source and Significance of Dissolved-Mineral Constituents and Properties of Water

(Adapted from Doll and others, 1963, p. 39-43)

CONSTITUENT OR		
PROPERTY	SOURCE OR CAUSE	SIGNIFICANCE
Silica (SiO ₂)	Dissolved from practically all rocks and soils, commonly less than 30 mg/l. High concentrations, as much as 100 mg/l, generally occur in highly alkaline waters.	Forms hard scale in pipes and boilers. Carried over in steam of high pressure boilers to form deposits on blades of turbines. Inhibits deterioration of zeolite-type water softeners.
Iron (Fe)	Dissolved from practically all rocks and soils. May also be derived from iron pipes, pumps, and other equipment.	On exposure to air, iron in ground water oxidizes to reddish-brown precipitate. More than about 0.3 mg/l stains laundry and utensils reddish-brown. Objectionable for food processing, textile processing, beverages, ice manufacture, brewing, and other processes. U.S. Public Health Service (1962) drinking water standards state that iron should not exceed 0.3 mg/l. Larger quantities cause unpleasant taste and favor growth of iron bacteria.
Calcium (Ca) and Magnesium (Mg)	Dissolved from practically all soils and rocks, but especially from limestone, dolomite, and gypsum. Calcium and magnesium are found in large quantities in some brines. Magnesium is present in large quantities in sea water.	Cause most of the hardness and scale-forming properties of water; soap consuming (see hardness). Waters low in calcium and magnesium desired in electroplating, tanning, dyeing, and in textile manufacturing.
Sodium (Na) and Potassium (K)	Dissolved from practically all rocks and soils. Found also in oil-field brines, sea water, industrial brines, and sewage.	Large amounts, in combination with chloride, give a salty taste. Moderate quantities have little effect on the usefullness of water for most purposes. Sodium salts may cause foaming in steam boilers and a high sodium content may limit the use of water for irrigation.
Bicarbonate (HCO ₃) and Carbonate (CO ₃)	Action of carbon dioxide in water on carbonate rocks such as limestone and dolomite.	Bicarbonate and carbonate produce alkalinity. Bicarbonates of calcium and magnesium decompose in steam boilers and hot water facilities to form scale and release corrosive carbon-dioxide gas. In combination with calcium and magnesium, cause carbonate hardness.
Sulfate (SO₄)	Dissolved from rocks and soils containing gypsum, iron sulfides, and other sulfur compounds. Commonly present in some industrial wastes.	Sulfate in water containing calcium forms hard scale in steam boilers. In large amounts, sulfate in combination with other ions gives bitter taste to water. U.S. Public Health Service (1962) drinking water standards recommend that the sulfate content should not exceed 250 mg/l.
Chloride (Cl)	Dissolved from rocks and soils. Present in sewage and found in large amounts in oil-field brines, sea water, and industrial brines.	In large amounts in combination with sodium, gives salty taste to drinking water. In large quantities, increases the corrosiveness of water. U.S. Public Health Service (1962) drinking water standards recommend that the chloride content should not exceed 250 mg/l.
Fluorice (F)	Dissolved in small to minute quantities from most rocks and soils. Added to many waters by fluoridation of municipal supplies.	Fluoride in drinking water reduces the incidence of tooth decay when the water is consumed during the period of enamel calcification. However, it may cause mottling of the teeth, depending on the concentration of fluoride, the age of the child, amount of drinking water consumed, and susceptibility of the individual (Maier, 1950, p. 1120-1132).
Nitrata (NO ₃)	Decaying organic matter, sewage, fertilizers, and nitrates in soil.	Concentration much greater than the local average may suggest pollution. U.S. Public Health Service (1962) drinking water standards suggest a limit of 45 mg/l. Waters of high nitrate content have been reported to be the cause of methemoglobinemia (an often fatal disease in infants) and therefore should not be used in infant feeding (Maxcy, 1950, p. 271). Nitrate shown to be helpful in reducing inter-crystalline cracking of boiler steel. It encourages growth of algae and other organisms which produce undesirable tastes and odors.

Table 2.—Source and Significance of Dissolved-Mineral Constituents and Properties of Water—Continued

CONSTITUENT

OR PROPERTY	SOURCE OR CAUSE	SIGNIFICANCE
Boron (B)	A minor constituent of rocks and of natural waters.	An excessive boron content will make water unsuitable for irrigation. Wilcox (1955, p. 11) indicated that a boron concentration of as much as 1.0 mg/l is permissible for irrigating sensitive crops; as much as 2.0 mg/l for semitolerant crops; and as much as 3.0 mg/l for tolerant crops. Crops sensitive to boron include most deciduous fruit and nut trees and navy beans semitolerant crops include most small grains, potatoes and some other vegetables, and cotton; and tolerant crops include alfalfa most root vegetables, and the date palm.
Dissolved solids	Chiefly mineral constituents dissolved from rocks and soils.	U.S. Public Health Service (1962) drinking water standard: recommend that waters containing more than 500 mg/l dissolved solids not be used if other less mineralized supplies are available For many purposes the dissolved-solids content is a majo limitation on the use of water.
Hardness as CaCO3	In most waters nearly all the hardness is due to calcium and magnesium. All of the metallic cations other than the alkali metals also cause hardness.	Consumes soap before a lather will form. Deposits soap curd or bathtubs. Hard water forms scale in boilers, water heaters, and pipes. Hardness equivalent to the bicarbonate and carbonate i called carbonate hardness. Any hardness in excess of this i called non-carbonate hardness.
Sodium-adsorption ratio (SAR)	Sodium in water.	A ratio for soil extracts and irrigation waters used to express th relative activity of sodium ions in exchange reactions with so (U.S. Salinity Laboratory Staff, 1954, p. 72, 156). Defined b the following equation:
		$SAR = \frac{Na^+}{\sqrt{Ca^{++} + Mg^{++}}},$
		where Na ⁺ , Ca ⁺⁺ , and Mg ⁺⁺ represent the concentrations i milliequivalents per liter (me/l) of the respective ions.
Residual sodium Sodium and carbonate or carbonate bicarbonate in water. (RSC)		As calcium and magnesium precipitate as carbonates in the so the relative proportion of sodium in the water is increase (Eaton, 1950, p. 123-133). Defined by the following equation
		$RSC = (CO_3^{-+} + HCO_3^{} - (Ca^{++} + Mg^{++}))$
	where CO3 [,] HCO3 ⁻ , Ca ⁺⁺ , and Mg ⁺⁺ represent th concentrations in milliequivalents per liter (me/l) of th respective ions.	
Specific conductance (micromhos at 25°C)	Mineral content of the water.	Indicates degree of mineralization. Specific conductance is measure of the capacity of the water to conduct an electr current. Varies with concentration and degree of ionization the constituents.
Hydrogen ion concentration (pH)	Acids, acid-generating salts, and free carbon dioxide lower the pH. Carbonates, bicarbonates, hydroxides, phosphates, silicates,	A pH of 7.0 indicates neutrality of a solution. Values higher tha 7.0 denote increasing alkalinity; values lower than 7.0 indica increasing acidity. pH is a measure of the activity of t hydrogen ions. Corrosiveness of water generally increases wi decreasing pH. However, excessively alkaline waters may al

purposes other than the chemical quality of water. Soil type, drainage, management practice, crop type, climate, and quantity of water used all have an important bearing on the continued productivity of irrigated soils.

The chemical characteristics of water that are of primary concern in determining its suitability for irrigation are: (1) Specific conductance, (2) percent sodium, (3) sodium-adsorption ratio (SAR), (4) residual sodium carbonate (RSC), and (5) concentrations of boron that may be toxic to crops. Specific conductance is a measure used in the field to give an indication of the concentration of soluble salts in the water. Percent sodium is a term used to indicate the proportion of sodium ions in solution in relation to the total cation concentration. Sodium-adsorption ratio is used to express the relative activity of sodium ions in exchange reactions with soil.

A system of classification commonly used for judging the quality of water for irrigation was proposed by the U.S. Salinity Laboratory Staff (1954). The classification is based on the salinity hazard as measured by the electrical conductivity (specific conductance) of the water and the sodium, or alkali, hazard as measured by the sodium-adsorption ratio (SAR). The diagram used in this classification is shown as Figure 10. The intersection of a horizontal line projected from the SAR value found on the vertical scale with a vertical line projected from the specific conductance value found on the horizontal scale of the diagram classifies the particular water analyzed as to its salinity hazard (C1, C2, C3, or C4 below the horizontal scale) and sodium hazard (S1, S2, S3, or S4 to the left along the vertical scale). Limitations concerning the use of waters so classified are given in Table 3.

The degree of salt concentration in irrigation water is usually not high enough to affect the plant growth. High salt accumulation in the soil, however, does affect plant growth. As the salt concentration in the water

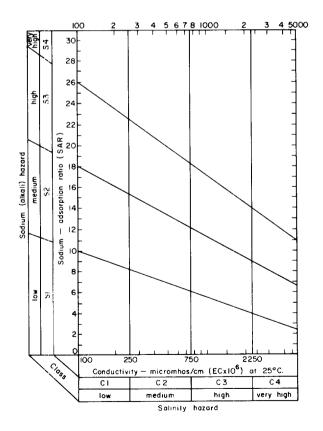


Figure 10.–Diagram for the Classification of Irrigation Waters (After U.S. Salinity Laboratory Staff, 1954, p. 80)

increases, the salinity hazard, or the tendency of salts to accumulate in the soil, also increases. Generally the better the soil drainage and permeability, the higher the salinity of the water that may be used for irrigation. It should also be kept in mind, however, that different crops have different salt tolerances.

Application of waters with excessive sodium can cause soil-structure breakdown by increasing the concentration of sodium in the soil. Affected soils tend to become plastic and impermeable to water and air movement, causing cultivation difficulties and drainage problems. Soils with excessive accumulations of sodium are harmful to sodium-sensitive plants which can result in crop damage.

The RSC is another factor used in assessing the quality of water for irrigation. As soil begins to dry following irrigation, the remaining solution in the soil becomes progressively more concentrated. This condition creates a tendency for compounds less soluble than sodium carbonate, such as calcium and magnesium carbonates, to precipitate from solution. The result is an increase in the proportion of sodium in solution. The extent to which calcium and magnesium carbonates will precipitate and the conditions favoring this precipitation are not fully understood. Wilcox (1955, p. 11) gives the following limits for residual sodium carbonate (RSC) for irrigation waters: above 2.5 me/l (milliequivalents per liter) is not suitable for irrigation, 1.25 to 2.5 me/l is marginal, and water containing less than 1.25 me/l is probably safe (Table 2).

Boron is necessary for plant growth, but is highly toxic at concentrations slightly more than optimum. Table 2 shows limits that have been set on boron concentrations for water used for irrigation.

Changes in Chemical Quality

In addition to usually gradual changes in chemical quality of ground water that can be brought about by natural mineralization, man also causes lasting changes through contamination such as: disposal of industrial waste into improperly completed, or faulty, disposal pits or wells; inadequate plugging of test holes; severe corrosion of oil-well and other casings which permits highly mineralized water to enter and contaminate fresh water aquifers; improper disposal of wastes into surface streams providing recharge to aquifers; and poorly constructed wells with improper casing or cementing which allows water of inferior quality to enter the well or move into an aquifer having a lower hydrostatic head.

Table 3.—Water-Use Limitations of Salinity and Sodium Hazard—Classified Irrigation Waters Shown in Figure 10 (After Lyerly et al., 1957, p. 13-15).

HAZARD	CLASSIFICATION AND LIMITATIONS
	C1) Low-salinity water—can be used for irrigation with most crops on most soils with little likelihood that soil salinity will develop. Some leaching is required; care should be taken with soils of extremely low permeability.
	C2) Medium-salinity water—can be used if a moderate amount of leaching occurs. Plants with moderate salt tolerance can be grown in most cases without special practices for salinity control.
Salinity	C3) High-salinity water—cannot be used on soils with restricted drainage. Even with adequate drainage, special management for salinity control may be required. Plants selected should have good salt tolerance.
	C4) Very high-salinity water—may be used occasionally under special conditions. Soils must be permeable and drainage adequate. Highly salt-tolerant crops, only, should be selected. Excess irrigation water must be applied to provide considerable leaching.
	S1) Low-sodium water—can be used for irrigation on almost all soils with little danger of the development of harmful levels of exchangeable sodium. However, sodium-sensitive crops, such as stone-fruit trees and avocados, may accumulate injurious concentrations of sodium.
	S2) Medium-sodium water—recommended for use on coarse-textured or organic soils having good permeability. Unless gypsum is present in the soil, this water will present an appreciable sodium hazard in fine-textured soils having high cation-exchange capacity, especially under low-leaching conditions.
Sodium	S3) High-sodium water—requires special soil management (good drainage, high leaching, organic matter additions) as it may produce harmful levels of exchangeable sodium in most soils although, not necessarily in gypsiferous soils. Chemical amendments may be required for replacement of exchangeable sodium, but this may not be feasible with waters of very high salinity.

S4) Very high-sodium water-generally unsatisfactory for irrigation except at low and, possibly, medium salinity, where the solution of calicium from the soil or use of gypsum or other additives may make the use of these waters feasible.

It is desirable that the quality of water produced by a well remain constant. However, heavy demainds on an aquifer by increased pumpage will impose new hydrologic conditions of possible regional extent upon the aquifer. The result may be the invasion of the aquifer by water of undesirable quality.

Short-term local changes of water quality may be brought about by adjustment of hydraulic pressures of an aquifer caused by the demands of pumping. In the case of an irrigation well producing water from several zones, each of which may contain water of different quality, initial withdrawals will reflect the quality of the water from the zone having the highest hydrostatic head. As pumping continues, the quality of the water produced will likely change to that of the zone which contributes the greatest quantity of water to the well under the altered pressure conditions. The amount of water contributed by each zone will depend upon the transmissibility of the zone as well as the hydraulic head. In this manner, the quality of water pumped would have significant changes over a period of time and would eventually stabilize.

Treatment of Water

Water that does not meet requirements for a particular need may be treated so that it can become usable for that need. Treatment methods include softening, aeration, filtration, cooling, blending, and addition of chemicals. The limiting factor on water treatment is economics. Once a treatment is established on a particular ground water it will probably not have to be changed as the chemical characteristics of an uncortaminated ground water will usually remain near constant.

AVAILABILITY AND QUALITY OF GROUND WATER

Principal Aquifers

Recent Alluvium

The Recent alluvium, particularly that which is located along Jim Ned Creek from just northwest of Tuscola to a short distance east of Lawn, is believed to be the most important aquifer in Taylor County (Figures 5 and 11). This is based on the estimated amount of water used from this aquifer as compared to all other aquifers in the county. A total of 219 wells which produce or have produced from this aquifer were inventoried during this study (Table 5).

Extent of the Aquifer

Deposits of alluvium are found in the channels and small flood plains of most of the drainage tributaries in the county. The maximum thickness of this aquifer is believed to be about 30 feet. The alluvial deposits cover an estimated 20 percent of the surface area of the county with the largest concentration found in the eastern one-half of the county.

Source and Occurrence of Ground Water

Besides precipitation falling directly on the outcrop, the alluvium derives its water through seepage of runoff water from heavy rainfall and from lakes and ponds on or in close proximity to the outcrop. In the southern part of the county, discharge from Cretaceous rocks undoubtedly contributes water to the alluvium, particularly along Elm Creek. Ground water occurs in the alluvium along most of the major drainage tributaries in all but the extreme southwest part of the county. The amount of water available for use will vary according to the saturated thickness, porosity, and permeability.

Clays, silts, and soils which are fine-grained frequently have high porosities (50 percent and higher) but yield small to insignificant amounts of water due to poor or low permeabilities. Better yields are usually found in the coarser grained sands and gravels because of higher permeability. Known areas in the county in which wells have the high yields required for irrigation are along Jim Ned and Elm Creeks, and also at one place each on Cat Claw and Nubia Creeks (Figure 25).

Movement, Recharge, and Discharge of Ground Water

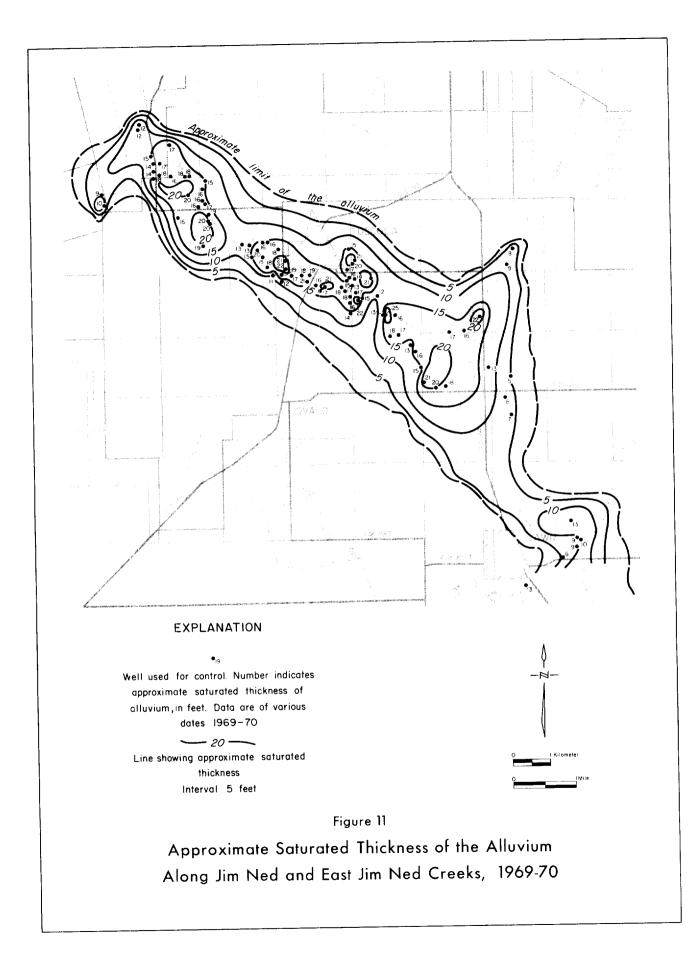
North of the Callahan Divide in Taylor County the general direction of movement of the ground water in alluvium along streams is northerly, and to the south of the divide it moves in a southerly direction. In Taylor County, the slope of the water table of alluvium ground water is closely related to the slope of the land surface. Local anomalies caused by pumping cause some of the ground water to move toward these points of artificial discharge.

The main source of recharge to the alluvium is precipitation on the outcrop and surface runoff. In areas of irrigation the alluvium is also recharged by infiltration of some of the water pumped from wells.

Natural discharge of alluvial ground water is probably small in the county. It can be discharged into any of the westward dipping Permian strata with which the alluvium may be in contact if geologic and hydrologic conditions are favorable. Drainage by effluent seepage is believed to occur along Jim Ned Creek where erosion has lowered the streambed below the level of the water table. Most of the ground-water discharge from the alluvium is a result of pumping.

Chemical Quality

A total of 131 water samples were collected from wells that produce water from the alluvium in Taylor County for chemical analysis during this investigation. These analyses are shown in Table 7.



Ranges in concentration of the principal chemical constituents found in these samples are as follows:

Calcium	23	to	306	mg/I
Magnesium	6	to	378	mg/I
Sodium plus Potassium	7	to 1	,010	mg/l
Bicarbonate	100	to	960	mg/l
Sulfate	12	to 1	,620	mg/l
Chloride	11	to 1	,140	mg/l
Fluoride	0.3	to	8.4	mg/l
Nitrate<	0.4	to	326	mg/l

By applying the general classification of waters devised by Winslow and Kister (1956, p. 5), it was determined that 34 percent of the alluvium ground-water samples collected were fresh water (less than 1,000 mg/l dissolved solids), 61 percent were slightly saline water (1,000 to 3,000 mg/l dissolved solids), and 5 percent were moderately saline water (3,000 to 10,000 mg/l dissolved solids). Only about 10 percent of the samples analyzed were within the range of dissolved-solids concentration (less than 500 mg/l) recommended for public drinking water by the U.S. Public Health Service (1962). Limited historical data in the Tuscola area show the following changes:

		DISSOLVED-SOLIDS CONTENT AND DATE SAMPLED			
WELL	PREVIOUS STUDIES	THIS STUDY			
30-50-121	739 mg/l (1939)	1,950 mg/l (1970)			
30-50-501	1,130 mg/l (1960)	1,110 mg/l (1970)			
30-50-505	1,030 mg/l (1946)	1,260 mg/l (1969)			
30-50-507	1,380 mg/I (1946)	1,390 mg/l (1970)			
30-50-601	1,060 mg/l (1960)	1,230 mg/t (1969)			

The alluvium ground water typically is very hard, as 97 percent of the water samples contained more than 180 mg/l total hardness. Table 2 presents the cause and significance of water hardness. Cretaceous beds forming much of the surface in Taylor County contain considerable amounts of limestone while the Permian strata, also exposed in Taylor County, contain some dolomite, gypsum, and limestone (Table 1 and Figure 5). These types of rocks contain much calcium and magnesium. Some of these constituents found in alluvium ground water undoubtedly were carried into the aquifer in solution by waters which first passed over and through the Cretaceous and Permian strata. U.S. Public Health Service (1962) drinking-water standards recommended that sulfate content of water not exceed 250 mg/l. Table 2 indicates sources and significance of sulfate in water. About 58 percent of the analyses of the water samples from the alluvium are within the recommended range. Another 31 percent range from 250 to 500 mg/l while the remaining 11 percent are over 500 mg/l. It is believed that much of the sulfate content of these waters was derived from the Permian rocks.

Under conditions pointed out in Table 2, an optimum amount of fluoride in drinking water reduces tooth decay but fluoride may cause mottling or discoloration of the teeth when the optimum amount is slightly exceeded. The optimum fluoride level in any given community depends on climatic conditions since air temperature primarily influences the amount of water ingested by children. In the Taylor County region the recommended fluoride concentration range is from a lower limit of 0.7 to an upper limit of 1.0 mg/l. About 30 percent of the water samples analyzed were between these limits, while nearly 60 percent exceeded the upper limit and slightly over 10 percent fell below the lower limit. The highest fluoride concentration found in the county was 8.4 mg/l in water from well 30-50-624. The cause for the higher fluoride concentration in this well is not known.

In some areas, water supplies containing fluoride levels outside the recommended range for the particular area have been successfully treated to bring them within recommended levels.

Serious and sometimes fatal poisoning has occurred as a result of infants drinking well water containing nitrate. In some instances adults drinking the same water were not affected; however, man and animal have been and can be poisoned by excessive concentrations of nitrate in drinking water. For these reasons the concentration of nitrate in water used for drinking purposes is recommended to be no higher than 45 mg/l. It would be advisable to refrain from feeding infants the milk from cows, goats, or the mother if their drinking-water supply contains nitrate concentrations exceeding this amount.

In localized areas, high nitrate concentrations in water from wells may be due to sewage from septic tanks or from animal waste in feedlots and barnyards. Dead animals in the wells can also account for temporary high nitrate concentrations in ground water.

Nitrate concentrations which appear to be abnormally high in waters over widespread areas may be

more difficult to explain. It has been suggested (Huberty, Pillsbury, and Sokoloff, 1945, p. 14-15) that in certain farming areas in California the high nitrate concentrations found in the ground water may be the result of the quick decomposition of organic matter and leaching of soluble salines to the ground water through heavy application of irrigation water to those previously mesquite-forested lands.

Nitrate content in the alluvium ground water analyzed ranged from less than 0.4 to 326 mg/l. The nitrate concentration in 54 percent of the water samples was less than the recommended limit for drinking water. Forty-six percent ranged from 45 to 210 mg/l, and one unused, dug well, 30-50-627, about 1 mile southeast of Tuscola, contained water with a nitrate concentration of 326 mg/l.

Sixty-five percent of the alluvium ground-water samples collected during this study came from wells along Jim Ned Creek and its tributaries, from northwest of Tuscola to east of Lawn. The remaining 35 percent were collected from wells scattered along Nubia, Mulberry,Little Elm, Elm, Cat Claw, Cedar, Lytle, and Bluff Creeks.

About 65 percent of the alluvium ground-water samples collected near Tuscola contained nitrate concentrations above 45 mg/l. Meager historical data in this area indicate that high nitrate in the ground water may be normal rather than the exception. The following list compares nitrate content of samples taken during this investigation and that of previous samples from the same wells:

		NITRATE CONTENT ANDDATE SAMPLED			
WELL_	PREVIOUS STUDIES	THIS STUDY			
30-50-121	72 mg/l (1939)	35 mg/l (1970)			
30-50-501	58 mg/l (1960)	37 mg/l (1970)			
30-50-505	114 mg/l (1946)	112 mg/l (1969)			
30-50-507	100 mg/l (1946)	57 mg/l (1970)			
30-50-601	117 mg/l (1960)	62 mg/l (1969)			

In each case an improvement as to nitrate content is shown; however, this meager historical record is insufficient to substantiate a general trend.

In an attempt to explain excessive nitrate concentrations in ground water in the general vicinity of Tuscola, a tabulation of the ground-water samples collected which had a nitrate concentration exceeding 45 mg/l was made. There appeared to be no general correlation which could be made consistently between the nitrate concentration of the sample and (1) the well use or yield corresponding to the sample, (2) the chloride content of the sample, (3) the location of the well from which the sample was taken with respect to a house, barnyard, or septic tank, (4) the distance and direction to Tuscola from the well, or (5) the use of the land surrounding the well. Well 30-50-205 is an example an apparent correlation between the high of concentration of nitrate found in the sample (100 mg/l) and the well location inside a livestock pen. The concentration of septic tanks used for sewage disposal in Tuscola is a possible source of some of the nitrate in the alluvium ground water in town and down gradient to the south, east, and southeast, but should not affect up gradient areas to the north. west, and northwest.

Of the samples collected in other areas, about 10 percent contained nitrate above the recommended limit for drinking water. Three of these samples came from wells located along Cedar Creek in the southeastern part of Abilene. Samples from a well on Bluff Creek west of Bradshaw, a well on Elm Creek about 2 miles north of Buffalo Gap, and a well on Elm Creek in north western Abilene also contained nitrate concentrations above the recommended 45 mg/l. The sample collected from a spring along Nubia Creek in western Taylor County contained 176 mg/l nitrate. A feed and livestock barn located up grade from the spring may be the nitrate source. The nitrate sources in most of the other locations were not determined.

Chloride concentrations ranged from 11 to 1,140 mg/l in the alluvium ground-water samples collected during this investigation. Average concentration from all samples was 275 mg/l. Slightly over 50 percent of the samples contained concentrations within the recommended 0 to 250 mg/l range. Fifteen samples contained chloride concentrations over 500 mg/l, and two of these contained more than 1,000 mg/l. Water samples from wells 30-35-403 and 30-50-301 had chloride concentrations of 1,050 and 1,140 mg/l, respectively. The sample from well 30-35-403 also contained 70 mg/l nitrate; a barn and livestock pen located a short distance up grade from the well is a possible source of organic contamination which could also account for some of the chloride in the water (Loehr, 1969, p. 203).

It is believed that some of the chloride contained in alluvium ground water was derived from oil-field brines through seepage from unlined surface disposal pits. These brines are characteristically very high in chloride. Likely some of the brine overflow from these pits also moved into the aquifer. Also, subsurface brines from improperly plugged oil tests and abandoned oil wells may have been the source for high chloride concentrations in the ground water in some areas.

Figure 23 shows a comparison of the ground water from apparently contaminated water wells with native-quality ground water in that particular area and a typical oil-field brine. Two of these wells that produce apparently contaminated water (30-27-706 and 30-50-227) are completed in the alluvium. Well 30-27-706 is within an area where brine disposal by injection wells was reported (Figure 22, area 10). There is oil production and several abandoned oil tests in the immediate vicinity of this well. Well 30-50-227 is adjacent to an area of reported brine disposal (Figure 22, area 30). There is also an abandoned oil test located up grade and approximately 1,000 feet from well 30-50-227.

Ground water in four of the five wells on which historical data are available in the Tuscola area showed an increase in chloride content during the comparison periods. The chloride increased from 106 mg/l in 1939 to 600 mg/l in 1970 in water from well 30-50-121 (see Table 7). The well is located inside area 30 of the reported brine disposal areas shown on Figure 22.

Some boron is necessary for plant growth. However, too high a concentration in ground water will render it useless for irrigation purposes. Waters with concentrations up to 1.0 mg/l may be used to irrigate boron-sensitive crops such as most fruit and some nut trees; a maximum content of 2.0 mg/l on semi-tolerant crops like most small grains, cotton, corn, potatoes, and some other vegetables; and concentrations up to 3.0 mg/l on tolerant crops such as alfalfa, date palm, asparagus, beets, onions, and most root vegetables.

A total of 31 samples of alluvium ground water collected during this study were analyzed for boron content. The concentrations found range from 0.2 to 1.6 mg/l. Nineteen of these samples were from wells located in the Tuscola and Lawn areas and were found to contain less than 1.0 mg/l boron. Three samples from wells located along Elm Creek in northern Abilene, and one sample from a well near Mulberry Creek south of Merkel, contained between 1.0 and 2.0 mg/l boron. One sample from a well on Cat Claw Creek and three samples from wells along Elm Creek, all located between Abilene and Buffalo Gap, contained less than 1.0 mg/l boron.

A system for determining the quality of irrigation waters based on the salinity hazard, as measured by the specific conductance, and the sodium (alkali) hazard, in terms of SAR, has been discussed previously in the section "General Chemical Quality of Ground Water". Using this system, the plots of 131 water samples collected from wells developed in the alluvium are shown on Figure 12. The majority of the waters are shown to have medium to very high salinity hazard (C_2 , C_3 , C_4) and the low to medium sodium or alkali hazard (S_1 , S_2). Limitations on use of irrigation waters of these classifications are shown on Table 3. In general terms, alluvium ground water used for irrigation in Taylor County should be restricted to soils with adequate permeability and drainage, preferably with a coarse texture. In cases involving use of the higher salinity hazard waters, careful salinity-control measures such as heavy pre-plant irrigation or deep plowing may be necessary. Plants selected should have moderate to high salt tolerance.

Percent sodium and sodium-adsorption ration (SAR) are terms used to indicate the degree to which irrigation water will tend to replace adsorbed calcium and magnesium in the soil with sodium. Continued irrigation with waters having high SAR values may damage the soil structure. In terms of percent sodium, this hazard is not likely to occur unless the percent sodium value is considerably higher than 50 (Hem, 1970, p. 229). According to the U.S. Department of Agriculture (U.S. Salinity Laboratory Staff, 1954, p. 72), the sodium-adsorption ratio is a better measure

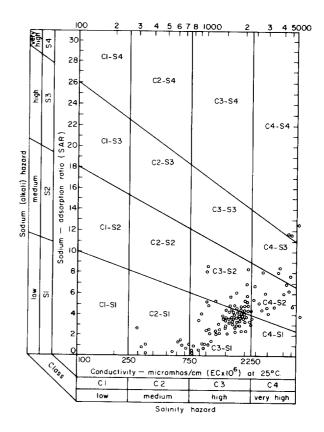


Figure 12.-Classification of Quaternary Alluvium Waters for Irrigation

of the suitability of irrigation water with respect to the sodium hazard. In 55 samples of alluvium ground water used for irrigation, the SAR ranged from 0.9 to 8.7 and averaged 4.1.

About 98 percent of the alluvium irrigation water samples collected were within the RSC (residual sodium carbonate) limit considered to be safe for irrigation (1.25 me/l or less). The samples from wells 30-34-304 and 307 on Elm Creek in northwest Abilene had RSC values of 7.50 and 5.87 me/l, respectively.

Hydraulic Properties of the Aquifer

In order to obtain some indication of the hydraulic properties of the alluvium aquifer, an aquifer pumping test was conducted December 14-15, 1970, on well 30-50-628, an irrigation well on the K. C. Roberson farm about 1 mile southeast of Tuscola. Alluvium saturated thickness at this site was 25 feet. From the pumping-test data the aquifer's coefficient of storage was calculated to be 0.035, and its coefficient of transmissibility 170,000 gpd/ft (gallons per day per foot).

Three test holes (30-50-651, 652, and 653) were drilled near the test well for use as observation wells during the aquifer test. The lithology encountered in these observation wells is described in Table 6. Formation samples were obtained from observation well 30-50-653 for analysis by the Texas Water Development Board's Materials Testing Laboratory in Austin. The measured porosity of the alluvium encountered in this well was about 34 percent; however, this figure is not necessarily representative of the average porosity of the alluvium regionally. The porosity of the alluvium will vary from one area to another due mainly to changes in formation lithology.

Specific capacity of the aquifer-test well, 30-50-628, was 170 gpm/ft (gallons per minute per foot of drawdown), and its average yield during the test was 389 gpm. Table 4 shows specific capacities and other information pertaining to well yields, for this and five additional irrigation wells completed in the alluvium.

The average transmissibility of 170,000 gpd/ft calculated from the aquifer test is considered to be reliable for only the area immediately surrounding the test well. Many more such tests would be needed to arrive at an average figure for the entire extent of the alluvium in the county.

Since the alluvium aquifer is under water-table conditions, the coefficient of storage, 0.035, is

approximately the same as the specific yield of that part of the aquifer dewatered during pumping.

Pumping of ground water from an aquifer such as the alluvium over extended periods can have widespread effects on water levels. When a well is pumped a cone of depression is formed in the water table surrounding the well. Continued pumping removes water from storage causing this cone of depression to expand until a source of replenishment equal to the pumping rate at the well is intercepted. If several closely spaced wells are pumping simultaneously from the same aquifer, their cones of depression will overlap causing additional lowering of water levels in the area (Figure 8). Some factors which determine the extent of the cone of depression are the transmissibility and storage coefficients of the aquifer, slope of the water table, recharge within the zone of influence of the well, the pumping rate, and the length of time the well is pumped.

Figure 13 portrays the theoretical effects on water levels, at various distances from a well, caused by pumping the well at a rate of 150 gpm continuously for periods of 1, 3, 10, and 30 days. The aquifer hydraulic characteristics shown in the figure are assumed for the alluvium along Jim Ned Creek and are based on data from the aquifer test conducted on well 30-50-628. The figure shows that the greatest amount of drawdown occurs during the early period of pumping, and that the pumping affects water levels at relatively large distances from the pumped well. It also gives an indication of proper spacing between wells for least interference.

History of Development

Use of ground water from wells and springs is reported as early as the 1880's in Taylor County. It is likely that the first wells came into existence soon after the arrival of the earliest settlers. Figure 14 shows graphically the estimated pumpage of ground water for industrial, irrigation, and public supply over a 16-year period from 1955 through 1970.

The earliest known irrigation with alluvium ground water was in the mid-1940's along Elm Creek southwest of Abilene. However, from a standpoint of the amount of ground water used, the main irrigation area is along Jim Ned Creek in the southeastern part of the county (Figure 25). Irrigation in this area began in the early 1950's. In general, irrigation pumpage has increased fairly steadily from the mid-1950's through 1970. Figure 14 illustrates this and shows that the 1970 pumpage was about five times that in the 1955-56 period. The above-average increase in pumpage in 1967 may have been due to below-average rainfall during part

Table 4.—Yields of Selected Irrigation Wells

WELL	TYPE PUMP	HORSE- POWER	WELL DEPTH (ft)	PUMPING DEPTH (ft)	AQUIFER	PUMPING RATE (gpm)	SPECIFIC CAPACITY (gpm/ft)	DISTRI- BUTION SYSTEM
XW-29-40-315	Submersible	3	100	73.4	Pc	51	0.9	Closed
XW-29-40-601	do	2	110	26.5	Pc	41	3.2	Do.
XW-29-40-605	do	3	108	20.8	Pc	53	6.8	Do.
XW-30-25-716	do	3	69	21.2	Qs, Pc	41	2.6	Do.
XW-30-42-201	Centrifugal	4	44	21.5	Qal	46	17.7	Do.
XW-30-42-203	Submersible	3	45	37.4	Qal	51	9.4	Do.
XW-30-42-501	Turbine	10	42	-	Qal	193		Do.
XW-30-50-508	Centrifugal	5	24	14.5	Qal	51	5.7	Do.
XW-30-50-511	do	7.5	26	18.4	Qal	86	8.4	Do.
XW-30-50-602	do	1	24	-	Qal	61	-	Open
XW-30-50-603	do	7.5	30	14.5	Qal	256	45.7	Do.
XW-30-50-628	do	10	36	12.3	Qal	580	170.0	Do.
XW-30-50-633	do	1.5	23	-	Qal	127	-	Do.

¹ Aquifers: Qal, Quaternary alluvium; Qs, Seymour Formation; Pc, Choza Formation.

of the growing season (July and August). The estimated total pumpage for irrigation purposes during the period 1955-70 was 18,500 acre-feet. Development of the alluvium has continued along Jim Ned Creek. Several new irrigation wells are known to have been drilled in the first part of 1971. Also some development along Elm Creek occurred during 1971. Ninety-eight alluvium wells used for irrigation were inventoried during this study.

A total of nine public-supply wells completed in the alluvium were inventoried during this investigation (Table 5 and Figure 25). Five of the wells as of 1971 are in use in the communities of Tuscola, Buffalo Gap, and Ovalo while the remainder have been converted to other uses or abandoned. Earliest known public-supply wells in the county were completed in the 1920's; however, it is probable that wells were also used for public supply prior to this time. The estimated pumpage for public supply, over the period 1955-70, is 1,400 acre-feet. Figure 14 shows that the pumpage rate has been fairly constant over the entire period. The last alluvium wells known to have been drilled for public supply were completed in the early 1960's.

During the course of this study 25 wells used for industrial purposes were inventoried. Four of these were completed in the alluvium. Two of the four wells provide insignificant amounts of water while two others are used in a gas-plant operation west of Tuscola. The estimated total amount of alluvium ground water pumped for industrial use from 1955 through 1970 is 120 acre-feet. Pumpage during the 1955-57 period was greater than in more recent times, but a steady increase has occurred since 1966.

It is very probable that alluvium ground water has been used for domestic and livestock purposes since shortly after the first settlers arrived in the county. Some wells are reported to have been in continuous use since the mid-1880's. It is estimated that about 1,800 acre-feet of ground water was used for domestic and livestock supplies during 1970. Of this figure, an estimated 1,100 acre-feet was used for livestock purposes which is an increase of slightly under 200 acre-feet above the 1969 estimate. Domestic use of ground water has declined for the past decade due primarily to an increase in availability of surface water.

Changes in Water Levels

Figure 15 shows the water-level fluctuations of eight selected wells in the county from October 1969 to January 1971. In general, it portrays water levels beginning to decline in early summer, reaching a low point, and remaining steady into winter.

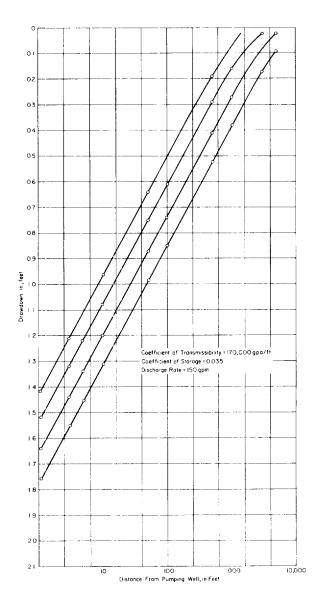


Figure 13.–Diagram Showing Relation of Decline in Water Levels to Time and Distance as a Result of Pumping From the Alluvium Along Jim Ned Creek

The decline of the water levels during the summer and early fall months (May-September) is considered normal because maximum use of the ground water occurs during this time. The low water levels shown in the mid-fall to mid-winter months (October 1970 to January 1971) are believed to be a result of below-average rainfall during the last half of 1970 (Figure 15) as well as pumpage of ground water during the summer months for irrigation purposes. If normal rainfall had occurred in the fall months, it is believed that the water levels would have begun a slow steady rise. Wells 30-50-118, 510, 606, 631, and 30-51-706 are completed in the alluvium. All except well 706 are in an area where the primary use of the ground water is for irrigation. Well 706 reflects the least water-level fluctuation of 1.99 feet over the period, while well 606 shows the greatest change of 6.10 feet.

Forty-six alluvium wells with previous water-level data were inventoried during this study (Table 5). About 80 percent of these are located along Jim Ned Creek. Considering the type of data collected (reported or measured water levels) as well as time of year the data were collected, a net rise in water levels in the alluvium along Jim Ned Creek is indicated over the historical period.

Well Construction

The first alluvium wells developed in Taylor County were hand dug. This method has been used in recent time also, but most wells are drilled. Well depths vary from 12 to 60 feet with a majority of the wells ranging from 20 to 30 feet deep.

Dug wells were usually lined with stone, brick, or concrete rings. These wells vary from two to several feet in diameter. Most of the dug wells penetrated only a few feet of the alluvium.

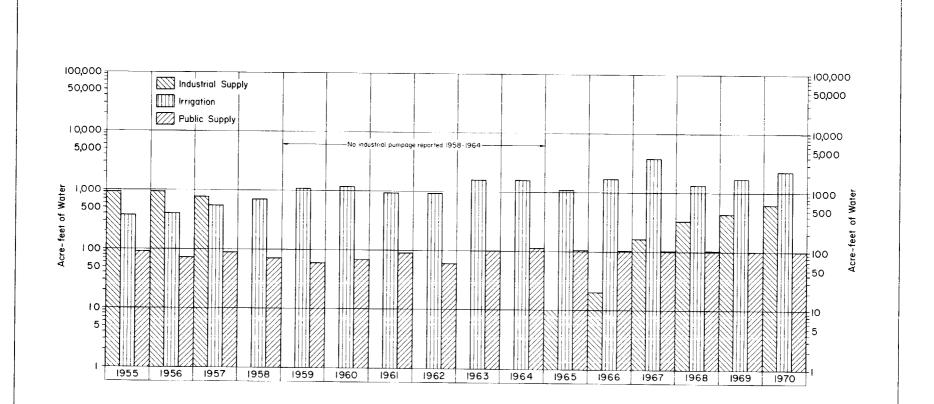
The drilled wells usually penetrate the entire water-bearing zone. Casing sizes range from 4 to 24 inches in diameter. Plastic or steel pipe has been used to case the bore hole. The steel pipe varies from heavy gauge oil-well casing to light gauge sheet-metal. In general, the casing is slotted or perforated opposite part of all of the water-bearing zone. In most cases, the drilled wells developed for irrigation or industrial purposes are of a larger diameter than those for domestic use. The drilled holes are usually reamed to larger diameters, casing is set on bottom with perforation or slots opposite the water-bearing zone, and the annular space is gravel packed.

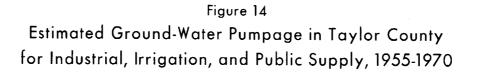
In the Tuscola area, it is common practice to construct a cellar lined with brick or concrete into which the pump is placed in order to reduce lift height.

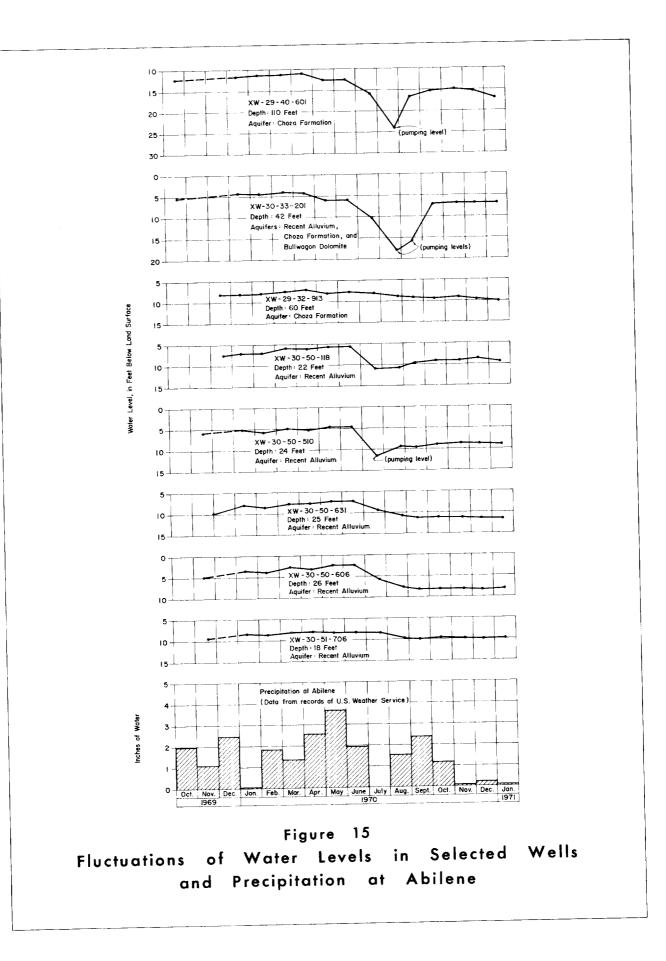
Availability of Ground Water for Future Development

In general, from the data collected during this study it appears that small amounts of ground water from the alluvium are available for additional development for irrigation use in Taylor County. Data collected are insufficent to determine exact amounts.

The alluvium along Jim Ned Creek from northwest of Tuscola to east of Lawn is estimated to contain about







4,400 acre-feet of ground water in storage. This is based on the aquifer having an areal extent of 19 to 20 square miles, an average saturated thickness of 10 feet, and a coefficient of storage of 0.035. Average annual recharge to the aquifer from rainfall is estimated to be slightly over 1,500 acre-feet. Irrigation pumpage from the aquifer is estimated to have been slightly less than 1,500 acre-feet during 1970, a drier than average year during which the alluvium water levels generally showed only small net declines. Although the data cannot be considered conclusive, they indicate the possibility that a small amount of ground water may be available in the area for additional irrigation development. In one area along East Jim Ned Creek the quality of the alluvium ground water had deteriorated to the point where the landowner no longer used the water for irrigation.

It was reported that along Elm Creek north of Buffalo Gap, wells cannot be pumped for too long a period without lowering the water levels severely. This indicates poor transmissibility or a small aquifer extent or probably both conditions in this case, and limits the water available for irrigation in this particular area.

Additional ground water for domestic and livestock use is probably available along many of the other major drainage tributaries in the county, but to what extent is not known.

Antlers Formation

The Antlers Formation is considered to be the second most important aquifer in the county due to its large areal extent and apparent reliability as a source for usable quality water. The ranching industry in south Taylor County depends on it to a great extent as a source for livestock water supply. It is also used to a lesser degree in this area for domestic purposes.

Extent of the Aquifer

Cretaceous rocks of the Fredericksburg Group and Antlers Formation are located for the most part in the southern half of the county (Figure 5 and Table 1). Erosion has separated these rocks into two areas, those east of U.S. Highway 83-84 and those to the west of Buffalo Gap and Tuscola. The Cretaceous rocks to the west of Buffalo Gap and Tuscola are a part of a large erosional remnant, or outlier, of Cretaceous rocks which extends from Taylor County across Nolan County and then south into Coke County. Those Cretaceous rocks east of U.S. Highway 83-84 are a part of a much smaller outlier of Cretaceous which extends from Taylor County into western Callahan County. Prior to extensive erosion requiring vast amounts of time, these outliers were once part of a system of Cretaceous rocks which covered all of these counties and the entire area to the south and east to the Llano Uplift. The areas of Cretaceous rocks in Taylor County cover approximately 275 square miles or about 30 percent of the surface area of the county. About 220 square miles of this total is located in the area to the west of Buffalo Gap and Tuscola. Other small outliers of these rocks occur near the main areas as shown on the geologic map (Figure 5).

Surface exposures of the Antlers Formation are shown in Figures 16 and 17. Lithology of the Antlers and the other Cretaceous rocks and their general water-bearing properties are given in Table 1. The Antlers Formation is believed to attain a maximum thickness of about 200 feet in the county.

A total of 94 wells believed to be completed in the Antlers were inventoried during this study.

Source, Recharge, and Occurrence of Ground Water

The source of the ground water and recharge to the aquifer is precipitation falling on the Cretaceous rocks. In some areas, small dams have been constructed across drainage ditches to capture runoff waters thereby providing additional recharge.



Figure 16.—Antlers Formation (Ka) in Unconformable Contact with Permian Rocks of the Clear Fork Group (Plcf), North of Lake Abilene, Central Taylor County



Figure 17.–Cross-bedding in the Antlers Formation, in-Road-cut along Farm Road 89 West of U.S. Highway 277, Southwest Taylor County

Usable amounts of ground water occur over most of the two larger areas of the Cretaceous. However, reports of dry tests drilled in the western part of the county may indicate that in some areas the porosity and permeability of the Cretaceous sequence are not adequate to yield ground water.

Movement and Discharge of Ground Water

Figure 18 is a map which shows the approximate water-level surface in the Cretaceous rocks in 1969-70. Each of the contour lines represents points of equal elevation of the water-level surface (water table) above sea level. The relationship of ground water contained in the Fredericksburg Group with that in the underlying Antlers Formation was not determined in this study. The control points used for construction of Figure 18 include some data from 27 springs that flow from the Fredericksburg Group, as well as data from numerous water wells, and two springs, that produce primarily from the Antlers Formation. The map shows the water table at its highest elevations in the western part of the county on either side of Elm Creek. In the area east of U.S. Highway 83-84, the water table is highest in the area about 8 miles east and 1 mile north of Tuscola. Since well control used for construction of the map was sparse, water-table conditions in many areas may differ from that portrayed on the map. It should also be pointed out that the higher water-table areas shown north and south of Elm Creek and west of U.S. Highway 277 may be a reflection of a perched water

table. Additional data are needed here to determine if this condition exists.

The ground water in the Cretaceous rocks is considered to be under water-table conditions in Taylor County. The movement of the ground water is outward from the central parts of the outliers and at right angles to the contour lines on Figure 18. Unless interrupted by areas of pumpage, the ground water continues its movement from the central areas of these outliers to points of natural discharge such as streams and springs or seeps.

Some natural discharge from the Antlers undoubtedly is lost to the Permian rocks upon which it rests. The alluvium along Elm Creek was observed receiving water that discharged from the Antlers Formation in an area near the point where U.S. Highway 277 crosses Elm Creek. How much of the Antlers discharge water enters these aquifers is not known. The many wells located over the two principal areas of Cretaceous rocks constitute many points of artificial discharge.

Chemical Quality

With the exceptions of excessive hardness and a deficiency of fluoride, the general chemical quality of Antlers ground water is good. Its low mineralization is to be expected since the source waters (precipitation) are usually low in chemical content and the distance traveled by these waters to reach the water table is short. Percolation of some of the waters through sediments high in calcium carbonate (limestone of the overlying Fredericksburg Group) accounts for hardness of the waters.

Samples were collected for chemical analyses from 51 wells and springs thought to produce ground water from the Antlers Formation. The results of these analyses are listed in Table 7.

The ranges in concentration of the principal chemical constituents are:

Calcium	58	to 185	i mg/l
Magnesium	6	to 45	i m g /l
Sodium plus potassium	6	to 77	mg/l
Bicarbonate 2	60	to 472	mg/l
Sulfate	6	to 216	i mg/l
Chloride	4	to 96	i mg/l
Fluoride	0.2	?to 2	.4 mg/i
Nitrate	0.4	to 143	mg/l

All samples of ground water collected from wells developed in the Antlers contained less than 1,000 mg/l dissolved solids and, therefore, are classed as fresh water (Winslow and Kisler, 1956, p. 5). The concentration of dissolved solids ranged from 270 to 750 mg/l with only 16 percent of the samples containing more than the 500 mg/l limit recommended by the U.S. Public Health Service (1962) for use on public conveyances.

All ground-water samples contained total hardness above 180 mg/l, which classifies them as very hard. This is not unexpected as most of the water entering the Antlers Formation first percolated through rocks of the Fredericksburg Group which consist predominately of limestone (see Table 2). The water samples ranged in hardness from 230 to 510 mg/l and averaged about 336 mg/l. The variation in total hardness did not appear to follow any discernible pattern.

The sulfate content of the ground water averages about 44 mg/l, well within the 250 mg/l limit recommended by the U.S. Public Health Service. Again, this is not considered unusual as the ground water has not moved through rocks containing a source for this constituent.

About 17 percent of the Antlers ground-water samples analyzed contained fluoride in the recommended range of 0.7 to 1 mg/l. Thirteen percent contained more than the maximum limit while the majority or 70 percent fell below the minimum limit. Fluoride concentrations of all samples average about 0.6 mg/l.

Six percent of all ground-water samples collected from the Antlers contained nitrate over the recommended 45 mg/l limit. Wells 30-51-201 and 601 contain 143 mg/l and 112 mg/l, respectively. Both wells are downgrade from livestock pens which may account for some of the excess nitrate. The only other well having over 45 mg/l nitrate is 29-56-502 with 78 mg/l. Causes for the slightly higher nitrate concentration in this well are unknown. The average nitrate content in all samples was about 14 mg/l.

The ground water from all wells sampled had chloride concentrations well below the 250 mg/l limit recommended. The average of all samples is near 29 mg/l.

Only eight water samples from the Antlers were analyzed for boron content. Seven samples contained 0.1 mg/l, and one had a content of 0.2 mg/l boron. Based on this sparse sampling, these waters appear to be suitable for irrigation on crops which are sensitive as well as those which are semi-tolerant to boron. The RSC values are well below the maximum limit considered safe for irrigation purposes (1.25 me/l). This is also true of the percent sodium values.

Since ground water from the Fredericksburg Group is similar in chemical content to that from the Antlers, both were plotted on one diagram for classification of irrigation waters (Figure 19). The plots for all 81 water samples reveal a range of salinity hazard from medium to high (C_2, C_3) and a low sodium hazard (S_1) . Table 3 indicates the limitation of waters in these classifications for irrigation use.

Generally, these waters should be used on only those soils with good drainage, salinity control should be maintained, and crops selected should have at least moderate salt tolerance. SAR values on the Antlers ground-water samples ranged from 0.1 to 5.2.

Hydraulic Properties of the Aquifer

The largest reported yield of wells developed in the Antlers Formation is 70 gpm (well 29-48-804).

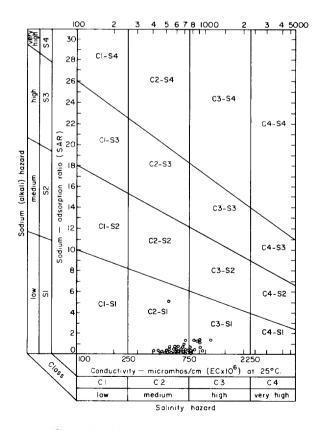


Figure 19.–Classification of Waters From the Cretaceous Rocks for Irrigation

History of Development

There are only six irrigation wells known in the county which are pumping ground water wholly or partly from the Antlers Formation. Two of these wells (29-48-801 and 803) are thought to be completed in both the Antlers and the alluvium. The ground water in the alluvium in these two wells is undoubtedly derived by discharge from the Antlers Formation. All of these wells are located along Elm Creek about 4-1/2 miles west of the intersection of U.S. Highway 277 and Farm Road 89 (Figure 25).

Water from 72 percent of the non-irrigation Antlers wells inventoried is used primarily for watering livestock. The earliest reported well completion in the Antlers Formation was 1887. This well, 30-51-501, is still in use and is located about 5 miles due east of Tuscola.

Changes in Water Levels

Water levels in wells thought to be completed in the Antlers Formation were measured mostly during the late fall and winter of 1969-70. These data, along with some control points obtained from springs flowing from Fredericksburg Group rocks, were used in construction of a water-level map (Figure 18). Water levels were again measured in as many of these wells as possible about 1 year later (Table 5). Declines in water levels which averaged almost 2 feet were noted in one-third of the wells. The range in decline was from 0.1 to 5.1 feet. The water level in one well remained constant, while rises averaging slightly over 3 feet occurred in 24 wells. The rises in water levels ranged from 0.1 to 14.0 feet.

The fluctuations in water levels occurred in both main areas of the Cretaceous rocks with no apparent pattern. Use of the ground water in both areas probably remains fairly constant from year to year so that above-average rainfall in any calendar year, such as occurred in Taylor County during 1969, might account for a general rise in water levels.

Well Construction

Wells inventoried that were developed in the Antlers Formation range in depth from 15 to 335 feet. Casing diameter is usually not over 8 inches. A common practice used in the deeper wells drilled prior to the 1940's was to set one 20- to 30-foot joint of thin gauge metal casing in the upper part of the hole, leaving the remainder of the hole uncased. This was usually done where the upper part of the hole consisted of limestones of the Fredericksburg Group. In wells drilled later, heavy steel casing was set on the bottom and slotted opposite the water-bearing zone.

In shallower wells, both types of steel as well as plastic casing are used. The diameter of casing seldom exceeds 12 inches. Generally, the casing is set on bottom and slotted or perforated opposite the water-bearing sandstone.

Availability of Ground Water for Future Development

Based on scanty hydrologic as well as geologic knowledge concerning the Antlers Formation, it is believed that additional ground water is available for development, so long as withdrawals are restricted to small amounts such as that from domestic or livestock wells.

Choza Formation

The Choza Formation produces ground-water yields sufficient for a limited amount of irrigation in the northwest quarter of the county around the town of Merkel (Figure 25 and Table 5).

It was reported that some wells used for public supply in Merkel pumped mud during the drought of the early 1950's. This indicates that the Choza is not dependable for continued heavy withdrawals during periods of drought.

General water-bearing characteristics and lithology of the formation are shown on Table 1. Sixty-three wells thought to produce entirely from the Choza were inventoried during this study.

Extent of the Aquifer

The Choza Formation is believed to form slightly less than 50 percent of the land surface in the western half of the county. It is exposed in a belt about 7 to 10 miles wide from the Taylor-Jones County line south to the Cretaceous plateau area. Merkel is in the north-central part of the outcrop. Choza rocks crop out again south of the Cretaceous plateau in an area 2 to 3 miles north of the Taylor-Runnels County line and east of U.S. Highway 277.

The regional dip of these Permian beds is to the west-northwest at less then one-half degree per mile. The principal fresh water-bearing zones are believed to occur in the basal 200 feet (Figures 27 and 28).

Source, Recharge, and Occurrence of Ground Water

Precipitation on the outcrop is the major source of ground water for the Choza. Discharge from the overlying Antlers Formation is probably an important source of recharge as the Antlers is in direct contact with the Choza over perhaps a 100 to 120 square mile area. Locally, ground-water discharge from the alluvium is also a probable source.

Ground water occurs in solution channels and fractures of the dolomitic limestones, and also in sandstone lenses, in the lower part of the formation. The ground water in the Choza is indicated to be under artesian conditions at some well sites and water-table conditions at others, as the static water levels in wells were encountered both considerably above and also very near the depth at which the ground water was first encountered.

Movement and Discharge of Ground Water

The direction of movement of the water is down gradient to areas of natural or artificial discharge. Natural discharge was observed at a small spring in a ravine near Mulberry Creek about 5-1/2 miles south of Merkel (Figure 25). The landowner reported this spring as being a reliable source of water.

Chemical Quality

Samples were collected for chemical analysis from thirty-one wells and the one spring. The results are tabulated in Table 7. Figure 9 also shows concentrations of some of the more predominate chemical constituents in samples from some selected wells of this area. The water from the Choza, generally, is very hard and its use for industrial purposes should not include laundering or use in boilers unless treated.

The ranges in concentration of the principal chemical constituents are:

Calcium 29	9 to	610	mg/I
Magnesium 14	4 to	383	mg/l
Sodium plus potassium 22	2 to	690	mg/l
Bicarbonate 2:	2 to	580	mg/l
Sulfate	4 to	2,600	mg/l
Chloride 18	8 to	1,740	mg/l
Fluoride	0 .6 to	3.0	l mg/l
Nitrate	0.4 to	212	mg/I

The range of dissolved solids is from 325 to 5,100 mg/l. Fifty percent of the ground-water samples analyzed are classified as fresh, 41 percent slightly saline, and 9 percent (3 samples) moderately saline. Only 6 percent of the analyzed waters would be suitable for use on a public conveyance (less than 500 mg/l). The average dissolved-solids concentration of all samples is 1,510 mg/l.

Historical water-quality data were available for two wells (29-40-501 and 502). The dissolved-solids content in a sample taken in 1939 and one during this investigation in 1970 from well 29-40-501 was 511 and 5,100 mg/l, respectively. This major increase in salinity indicates probable contamination. A sample collected in 1939 from well 29-40-502, and one taken during this investigation showed dissolved solids of 4,401 and 4,490 mg/l, respectively.

The hardness of the water samples ranged from 131 to 3,060 mg/l. With the exception of one sample collected from well 29-40-307, the water is classified as very hard (above 180 mg/l). Some of the hardness of the ground water may be due to leaching of calcium from limestone beds in the Choza by waters percolating through them. Another probable source is the recharge water that drains from the Cretaceous rocks.

Water samples from the Choza generally contain high sulfate concentrations. The average for all samples is 576 mg/l. One source for the sulfate is anhydrite or gypsum present in the formation. A little less than 50 percent of the samples contained sulfate above the recommended 250 mg/l limit. Slightly over one-half of these had sulfate content above 1,000 mg/l. Waters containing the higher amounts of sulfate could have a laxative effect on, and probably would have an undesirable taste to those not accustomed to drinking them.

Nitrate content of these water samples averaged 56 mg/l. Slightly over one-half the samples contained nitrate concentrations within the recommended 45 mg/l limit. Five wells contained water with nitrate concentrations ranging from 122 to 212 mg/l; however, the cause is not known for this high nitrate.

The chloride content for the wells sampled averaged 266 mg/l. Twenty-eight percent of the wells contained above the recommended 250 mg/l limit; the range in these wells was from 252 to 1,740 mg/l. Historical data on one well, 29-40-501, show a chloride increase from 18 mg/l in 1939 to 1,740 mg/l in 1970. Also, by comparing the other chemical constituents from both analyses shown in Table 7, it is apparent that the water has been altered. Other wells with chloride content considerably above the overall average of the samples are 29-40-201 (407 mg/l), 205 (650 mg/l), 502 (437 mg/l), 503 (760 mg/l), and 30-57-301 (690 mg/l). In each case the sodium and sulfate concentrations also appear above normal, as does the calcium except in well 30-57-301. From available data there does not appear to be an explanation for these higher concentrations.

Approximately 50 percent of the samples collected from wells completed in the Choza contained concentrations of fluoride which were within the recommended range for this area. The fluoride concentration is below the minimum limit (0.7 mg/l) in about 6 percent of the waters while the remaining 44 percent contain fluoride in excess of the maximum recommended limit (1.0 mg/l).

The boron content was analyzed in slightly under 40 percent of the ground-water samples from the Choza. About 58 percent of these samples contained boron concentrations up to 1.0 mg/l, and these waters could be used to irrigate boron-sensitive crops. The boron content ranged from 1.0 to 2.0 mg/l in the samples from wells 29-32-907, 29-40-503, and 605. These waters should be applied only on crops that are semi-tolerant to boron. One sample contained 2.2 mg/l boron (well 29-40-201). Application of this water for irrigation should be restricted to crops with a high tolerance for boron. The sample from well 29-40-502 contained 5.7 mg/l boron which renders the water unsuitable for irrigation.

Figure 20 shows the plots of sodium and salinity hazards for all samples collected from the Choza Formation plus the plots for three water samples from the Bullwagon Dolomite Member of the Vale Formation. These were plotted together because the Bullwagon Dolomite and the Choza Formation contribute some of the ground water used for irrigation near Merkel. The diagram reveals that these waters generally have a high to very high salinity hazard (C_3, C_4) and a low to medium sodium hazard (S_1, S_2) . Table 3 shows that these waters should be limited to soils with good drainage, preferably coarse texture, and good permeability. Salinity control may be necessary and only crops with moderate to high salt tolerance should be used. SAR values range from 1.2 to 7.9 and the percent sodium from 16.5 to 58.4. With the exception of well 29-40-307, all waters sampled contain RSC values under 1.25 me/l which apparently makes them safe for irrigation use.

Hydraulic Properties of the Aquifer

Power yield tests were conducted on three wells completed in the Choza Formation and one thought to be producing water from the Choza and the Seymour

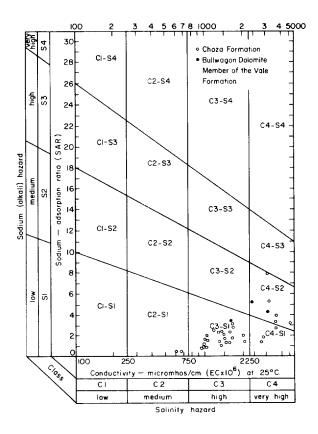


Figure 20.-Classification of Clear Fork Group Waters for Irrigation

Formation. Information derived from these tests is summarized in Table 4. Comparison of the measured pumping rates and specific capacities of these wells with those completed in the alluvium (same table) shows that some pumping rates are similar but, for the most part, the specific capacities of the Choza wells are lower.

History of Development

Of twenty-seven wells presently used for irrigation and yielding ground water exclusively from the Choza or in combination with other formations, one was drilled prior to 1950; eight were drilled between 1950 and 1960; sixteen were drilled after 1960; and two had unknown completion dates. Irrigation with ground water from the Choza probably began about 1950.

For the period 1955 through 1970, total irrigation pumpage from the Choza is estimated to have been about 3,300 acre-feet. Over this period an increase in annual pumpage is believed to have occurred at a fairly steady rate. The estimated pumpage during 1970 (560 acre-feet) was about seven times that during 1955 (80 acre-feet). Only two wells, 29-32-708 and 709, are known to be using water exclusively from the Choza for industrial purposes. Water from these wells is used in a feedlot operation and is estimated to be less than 5 percent of the total water used for this purpose. The wells were drilled in 1967. Well 29-40-501, unused at present, was dug in 1929 and used for an unknown length of time to supply water for a cotton gin in the community of Blair.

The town of Merkel has used surface water since 1955: however, prior to that time it depended on ground water from a number of wells developed in the Choza Formation. Fifteen of these wells were inventoried during this study (Five are presently privately owned). The cldest reported completion was in 1909. It was reported that during the drought of the early 1950's some of these wells pumped mud.

The earliest reported completion of a Choza well used for domestic or stock use was 1916.

Changes in Water Levels

Historical data show that water levels in wells 29-40-501 and 502 were lower in 1939 than in 1970 (Table 5). Both wells were in use during 1939 but are presently unused. These data are not considered sufficient, however, to indicate a significant change in water levels in the Choza Formation.

Well Construction

Most of the casing in wells completed in the Choza Formation is 8-inch diameter or smaller. A few irrigation wells are cased with 10- or 12-inch casing of heavy gauge steel. Scattered hand-dug wells range from 2-1/2 feet to as much as 15 feet in diameter. Casing for the dug wells is made of rock, cement, brick, or combinations of these. In the smaller diameter holes, usually the casing is set through the water-bearing zone and slotted opposite the interval or intervals yielding water. The deeper wells range to about 120 feet.

Availability of Ground Water for Future Development

Limited available data suggest that ground water in small amounts should be available for development from the Choza. The area most suitable for development probably is north of Merkel.

From estimated pumpage data, it appears that 500 to 1,000 acre-feet of ground water could be pumped

annually from the Choza in the Merkel area except in periods of prolonged drought.

San Angelo Formation

In Taylor County, the San Angelo Formation is probably as good an aquifer as the Choza Formation. Based on a reported withdrawal for 1970 of 500 acre-feet, water in the San Angelo appears adequate for limited industrial use. A feedlot operation which first began use of ground water in 1967 has steadily increased annual pumpage rates. Although the section thought to be water-bearing in the Choza Formation appears thicker than that of the San Angelo, reported information indicates that individual water producing zones are thicker in the San Angelo.

The San Angelo Formation exposed in Taylor County is predominately sandstone (Table 1). Recharge to the aquifer is likely at a faster rate than that of the Choza because of its probable ability to capture more precipitation and runoff per unit area of exposure.

Forty-seven wells believed to yield ground water exclusively from the San Angelo Formation were inventoried during this investigation.

Extent of the Aquifer

The San Angelo Formation occurs in a thin belt extending along and on either side of the Taylor-Nolan County line for almost the entire length of Taylor County (Figure 5). The outcrop area varies from about 2 to 5 miles in width. Of its estimated 90-square-mile occurrence within the county, about 30 percent is overlain by Cretaceous beds.

The estimated maximum thickness of the San Angelo Formation in the county is 200 feet; its water-bearing and lithologic characteristics are listed in Table 1.

Source, Recharge, and Occurrence of Ground Water

The major source of recharge to the San Angelo Formation is precipitation on the outcrop area. However, water from the Antlers Formation should contribute an appreciable amount of recharge where the two are in hydraulic contact.

The ground water in the San Angelo is reported to occur in one or more thin zones within the formation

which range in depth from 15 to over 100 feet. Most of the shallow wells inventoried were near the updip limit of the formation. The extent of fresh to slightly saline water-bearing zones of the San Angelo Formation is not known; however, wells developed in the San Angelo in southeast Nolan County are several miles downdip from the outcrop. Ground water in the San Angelo Formation occurs under artesian conditions downdip from the outcrop and under water-table conditions along the outcrop.

Movement and Discharge of Ground Water

Little is known of ground-water movement in the San Angelo. It is assumed to move down gradient toward points of discharge.

As far as is known, discharge from the San Angelo in Taylor County is through well withdrawals (artificial discharge). At one location on Valley Creek, west of the Shep community, water was repeatedly observed standing on San Angelo Sandstone which outcrops in the creek bed in this area. This water is believed to be rejected recharge, and probably was discharged from Cretaceous rocks.

Chemical Quality

The chemical analyses of 18 water samples collected from wells completed in the San Angelo Formation during this investigation are listed in Table 7. Figure 9 shows concentrations of some of the chemical constituents in water from selected wells located on the San Angelo outcrop. If the samples collected are representative, then these waters may be classified, generally, as fresh to slightly saline and very hard. Their use for industrial purposes should not include laundering or any process using boilers unless the water is treated.

The ranges in concentration of the principal chemical constituents of ground water from the San Angelo are as follows:

Calcium	59	to	460	mg/ł
Magnesium	17	to	340	mg/l
Sodium plus potassium	45	to	890	mg/l
Bicarbonate	288	to	540	mg/l
Sulfate	33	to 2	,180	mg/l
Chloride	10	to 1	,270	mg/l
Fluoride	0.6	to	8.2	mg/l
Nitrate <	0.4	to	252	mg/l

The content of dissolved solids ranges from 402 to 5,400 mg/l, and the average of all samples collected is 1,539 mg/l. Sixty-one percent of the ground-water samples are classified as fresh, 22 percent as slightly saline, and the remaining 17 percent as moderately saline. Only about 5 percent of the waters sampled would be acceptable for use on a public conveyance (less than 500 mg/l dissolved solids). Comparison of 1969 analyses with analyses performed in 1939 for four wells, 29-55-902, 29-56-702, 703, and 704, shows a considerable decrease in dissolved-solids content in wells 29-55-902 and 56-704 of 293 and 589 mg/l, respectively, and a slight increase in the other two wells.

The total hardness of all water samples ranged from 276 to 2,550 mg/l and averaged 773 mg/l. The calcium and magnesium in San Angelo sediments, plus hardness of water that discharges from the Cretaceous rocks in areas where those rocks are in contact with the San Angelo, in combination likely cause hardness of the San Angelo ground water. Again, comparison of the 1969 analyses with those performed 30 years earlier shows that the hardness of water from wells 29-55-902 and 29-56-704 decreased significantly by 200 mg/l and 157 mg/l, respectively, while that in well 29-56-703 increased by 110 mg/l and in 29-56-702 increased by only 13 mg/l. Changes in the calcium plus magnesium content followed the same pattern in these wells as the changes in dissolved-solids content and hardness.

The sulfate content of samples collected from the San Angelo Formation for analysis averaged 499 mg/l, almost 80 mg/l below the average for the Choza. Gypsum within the formation is a source of the sulfate. Approximately 61 percent of the water samples contained less than the recommended 250 mg/l limit. Of the samples with sulfate content above this limit, about 38 percent contained more than 1,000 mg/l. Taste and laxative effects are the principal reactions which may occur when consuming waters that contain excessive sulfate. Historical data from the previously mentioned four wells indicate a slight decrease in sulfate content since 1939.

Sixty-eight percent of the water samples analyzed contained concentrations of nitrate below the recommended 45 mg/l limit, and 26 percent ranged from 46 to 19 mg/l. Water from one well (29-56-701) contained 252 mg/l nitrate and, based on information in Table 2 and other sources, the water should be not be used for human or livestock consumption. A 1939 analysis of water from a well now destroyed, which was located just 40 feet northeast of the above well, shows a nitrate concentration less than 20 mg/l. This indicates possible nitrate contamination in at least the immediate area of the well, but the source of the contaminant is not known.

The average nitrate concentration from all samples is 43.3 mg/l. It is of interest to note that historical information on well 29-56-704 shows that the nitrate content from a sample taken in 1939 was 765 mg/l; and the nitrate concentration in the sample taken in 1969 was 13 mg/l. This improvement in nitrate content is opposite to the general trend of quality deterioration.

The average chloride concentration of all water samples is 296 mg/l. Fifty-six percent of the samples contained less than the maximum recommended 250 mg/l. The remaining 44 percent ranged from 264 to 1,270 mg/l and averaged slightly over 500 mg/l. Water from one well (29-32-721) which contained 1,270 mg/l chloride and 890 mg/l sodium may have been contaminated by oil-field brine. Brine disposal was reported in this immediate area (Figure 22, area 1), and oil wells surround the water well.

Only about 17 percent of the samples analyzed contained fluoride concentrations within the desired 0.7 to 1.0 mg/l range. About 67 percent contained more than the maximum limit recommended while the remaining 16 percent were below the minimum.

Samples were collected from seven wells for analysis of boron content. Water from only one well contains more boron than is considered safe for irrigation of boron sensitive crops. Water from all seven wells could safely be applied to crops that are semi-tolerant to boron.

Figure 21 indicates that most of the water is classed as high in salinity hazard and low in sodium hazard. Limitations on the irrigation use of waters in these classifications are listed in Table 3. Generally, application of these waters should be restricted to soils with good drainage and permeability and to crops with a high tolerance for salt. SAR values range from 1.2 to 7.7 and percent sodium from 25.7 to 50.7. All RSC values are under the 1.25 me/I limit for waters considered as safe for irrigation.

Hydraulic Properties of the Aquifer

Reported yields of the industrial wells used in a feedlot operation northeast of the town of Trent range from 40 to 180 gpm. The reported yields of domestic and stock wells range from 6 to 20 gpm.

History of Development

Ground water from the San Angelo Formation has been in use for many years (Table 5). The oldest well inventoried for domestic use was drilled in 1913. Seventeen industrial wells believed to produce ground water from the San Angelo were inventoried. One well (29-40-101) is used only occasionally. The other 16 were in operation during the time of inventory on the Cal-Tex Feed Yard approximately 2 miles northeast of Trent. Use of ground water at this feedlot began in 1967. The operator estimated yearly pumpage in acre-feet from 1967 through 1970 as: 134, 283, 279, and 504, respectively, for a 4-year total of 1,300 acre-feet.

Well 29-40-101 was completed in 1927. This well was used at one time for public supply but reportedly the water was in small amount and of poor quality.

Changes in Water Levels

In the area of the Shep community, comparison of water levels measured in four wells in 1939 and those measured during this investigation in 1969 reveals a rise of from 0.1 to 1.9 feet (Table 5).

Well Construction

Well depths near the eastern limit of the San Angelo Formation are shallow but reach as much as

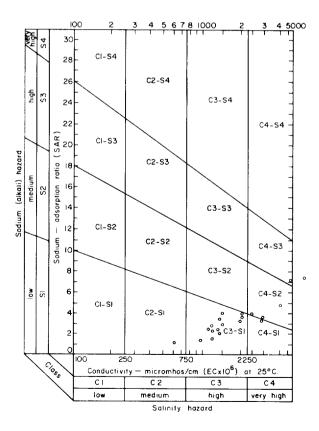


Figure 21.-Classification of San Angelo Formation Waters for Irrigation

165 feet to the west where successively younger beds overlie the water-bearing zones. Some wells are drilled and some are hand dug. The casing diameters range from 8 to 12 inches in the shallow drilled holes. The dug wells range from a few feet to 18 feet in diameter and are cased with brick, concrete, or light-gauge galvanized metal. In most of the shallow drilled wells, the casing is set through the aquifer and slotted or perforated opposite the water-bearing interval. The deeper wells are drilled and usually cased with light-gauge galvanized metal casing 4 to 6 inches in diameter.

Availability of Ground Water for Future Development

Based on data available, it is felt that limited additional ground water in the San Angelo is available for development. It is probable that the larger quantities occur in shallow zones near the eastern limit of the formation.

Other Water-Bearing Units

Ground water also occurs in Permian rocks of the Lueders Formation, Arroyo Formation, and Vale Formation, in ascending order; limestones of the Fredericksburg Group of Cretaceous age; and the Seymour Formation of Quarternary age.

The amount of ground water from these formations that is used at present, as well as that available for possible future development, is considered to be small to insignificant.

Lueders Formation

Extent of the Unit

The Lueders Formation outcrops in a narrow belt on either side of and extending along the Taylor-Callahan county line in the extreme southeast corner of Taylor County and north of the Cretaceous rocks to the vicinity of the Elmdale community. Northward these sediments are in the subsurface with only an occasional exposure along stream drainage (Figure 5).

Only six wells completed in the Lueders were inventoried during this study. General lithologic and water-bearing characteristics are shown in Table 1.

Source, Recharge, and Occurrence of Ground Water

The occurrence of the ground water is believed to be in fractures and solution cavities in the formation and, therefore, rather erratic. The sources of recharge are believed to be precipitation, discharge from the Cretaceous rocks, and to a lesser extent, discharge from the alluvium.

Limited data indicate that ground water in the Lueders occurs under both water-table and artesian conditions.

Movement and Discharge of Ground Water

Ground-water movement is assumed to be down gradient or toward points of artificial discharge.

Chemical Quality

Water samples from five of the six wells inventoried were collected for chemical analysis (Table 7 and Figure 9). The following discussion of the various chemical constituents is not considered to be representative of Lueders ground water in general, but only of the one area in the northeast part of the county from which all five samples were obtained.

Concentrations of the principal chemical constituents range as follows:

Calcium	174	to	780	mg/l
Magnesium	67	to	293	mg/l
Sodium plus potassium	230	to 1	1,750	mg/l
Bicarbonate	170	to	426	mg/l
Sulfate	265	to	600	mg/l
Chloride	415	to 4	1,320	mg/l
Fluoride	0.6	6 to	2.1	l mg/l
Nitrate	< 0.4	to	143	mg/l

The range of dissolved solids in the five samples is 1,430 to 8,030 mg/l. By the general classification based on dissolved-solids content (Winslow and Kister, 1956, p. 5), the waters from two wells (30-35-601 and 602) are slightly saline while those in the other wells (30-27-912, 913, and 30-35-301) are moderately saline. Comparison of dissolved-solids content of samples taken in 1939 with those obtained for this study in 1970 from wells

30-35-301 and 601 shows apparent alteration in the quality of water from each well but to a greater degree in well 301 (Figure 23).

The range of hardness for all water samples is 710 to 3,160 mg/l and, therefore, they are classified as very hard. This is not considered unusual since the water has moved through limestone (Tables 1 and 2).

The average sulfate content of all samples is 400 mg/!. None of the waters contained a sulfate level below the recommended 250 mg/l limit. Historical information shows considerable quality change in the water of well 30-35-301 and a small change in that of well 30-35-601 (Table 7).

The nitrate concentration average for the five samples is 66 mg/l. Three samples, from wells 30-27-912, 913, and 30-35-301, contained nitrate levels above the recommended 45 mg/l limit (Table 7). As with previously discussed constituents, the water from well 30-35-301 showed apparent alteration with a change in content from less than 20 mg/l nitrate in 1939 to 143 mg/l in the sample collected for chemical analysis in 1970. The cause for this increase is not known.

The chloride content averaged 1,734 mg/l in the five samples, considerably above the 250 mg/l maximum desirable. Again, the water in well 30-35-301 showed the greatest apparent alteration, from 126 mg/l in 1939 to 4,320 mg/l in 1970, while that of well 30-35-601 increased in chloride from 116 mg/l to 496 mg/l. The water in well 301 also contained 1,750 mg/l sodium, which is three to seven times more than that in each of the four other wells, indicating a good probability of contamination from oil-field brine (Figure 22, area 11). Samples from wells 30-27-912 and 913 had chloride levels of 1,960 and 1,480 mg/l, respectively, but a cause for probable alteration of the water quality in these wells is not apparent.

Water from three of the five wells had desirable fluoride levels, while that of well 30-27-913 contained 0.6 mg/l, less than the minimum recommended. Water from well 30-34-602 had a 2.1 mg/l content, well above the 1.0 mg/l upper limit recommended.

Hydraulic Properties of the Aquifer

In Taylor County, it is believed that the very low yields of Lueders wells will preclude their use for irrigation purposes.

Changes in Water Levels

Water-level conditions recorded in 1939 and those measured in 1970 show a rise of possibly about 14 feet in well 30-35-301 (dry in 1939), and a rise of approximately 1-1/2 feet in well 30-35-601.

Well Construction

All six wells inventoried were hand dug. Diameters of the wells range from 2 to 3 feet. Five are lined with brick and one with rock. The well depths range from 16 to 31 feet.

Arroyo Formation

Extent of the Unit

The surface extent of the Arroyo Formation can only be estimated in Taylor County. It is covered by surface soils, considerable Quaternary alluvium, and rocks of Cretaceous age. As shown by Figure 5, the estimated outcrop is in the eastern part of the county and extends in a belt 3 to 4 miles wide in a north-trending direction.

Seven wells and one spring believed to be completed in the Arroyo were inventoried. The general lithology and water-bearing properties are listed in Table 1.

Source, Recharge, and Occurrence of Ground Water

The primary sources of recharge to the Arroyo Formation are precipitation on the outcrop area and some discharge from Cretaceous rocks and alluvium. The ground water is believed to occur in solution cavities and possibly some fractures within thin limestone beds.

Very limited information indicates that the Arroyo ground water is, for the most part, under artesian conditions.

Movement and Discharge of Ground Water

Movement of ground water in the Arroyo is assumed to be down gradient to points of discharge.

One spring (30-43-802) appeared to flow from what was believed to be the Arroyo; however, its location is in close proximity to Cretaceous rocks, and the flow may be rejected recharge from that aquifer.

Chemical Quality

Samples were collected for chemical analysis from six of the seven wells and one spring. The results are shown in Table 7 and Figure 9. As with all other ground water in the county, the Arroyo waters are classed as very hard.

The ranges in concentration of the principal chemical constituents are:

Calcium	55 to 173 mg/l
Magnesium	26 to 157 mg/l
Sodium plus potassium	37 to 570 mg/l
Bicarbonate	345 to 630 mg/l
Sulfate	70 to 720 mg/l
Chloride	56 to 650 mg/l
Fluoride	0.5 to 5.7 mg/l
Nitrate	0.4 to 185 mg/l

The dissolved-solids concentration of the seven samples ranges from 510 to 2,460 mg/l and averages 1,331 mg/l. Two of the samples, from wells 30-43-801 and 802, contained dissolved-solids concentrations under 1,000 mg/l and are classified as fresh water. The remaining five samples ranged between 1,000 and 3,000 mg/l which classifies them as slightly saline. Historical information on one well (30-43-202) indicates an increase in the concentration of dissolved solids, from 463 mg/l (1939 sample) to 1,620 mg/l (1970 sample). It is not known whether this is natural or artificial alteration.

Hardness of water from the Arroyo ranges from 378 to 860 mg/l and, therefore, the water is classified as very hard. Water hardness in well 30-43-202 showed a noticeable increase from 118 mg/l in 1939 to 620 rng/l in 1970.

The average sulfate content of the seven samples was 250 mg/l. Four of the samples had sulfate levels under the maximum recommended by the U.S. Public Health Service (Table 7). The analyses for well 30-43-202 show a change in sulfate content from 85 to 275 mg/l (1939 to 1970).

Two of the seven samples contained nitrate concentrations above the recommended 45 mg/l limit. In well 30-35-201 the nitrate content was 143 mg/l. This well is used only for livestock watering and is located in a stock pen. Well 30-43-202 contained a nitrate level of 185 mg/l, but the source for the high concentration is not apparent. A sample collected in 1939 from this well showed a nitrate concentration of 60 mg/l.

The average chloride content of the seven samples was 335 mg/l. Two wells, 30-43-801 and 802, had chloride concentrations below the acceptable 250 mg/l limit. Well 30-35-202 contained a noticeably higher content of chloride as well as sodium and sulfate (650, 570, and 720 mg/l, respectively). Well 30-43-202 increased in chloride content from 98 mg/l in 1939 to 409 mg/l in 1970.

A desired level of fluoride (0.7 to 1.0 mg/l) was present in the sample from well 30-43-802. The water sample from well 30-43-801 contained less than the minimum recommended, while the remaining five samples exceeded the maximum recommended for this area.

Hydraulic Properties of the Aquifer

The yields of wells developed in the Arroyo in Taylor County are believed to be too small for irrigation use.

Well Construction

The depths of the Arroyo wells range from 27 to 180 feet. Three wells are hand dug and range in diameter from 3 to 4-1/2 feet. One of these wells is not cased while the other two are lined with rock and cement. Four wells are drilled and are cased with steel casing ranging from 4-1/2 to 7 inches in diameter.

Vale Formation

A total of eight wells were inventoried which were completed solely in the Vale Formation. Five of these are believed to be completed in the Bullwagon Dolomite Member only (Table 5). The general lithology and water-bearing properties of the Vale are shown in Table 1.

Extent of the Unit

Where it is not covered by surface soils or deposits of Quaternary and Cretaceous ages, the Vale is exposed in a belt about 10 to 12 miles wide which trends in a north direction across Taylor County (Figure 5). Because of the prominent scarp formed by the Bullwagon Dolomite east of Merkel, the top of Vale is easily discernible as long as the scarp persists. However, the southernmost reported exposure of the Bullwagon in Taylor County occurs on the north side of Farm Road 1235 at Bull Wagon Creek, about 5 miles southeast of Merkel. From this point south, the top of the Vale is only approximated. The base of the Vale in this study is considered to be at the top of the Standpipe Limestone. Reported exposures of the Standpipe occur along the west side of Lytle Cove about 3-1/2 miles southwest of Potosi; elsewhere the position of the base of the Vale is estimated.

Source, Recharge, and Occurrence of Ground Water

The source of recharge water for the Vale is primarily precipitation on its outcrop; however, discharges from Quaternary and Cretaceous sediments probably contribute significant amounts locally.

Occurrence of ground water in the Bullwagon Dolomite Member is probably in solution channels and fractures and may be quite erratic. Otherwise in the Vale, the ground water is believed to occur in small, thin sandstone lenses of low permeability.

Ground water in the Vale Formation, including the Bullwagon Dolomite Member, is generally under artesian conditions.

Movement and Discharge of Ground Water

Movement of ground water in the Vale Formation is down gradient to discharge areas. The only known method of discharge from the Vale is through well withdrawals.

Chemical Quality

Five wells completed in the Vale Formation were sampled for chemical analysis. Three of the wells were completed in the Bullwagon Dolomite, while the remaining two were completed in a lower section of the Vale. The results of these analyses are shown in Table 7 and Figure 9. The concentration ranges of the principal chemical constituents are:

Calcium	53	to	403	mg/l
Magnesium	52	to	248	mg/l
Sodium plus potassium	184	to	734	mg/l
Bicarbonate	306	to	950	mg/l
Sulfate	206	to	1,080	mg/l
Chloride	179	to	1,510	mg/l
Fluoride	0.8	to	3.0) mg/l
Nitrate	< 0.4	to	176	mg/I

The dissolved-solids content of all samples ranges from 1,120 to 4,200 mg/l and averages 2,154 mg/l. Four samples are classified as slightly saline (1,000 to 3,000 mg/l). One sample, from well 30-33-506, contained 4,200 mg/l dissolved solids and is classified as moderately saline water.

The hardness range is from 489 to 2,030 mg/l, with an average of 964 mg/l. Since waters with hardness over 180 mg/l are classified as very hard, all Vale water sampled falls into this classification.

The sulfate content of all five samples averaged 524 mg/l, about the same as that for the Choza Formation. Water from well 30-33-504 contained the least amount of sulfate (206 mg/l) of the five samples analyzed while that from well 30-33-506 contained the greatest amount (1,080 mg/l).

Four of the five samples contained nitrate in excess of the recommended 45 mg/l limit (wells 30-33-501, 503, 504, and 506). Samples from wells 501, 503, and 504 contained concentrations of 143, 120, and 176 mg/l, respectively. The water from well 506 contained 54 mg/l, slightly above the recommended limit. It is not known whether or not high nitrate concentrations in Vale Formation ground water are restricted to this one area. All three samples of ground water from the wells developed in the Bullwagon Dolomite contained nitrate in much higher concentrations than were found in the ground water from the two wells developed in the lower part of the Vale Formation; however, it is not known whether this pattern persists regionally.

The average chloride concentration of all water samples was 580 mg/l. The samples from two wells, 30-33-504 and 30-34-401, had chloride levels below the 250 mg/l limit. The water in well 30-33-506 contained almost three times the chloride concentration (1,510 mg/l) found in the sample with the next highest concentration. The sodium content of the water in well 506 is considerably higher (730 mg/l) than that in the water from the other four wells. The higher concentrations of sodium and chloride in the water from this well indicate apparent contamination of the water by brine (Figures 22 and 23).

The fluoride concentrations in two of the samples were within the desired 0.7 to 1.0 mg/l range while the remaining three samples contained more than the acceptable level.

Four water samples were analyzed for boron content. Three contained less than 1.0 mg/l, indicating that these waters should be safe to irrigate boron-sensitive crops. The water sample from well 30-33-506 contained 2.3 mg/l, indicating that irrigation with this water should be restricted to crops that have a tolerance for boron.

Water found in the Bullwagon Dolomite Member is classified as having a high to very high salinity hazard and a low to medium sodium hazard (Figure 20). Analyses of the ground water found at other horizons in the Vale Formation indicate that it has a very high salinity hazard and a high sodium hazard. Use of any of this water for irrigation should be limited.

Hydraulic Properties of the Aquifer

Three wells near Buzzard Peak, about 7 miles southeast of Merkel, have reported yields of 50 to 60 gpm (Table 5 and Figure 25). These wells, 30-41-201, 203, and 204, are believed to be developed in both the Choza and Vale Formations. Well 201 is used for irrigation and the other two for light industrial purposes. Two more industrial wells located in this same area have been drilled since the inventory for this study was completed and their yields are reported to be similar to the other three wells.

History of Development

Development of wells in the Vale Formation for industrial water supply began in 1966 and has continued into 1970. The estimated total pumpage through 1970 for wells 30-41-203 and 204 was 125 acre-feet.

Well Construction

All inventoried wells completed in the Vale Formation, including those completed in the Bullwagon Dolomite, are drilled wells and the maximum reported depth is 124 feet. The holes are cased with 7-inch or smaller diameter steel casing. In most instances, the casing depth is unknown; however, one well was reported to have casing set on bottom and slotted opposite the water-bearing interval, while another was reported to be an open-hole completion with only the upper part of the hole cased.

Availability of Ground Water for Future Development

Based on limited data, it would appear that some additional ground water from the Bullwagon Dolomite is available in the Merkel area. A dry test was reportedly drilled within one-quarter mile of wells 30-41-201, 203, and 204 in the Buzzard Peak area. The test was reported to be of sufficient depth to have penetrated all known water-bearing zones and may indicate a very limited areal extent of the water productive units in this immediate vicinity.

Fredericksburg Group

Extent of the Unit

It is estimated that about 75 percent, or 200 square miles, of the land surface formed by Cretaceous System rocks in southern Taylor County belongs to the Fredericksburg Group. These rocks make up the "cap rock" for the mesas and buttes in this area. The lithology and general water-bearing characteristics of these rocks are shown in Table 1.

The only source of ground water for one well and 29 springs inventoried during this study is rocks of the Fredericksburg Group.

Source, Recharge, and Occurrence of Ground Water

The source of recharge for ground water in the Fredericksburg Group is precipitation on the outcrop. Ground water is believed to occur mostly in solution channels within the limestones and to a lesser extent in thin zones of interbedded soft shales and limestones. Although ground water is known to be present in Fredericksburg Group rocks over most of the outcrop area except that north of Farm Road 89 and west of U.S. Highway 277, its reliability in general as a water supply is considered poor because many of the springs are reported to cease flowing during periods of drought.

Discharge and Movement of Ground Water

Discharge of ground water from the Fredericksburg Group occurs both naturally, in many scattered springs, and artificially through pumped wells. In general, movement of the ground water is down gradient to discharge points such as springs or seeps. Locally, ground-water movement may be toward a pumped well.

Chemical Quality

Table 7 shows the results of chemical analyses of water samples collected from one well and 29 springs during this investigation. As with the water in the Antlers Formation, water in the Fredericksburg Group is of relatively good quality, except for fluoride and hardness.

The ranges in concentration of the principal chemical constituents are:

Calcium	64	to 121	mg/l
Magnesium	8	to 43	mg/l
Sodium plus potassium	7	to 59	mg/l
Bicarbonate	256	to 459	mg/l
Sulfate	10	to 59	mg/l
Chloride	8	to 109	mg/l
Fluoride	0.2	to 0 .	7 mg/l
Nitrate	0.4	to 41	mg/l

As shown by chemical analysis, the waters from the Fredericksburg Group approach the quality standards for drinking water recommended by the U.S. Public Health Service (1962). The exceptions are the fluoride concentrations, which were mostly below the desired minimum level of 0.7 mg/l, and the dissolved-solids content which in a sample from one well (29-47-601) was 570 mg/l. The generally low concentrations of chemical constituents might be expected as the water has probably moved relatively short distances through these rocks.

The concentration of dissolved solids averages 347 mg/l. The range is from 252 to 570 mg/l which classifies the water as fresh.

The water is very hard as indicated by the range of total hardness from 208 to 413 mg/l.

The Fredericksburg Group does not yield sufficient quantities of ground water for use in irrigating

crops. The water from this aquifer has a medium to high salinity hazard for irrigation use and a low sodium hazard.

The SAR and percent sodium values are low, ranging from 0.2 to 4.9 and 4.5 to 24.7, respectively. A sample from spring 29-47-604 which was analyzed for boron contained 0.1 mg/l, which is well within the range considered safe for use on boron sensitive plants. Based on RSC calculations, all samples were well within the range considered safe for irrigation of crops.

Seymour Formation

Extent of the Unit

Scattered remnants of what may be predominately the Seymour Formation of Quaternary age occur along the Taylor-Jones county line from just north of Abilene to northwest of Merkel (Figure 5). It is uncertain as to the thickness of these sediments; however, they reach as much as 40 feet at one location north of Merkel. These alluvial remnants extend about 3-1/2 miles into Taylor County.

Source, Recharge, and Occurrence of Ground Water

Precipitation is the primary source for recharge for these Quaternary sediments. The only known occurrence of ground water in this alluvial deposit is in sand and gravel in a small area about 3 miles north-northeast of Merkel (Figure 25).

Discharge and Movement of Ground Water

Well withdrawal is the only method known for discharge of this ground water. The ground water in the Seymour is assumed to be under water-table conditions, and its movement would be generally from points of higher to points of lower elevation.

Chemical Quality

A sample from well 30-25-707 was collected for chemical analysis (Table 7 and Figure 9). The water is of fair quality and is classified as very hard (292 mg/l hardness as calcium carbonate). The nitrate content is 62 mg/l. The dissolved-solids content is 436 mg/l, with calcium (49 mg/l) and bicarbonate (336 mg/l) the predominate ions. This water from the Seymour is classified for irrigation use as having a medium salinity hazard and low sodium hazard.

Hydraulic Properties of the Aquifer

in Taylor County, little is known of the hydraulic properties of these Quaternary sediments. Reported yields of wells range from 10 to 20 gpm.

History of Development

Well 30-25-707 is the only irrigation well known to be completed exclusively in these Quaternary sediments; however, five other irrigation wells in this immediate area are completed in the Quaternary and the Choza Formation (Table 5 and Figure 25). Well 707 was completed in 1948 while completion dates reported in four of the other wells were from 1954 to 1967.

The estimated pumpage for irrigation in this area for a 16-year period from 1955 through 1970 is about 95 acre-feet.

Well Construction

All three wells inventoried in this area which are developed in the Quaternary are reported to have been drilled. The casing in these wells is constructed of heavy gauge steel, is set on the bottom of the hole, and perforated opposite the water-bearing interval. The well depths range from 25 to 40 feet.

SURFACE-CASING RECOMMENDATIONS

The Texas Water Development Board recommends to members of the oil and gas industry and to the Texas Railroad Commission the depth to which ground water should be protected in drilling tests for oil and gas. The authority for participation by the Texas Water Development Board in this surface casing program is derived from rules promulgated by the Railroad Commission under authority given that agency by the statutes dealing with regulation of drilling and production activities of the oil industry.

Statewide Rule 8 of the Railroad Commission required that all fresh water be protected in drilling or production activities.

Statewide Rule 13 of the Railroad Commission requires that an operator obtain a letter from the Texas Water Development Board stating the depth to which fresh water strata should be protected before drilling and setting casing in his first well in a field or area.

In carrying out its duties under Rule 13 the Texas Water Development Board maintains technical data files for all areas of the State which serve as a basis for preparing recommendations to operators contemplating the drilling of test wells. The depth to which ground water of usable quality should be protected is based on all pertinent information available to the surface casing program staff at the time the recommendation is given. Recommended depths in any one area may therefore be revised from time to time as additional information becomes available. Known depths of wells producing, or formerly in use to produce, ground water of usable quality, such as domestic, municipal, industrial, livestock, and irrigation wells, are of primary value in ascertaining these recommended depths. Electric or gamma-ray neutron logs of oil and gas tests are used in many areas of the State to determine the depth to which the base of usable-quality ground water occurs. Surface elevation is considered when a recommendation is given in an area that has moderate to high surface relief, a common condition in north-central Texas counties. This consideration is imperative when the slope of the land surface does not conform to the dip of the underlying geologic formations because of the danger that poor quality water will cause contamination of surface and ground water by moving along the dip of the beds to points of discharge in stream channels. All of this information is interpreted in the light of the best knowledge of the geology and ground-water hydrology available on the area involved.

Because of the erratic occurrence of ground water in Taylor County, described in preceding sections of this report, known depths of water wells should be given special weight in preparing surface-casing recommendations in the county. Ground water of usable quality is known to occur at the ground surface and to depths ranging to nearly 300 feet. In some areas in the southern part of the county usable-quality ground water may occur at depths of 500 feet or more. Thus, information obtained as a result of this study indicate that a county-wide depth recommendation for protection of ground water is not feasible. Further, these recommendations should be made on a well-to-well or lease-to-lease basis in order to afford maximum protection without imposing unnecessary economic burden.

PRODUCTION AND DISPOSAL OF OIL-FIELD BRINE

In 1962 and 1968, data concerning 1961 and 1967 oil-field brine production and disposal methods were

collected by the Railroad Commission of Texas, the Texas Water Quality Board, the Texas Water Commission (in 1962), and the Texas Water Development Board (in 1968). These data were submitted by the oil and gas operators and are summarized in Table 9.

Areas and Methods of Disposal and Quantities

Figure 22 delineates areas of disposal, methods of disposal, and quantities of brine disposed. The outlined areas represent the greatest concentrations of producing oil or gas wells from which some brine production was reported and do not necessarily coincide with the outlines of individual oil or gas fields. Areas 1 through 26 fall in the Brazos River drainage system. Areas 27 through 34 are in the Colorado River drainage system. The area number designations and the disposal and production statistics are tabulated by individual fields in Table 9.

Methods of disposal of brines are by injection into the subsurface, discharge into surface pits, and miscellaneous.

Injection of brines into the subsurface is accomplished by directing the water down well bores, either under pressure or by gravity, into permeable zones below the surface of the ground, and below all zones productive or potentially productive of fresh water. This method is commonly used in secondary recovery operations of the oil industry.

Surface-pit disposal is accomplished by placing the brines into dug pits for evaporation. The use of this method of disposal is prohibited by a Railroad Commission order effective January 1, 1969.

Miscellaneous disposal is accomplished by hauling the brines by truck from one area to another for disposal by injection wells or surface pits, or dumping on roadways or into surface drainageways.

Of the 29 areas reporting brine disposal by surface pits in 1961, 11 were still using this method in 1967. Ten of the 11 areas reported 50 to nearly 100 percent reductions in disposal by surface pits while one, area 22 on Figure 22, reported an increase in disposal by this method. Eighteen of the areas reporting disposals by surface pits in 1961 apparently had discontinued that method by 1967. Three areas reported disposal of brine by injection only, in 1961 and 1967. Three areas reporting brine production in 1961 did not report any production in 1967. Two areas reporting brine production in 1967 did not report any in 1961.

A comparison of the relative amounts of brine disposed of by the three methods for the years 1961 and 1967 is as follows:

	PERCENTAGE OF TOTAL DISPOSAL						
YEAR	INJECTION	PITS	MISCELLANEOUS				
1961	87.6	11.7	0.7				
1967	98.7	.8	.5				

Reported brine production in 1961 and 1967 for Taylor County is listed in Table 9. Briefly, the table shows an overall reduction in brine produced to 4,307,897 barrels from 4,745,183 barrels in 1961, a drop of slightly under 5 percent. Reported pit disposal was down to 32,727 barrels from 554,658 barrels in 1961, a drop of about 94 percent. The reported injection disposal was up to 4,254,211 barrels in 1967 from 4,154,872 barrels in 1961 or a gain of approximately 2 percent. Miscellaneous disposal was down to 20,959 barrels from 35,653 barrels in 1961 or a drop of about 41 percent.

Chemical Quality of Produced Brine

Table 8 is a tabulation of chemical analyses of some oil-field brines in Taylor County (Laxon et al., 1960). These analyses show that, generally, the same ions are present in the brines as in waters used for irrigation, industrial, public supply, domestic, and stock use (Table 7). Comparison of the analyses from the two tables also shows that calcium, chloride, magnesium, and sodium ions are in greater concentrations in the brines as are the total dissolved solids. Ranges of dissolved-solids concentration from Table 8 and Table 7 are 61,000 to 226,900 ppm and 174 to 8,030 ppm, respectively. Also, a comparison of ion concentration ranges between the two tables is as follows:

ION	RANGE (ppm) TABLE 8 (Oil-field brine)	RANGE (ppm or mg/l) TABLE 7 (Ground water)					
Calcium	1,484 to 20,000	23 to 780					
Chloride	32,853 to 126,500	4 to 4,320					
Magnesium	463 to 2,890	6 to 383					
Sodium	17,425 to 53,600	6 to 1,750					

Produced Brine as a Potential Source of Ground-Water Contamination

A primary potential source of ground-water contamination is through improper disposal of oil-field brines by discharge into unlined surface pits, by injection into the subsurface through faulty injection wells, or by leakage in improperly plugged or cased oil tests and wells.

Contamination of ground water by the downward percolation of brine from unlined pits through permeable soils can and probably has done almost irreversible damage to some aquifers. It is believed that this method of disposal has contributed, to what degree is unknown, to the contamination of more than one aquifer in Taylor County.

In areas of oil production, brine under natural or introduced pressure may move up the bore hole and into a fresh-water zone if it is not properly protected by casing and cement. Brines produced with oil and gas may co-mingle with usable-quality water in several ways; much work has been done by the oil industry and the Railroad Commission of Texas to correct this contamination problem associated with oil and gas production.

GROUND-WATER PROBLEMS

Alteration of Native Water Quality

Ground water is altered chemically by natural and artificial means. Alteration by natural means is accomplished by the dissolving of minerals from the rocks over and through which water flows or percolates. Artificial alteration of ground-water quality may be by chemical or biological processes. Wells positioned down gradient from septic tanks, barnyards, feedlots, or other sources of organic wastes may produce contaminated ground water. A high nitrate content in the water is suggestive of a biological source of contamination. Brine accompanying the production of oil and gas is a very significant source for alteration of native quality ground water. The leaching or dissolving by water of some of the constituents in fertilizers added to soils is another means by which ground-water quality is altered.

Figure 22 shows several wells which are apparently contaminated. This illustration also indicates some areas of vegetative kill or those areas in which very little or no vegetation will grow because of soil contamination. These kill areas are apparently associated with brine produced in oil-field areas. The photographs shown in Figure 24 were taken in some of these areas.

In Figure 23, radial diagrams portray the relative concentrations of dissolved minerals in native ground water, in apparently contaminated ground water, and in typical oil-field brines. The diagrams show native ground water and apparently contaminated ground water in paired wells that are closely spared. Using the same scale for each plot, the percentages of the constituents shown were plotted on the appropriate coordinates and the plotted points were connected by straight lines. The resulting diagrams show the similarities or differences between the selected analyses.

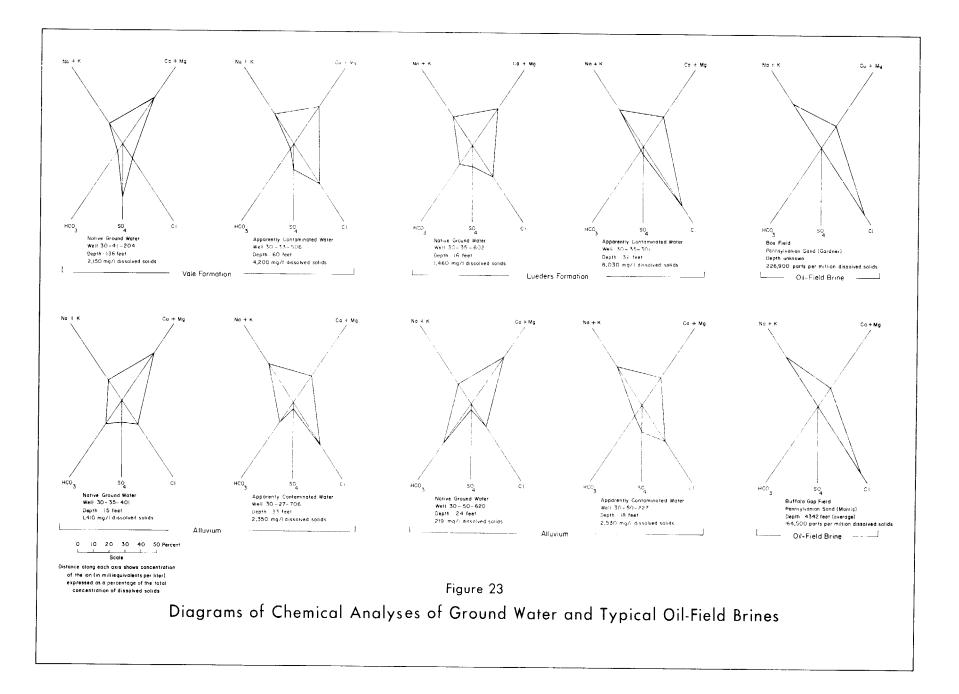
Areas of Vegetative Kill and Possible Causes

Each of the known areas of vegetative kill in Taylor County appears to be related to oil or gas production. These areas are small (approximately 2 acres or less) and few in number. In Figure 24, photograph A shows a small kill area which appears to have been caused by a pipeline leak. Photographs B and C show kill areas which appear to have been caused by tank battery leakage or overflow. Photograph D shows a seep of very saline water that is associated with a vegetative-kill area. Chemical analysis of the water revealed it contained 10,100 mg/l chloride and 16,300 mg/l dissolved solids. Photograph E shows a kill area in a drainage tributary down gradient from an oil field a short distance away. Photographs F, G, and H reveal evidence of apparent frequent overflow of oil from a tank battery. A main drainage tributary to a lake that is used on occasion for municipal water supply for Abilene lies just a short distance down gradient from this battery.

Twenty-seven areas which were reported to have "salt pollution" were hurriedly checked for evidence of vegetative kill. Although in most areas no evidence was seen, 23 were located in and along drainage from areas reporting brine production.

CONCLUSIONS

In terms of number of acre-feet of water used, the four most important water-bearing units in Taylor County are: The alluvium of the Quaternary System, particularly that along Jim Ned and Elm Creeks; the Choza Formation of the Permian System in and around the town of Merkel; the Antlers Formation of the Cretaceous System; and the San Angelo Formation of





A. Small vegetative-kill area apparently associated with leakage from a pipeline, NWNE J. G. Eels Survey No. 453. View is east.



B. Small vegetative-kill area which appears to have resulted from runoff from spillage at a tank battery, SESE W. M. Smith Survey No. 452. View is north.



C. Vegetative-kill area apparently caused by runoff from spillage at a tank battery (removed), extreme SW part J. C. Eccles Survey No. 472. View is northwest.



D. Seep (origin unknown) associated with vegetative-kill area about 1/3 mile to the northwest, east edge of Grimes CSL Survey No. 124. Water sample contained 3,670 mg/l sodium, 10,100 mg/l chloride, and 16,300 mg/l dissolved solids. View is northwest.

Figure 24.-Photographs of Vegetative-Kill and Possible Contamination Areas, 1970



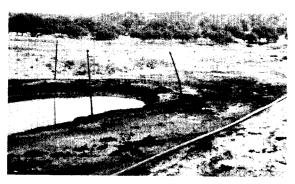
E. Vegetative-kill area down gradient from and along drainage passing through an oil field, extreme west end of J. Nabers Survey No. 9. View is northwest.



F. Tank battery location showing evidence of oil spillage and overflow. Small pit located in right center (dark area), Sec. 4, Blk. 1, ELRR Survey. View is west.



G. Same battery as F. Note dark overflow on side of tank. View is east.



H. Same pit as in F. Dark areas to right of pit indicate drainage to the right. Drainage tributary into Lake Abilene is located at about the base of the trees across center of photograph with drainage direction from left to right. View is northeast.

the Permian System. The Lueders, Arroyo, and Vale Formations of the Permian, and the Fredericksburg Group of the Cretaceous contain ground water in sufficient amounts for domestic and livestock use; however, the occurrence of the ground water is erratic, especially in the Permian rocks.

The demand for ground water in Taylor County is expected to continue as long as usable quantities are available because, generally, water in west-central Texas is in short supply as compared to other areas of the State.

The chemical quality of all ground water in the county varies from area to area. Waters in the Cretaceous rocks are classified as fresh and are the lowest in mineral content. Well yields are less than 100 gpm. Ground waters in the Quaternary rocks are classified as fresh to moderately saline and are the highest in mineral content. Well yields range from small to moderate.

Contamination, apparently from oil-field brines, is in evidence in waters of several wells over the county; however, determining the extent of contamination in the various aquifers as well as linking contamination directly to specific sources is beyond the scope of this study. Higher than average concentrations of nitrate in alluvium ground water in the Tuscola area may have resulted, in part, from the combined effect of many septic tanks concentrated in a relatively small area and nitrogen from fertilizers in use in this irrigated farming area. Since ground water in this area is used for human consumption, it is deemed advisable to set up a water-quality monitoring system.

Ground water found in the alluvium underlying the city of Abilene's landfill project located adjacent to Elm Creek appears to be adequately monitored for any quality changes which might occur as a result of this operation. The city maintains 14 observation wells on the project site. Ground-water samples are collected from these wells at regular intervals and submitted for chemical and bacterial analysis. Water samples should be collected periodically for analysis from the wells developed in the San Angelo Formation at the Cal-Tex Feed Yard northeast of Trent to detect any changes in water quality affecting ground water down gradient to the west.

There were insufficient data available to determine net changes in water levels in the various water-bearing units. A network consisting of one to three selected observation wells should be established for the Choza Formation, San Angelo Formation, Antlers Formation, and the Recent alluvium in order to determine the long-term effects of water use on the water levels of these units. Some or all of these wells could also serve as water-quality monitoring wells.

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Table 5.--Records of Selected Water Wells and Springs in Taylor County and Adjacent Areas

- Water levels
 Reported water levels are given to the nearest foot; measured water levels are given to the nearest tenth or hundredth of a foot.
 Method of lift and type of power: C, cylinder; E, electric; C, gasoline, butane, or natural gas; Cf, centrifugal; H, hand pump; J, jet; N, none; R, reciprocating; Sub, submersible; T, turbine; W, windmill. Number indicates horsepower.
 Use of water
 D, domestic; ind, industrial; irr, irrigation; N, none; P, public supply; S, livestock.
 Letter prefixes
 BX, Callahan County wells; PY. Jones County wells; UA, Nolan County wells; XW. Taylor County wells.
 Water-bearing units
 Q dal, Quaternary alluvium; Qu, undivided Quaternary surficial deposits; Qs, Seymour Formation; Kf, Fredericksburg Group; Ka, Antlers Formation; Pasa, San Angelo Formation; Pc, Choza Formation; Pl, Lueders Formation.

Altitude of land surface was determined from topographic maps.

					CASI	NG				TER LEVEL			
WELL	OWNER	DRILLER	DATE Completed	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-29-31-904	Lola Lee O'Kelly	Robert Higgins	1964	28	7	28	Psa	1,908	2.94	May 4, 1970	c, w	S	Water reported at 14 ft from sand. Casing slotted from 15 to 28 ft.
905	H. C. Hammer			23			Psa	1,903	2.96	do	N	N	Dug well.
* 906	do	Bob Dennis		80	6	40	Psa, Pcm	1,903	5.60	də	J, E, 1/2	N	Water reported at 14, 35, and 65 ft. Crooked hole. Casing perforated at 35 ft.
32 - 702	R. L. Bland, Jr.	Jack Leonard	1968	23	12		Psa	1,863			Sub, E, 5	Ind	Reported yield 140 gpm. Water reported from sand and gravel at 14 to 17 ft. Well screened from 15 to 23 ft.
/03	do	do	1968	Ž2	12		Psa	1,863			Sub, E, 5	Ind	Reported yield 120 gpm. Water reported from sand and gravel at 14 to 17 ft. Well screen from 14 to 22 ft.
704	do	do	1968	23	8		Psa	1.864			T. E. 5	Ind	Reported yield 180 gpm. Water reported from sand and gravel at 14 to 17 ft. Well serven from 15 to 23 ft.
705	do	do	1968	25	12		Psa	1,864			т, е, 5	Ind	Reported yield 125 gpm. Water reported from sand and gravel. Well screen from 17 to 25 ft.
706	do	do	1968	23	12		Psa	1,864			Sub, E, 5	Ind	Reported yield 125 gpm. Water reported from sand and gravel. Well screen from 15 to 23 ft.
707	do		1969	72	12	10	Рс, Рст	1,870	17.20	Oct. 16, 1969	N	N	Reported yield 20 gpm. Water reported from shale. Small amount of sand and gravel reported.
708	do	Jack Leonard	1967	110	8	110	Pc	1,881			Sub, E,	Ind	Reported yield 30 gpm. Water reported from shale.
709	do	Johnson & Henderson	1967	103	8		Рс	1.879			Sub, E, 1	Ind	Reported yield 35 gpm. Water reported from shale at 75 fL.
710	do	Jack Leonard	1968	26	12		Psa	1.876	8.31	Oct. 16, 1969	Sub, Е, З	Lind	Reported yield /5 gpm, Water reported from sand and gravel. Well screen from 18 to 26 ft.
711	do	do	1968	27	12		Psa	1,877			Sub. E, 3	Ind	Reported yield 70 gpm. Water reported from sand and gravel. Well screen from 19 to 27 ft.
712	do	do	1968	27	12		Psa	1,877			Sub. E, 3	Ind	Reported yield 77 gpm. Water reported from sand and gravel. Well screen from 19 to 27 ft.
713	đo	do	1968	29	9		Psa	1.878			Sub, E, 3	Ind	Reported yield 70 gpm. Water reported from sand and gravel. Well screen from 21 to 29 ft.
* 714	do	Johnson & Henderson	1968	23	10		Psa	1,878	12.4	Oct. 16, 1969	Cf, E, 1	Ind	Reported yield 40 gpm. Water reported from sand and gravel at 16 to 21 ft.
715	do	do	1968	25	10		Psa	1,878	13.11	do	Cf, E, 1-1/2	Ind	Reported yield 60 gpm. Water reported from sand and gravel at 16 to 23 ft.

See footnotes at end of table.

					DEPTH	CAS	ING				ATER LEVEL		1	
	WELL	OWNER	DRILLER	DATE COMPLETED	OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
	W-29-32-716 717	R. L. Bland, Jr. do	Johnson & Henderson	1968	26	10		Psa	1,877	12.82	Oct. 16, 1969	0 Cf. E, 2	Ind	Reported yield 80 gpm. Water reported from san and gravel at 18 to 24 ft.
	718	do	 do	1967 1966	26 27	10		Psa	1,878	14.39	Oct. 15, 1969	2/	Ind	Reported yield 90 gpm. Water reported from san and gravel at 15 to 25 ft. This well on manifold with well XW-29-32-718.
	719	do				10	27	Psa	1,878	13.30	do	Cf. E, 5	Ind	Reported yield 135 gpm. Water reported from sa and gravel at 15 to 25 ft. On manifold with well XW-29-32-717. Well screen from 19 to 27 ft.
*	720	do	do	1968	2.5	12	25	Psa	1,879	14.40	do	Sub, E,	Ind	Reported yield more than 90 gpm. Water reported from sand and gravel at 19 to 23 ft.
Ĥ	/21	B. W. Hamner	do Robert Higgins	1967	26	11		Psa	1,879	15.56	do	Cf, E,	Ind	Reported yield 120 gpm. Water reported from sar and gravel at 15 to 25 tt.
ż	907	Jarrett E. Williams	do	1966	40	6	22	Psa	1,885	2.33	May 4, 1970	Cf, E, 1/3	S	Reported yield 7 gpm. Water reported from sand at 7 ft. Casing slotted from 7 to 12 ft.
	908	do	do	1964	80	6	80	Pc	1,829	35.75	Nov. 4, 1969	Sub, E, 1	irr	Reported yield 30 gpm. Water reported at 50 to 52 and 67 to 69 ft. Casing perforated from 62 to 80 ft. <u>3</u> /
ķ	909	do		1964	80	6	80	Pc	1,817	18.29	do	Sub, E, 1-1/2	Irr	Reported yield 45 gpm. Water reported at 26-28, 54-56, and 68-70 ft. Casing slotted from 50 to 80 ft. 3:
			do	1964	40	7		Pc	1,814	7.82	Dec. 15, 1969	N	Irr	Reported yield 150 gpm, Well has not been used in 4 or 5 years. Pumped occasionally with centrifugal pump.
	910	do	ofi	1964	60	5	60	Pc	1,841	36.34	Dec. 15, 1969	c. w	D.S	
	911	do			50	5	50	Pc	1,841			Sub, E,	0	Reported yield 5 gpm.
	912	do			70	6	70	Pc	1,840	35.87	Dec. 15, 1969	1/2 Sub, E,	D	Reported yield 10 gpm.
	913	do			60	4		Pc	1.814	8.08 7.10 8.80 10.06	do Apr. 15, 1970 Aug. 24, 1970 Jan. 15, 1971	3/4 C, W	S	Reported yield 12 gpm. This well previously an observation well.
		H. C. Hamner	Bob Dennis	1955	85	6	85	Psa	1,917	10.83	May 4, 1970	J, E, 1/2	S	Water reported at 65 ft. Casing perforated at 65 ft.
	302	do	Jack Leonard	1969	20	12	20	Psa	1,914	7.37	do	N	N	Reported yield 20 gpm. Water reported at 13 ft. Casing slotted from 13 to 19 ft.
			A. L. Hicks	1970	60	7	20	Psa	1,981	7.52	May 8, 1970	с, w	N	Reported yield 4 gpm. Water reported from green sandy clay at 22 to 24 ft. 3
		Jessie Acuna Frank Brnovak		1952	97	6	97	Psa	2,055	51.68	do	с, w	D	Reported yield 6 gpm. Water reported at 65 and 80 ft from white sand.
	903				130	5		Psa	2,140	48.54	May 19, 1970	N	N	
	1	do			130	5		Psa	2,160	66.80	do	N	N	
	904	dø			101	5		Psa	2,160	69,94	do	N		
	905	do			130	5		Psa	2,160	97.8	do	с, w	N D	 Reported good well.

Table 5.--Records of Selected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

Table 5. -- Records of Selected Water Wells and Springs in Taylor County and Adjacent Areas -- Continued

					CASI	ING				TER LEVEL			
WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-29-32-906				33	5		Psa	2,130	14,50	May 19, 1970	c, w	N	
* 907	do			90	5		Psa	2,108	12.64	do	c, w	s	
* 908	A. D. Barnes	Robert Higgins	1963	125	6	20	Psa	2,083	21,99	do	Ј, Е, 1	D. S	Reported yield 10 gpm, Water reported at 100 ft.
909	do			50	6	50	Psa	2,082	16.15	do	с, w	N	Reported weak well.
40-101	City of Trent		1927	50			Psa	1,910	22 15.88	July 25, 1939 Nov. 6, 1969	T, E, 5	Ind	Dug well. Former municipal well, used occasionally for industrial purposes. Well 1. 8/
102	do	Mr. Newhouse	1952	15	5		Psa	1,912	12.0	Nov. 5, 1969	N	N	Dug well. Reported weak well, May be caved.
103	do	do	1952	23	5		Psa	1,912	10.8	do	N	N	Dug well, Reported weak well.
104	do	do	1952		5		Psa	1,911			N	N	Dug well. Reported weak well. Reported caved at 7 ft.
* 105	do	do	1952	33			Psa	1,911	10.6	Nov. 5, 1969	N	N	Dug well. Reported weak well.
106	do	do	1952	15	5		Psa	1,911	9.1	do	N	N	Do.
107	do	do	1952	18	5		Psa	1,910	11.4	do	N	N	Do.
* 201	J. K. Pee	Mr. Sublett	1935	33	6	30	Pc	1,828	8,72	Apr. 15, 1970	с, w	S	Water reported at 14 and 30 ft.
* 202	do	do		80	4	80	Pc	1,835	9.4	do	C, G	S	
* 203	Earl Schultz	Robert Higgins	1958	55	8	55	Pc	1,874	5.31	May 5, 1970	J, E, 3/4	D, S	Water reported at 42 and 50 ft.
204	do			20			Рс	1,872	6.63	do	N	N	Dug well. Reported yield 4 barrels per day.
* 205	do			90	5		Pc	1,879			с, w	N	Reported good well. Appears caved at approximately 10 ft.
* 301	City of Merkel		1909	100	7	30	Рс	1,866	15.4	Oct. 20, 1969	N	N	Reported yield 50 gpm in 1946. Last used for municipal supply in July 1955. Connected by tunnel to $XW-29-40-308$. Reported to be destroyed.
302	do	L. Sublett	1925	100	8	20	Pc	1,867	13	do	T, E, 7-1/2	N	Reported yield 50 gpm. Last used for municipal supply in July 1955. Connected by tunnel to XW-29-40-304.
* 303	do	do	1926	100	ñ	20	Pc	1,867	10.4	do	N	N	Reported yield 50 gpm. Last used for municipal supply in July 1955. Connected by tunnel to XW-29-40-305.
304	C. H. Hobbs	W. E. Kimmery	1926	70			Pc	1,867	64.1 <i>4</i> 10.4	Apr. 17, 1946 Oct. 20, 1969	Sub, E, 3	Irr	Dug well. Reported yield 50 gpm. Last used for municipal supply in July 1955. Connected by tunnel to XW-29-40-302.
305	City of Merkel	do	1945	63			Pc	1,867	62.3 4	Apr. 17, 1946	N	N	Dug well. Last used for municipal supply in July 1955. Reported yield 50 gpm. Connected by tunnel to XW-29-40-303.
306	do			100	7		Pc	1,863			N	N	Last used for municipal supply in July 1955.
* 307	do			100	7		Pc	1,862	9.0	Oct. 20, 1969	N	N	Last used for municipal supply in July 1955. Well caved at about 12 ft.
308	do	J. B. Ferrier		75			Pc	1,866			N	N	Well destroyed. Last used for municipal supply in July 1955. Reported yield 50 gpm.

See footnotes at end of table.

Table 5Records of	Selected Water Wells	and Springs	in Taylor County	and Adjacent AreasContinued	
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						CAST	NG				TER LEVEL			
ţ	VELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
XW-2	29-40-309	City of Merkel	L. Sublett	1926	100	8	20	Pc	1,867		Apr. 17, 1946	N	N	Reported yield 18 gpm in 1946. Last used for municipal supply in July 1955. Caved above 10 ft.
	310	do			100	7		Pc	1,865			N	N	Last used for municipal supply in July 1955. Filled with debris to 6 ft.
	311	do			100	7		Pc	1,860			N	N	Last used for municipal supply in July 1955. Caved at 11 ft.
*	312	Jarrett E. Williams	Robert Higgins	1964	93	7	93	Pc	1.820	16.39	Dec. 15. 1969	Sub. E. 5	Irr	Reported vield 150 gpm. Water reported at 30-31. 55-57, and 67-69 it. Casing slotted at 32-60 and 70-90 ft. 3
÷	313	W. E. Wisenhunt	do	1968	98	8	30	Pc	1,870			Sub. E. 5	S, Irr	Reported yield 75 gpm. Water reported from 34. 51, 68 ft (25 gpm), and 90 ft (25 gpm).
	314	do			80			Pc	1,870	14.05	Feb. 9, 1970	J, E	D, S	Water reported from 80 ft.
*	315	A. P. Wozencraft	Robert Higgins	1968	100	7	100	Pc.	1,878	14.75	do	Sub, E, 3	S, Irr	Measured yield 51 gpm July 29, 1970. Water reported from 22, 42 to 43, 72 ft (strongest zone), and 91 ft. Casing slotted at 60 to 100 ft. 7,
	316	Joe Henry		1962	70	12	50	Рс	1,849	33.20	May 8,1970	J, E, 3/4	D, S	Water reported at 42 and 65 ft.
	317	do	Robert Higgins	1965	100	11	30	Рс	1,845	26.59	do	Sub, E, 7-1/2	Irr	Reported yield 80 gpm. Water reported at 41-42, 69-72, and 79-81 ft. $\underline{3}$
	318	Merkel Country Club	do	1958	100	5	20	Pc	1,855	33.83	May 7, 1970	J, Е, 1	Irr	Reported yield 15 gpm. Water reported at 40, 55. and 70 ft.
*	319	do	do	1958	100	5	20	Pc	1,849	32.27	do	J. E. 1	Irr	Reported yield 30 gpm. Water reported at 40, 55, and 70 ft.
*	320	do	do	1958	100	5	20	Pc	1,837	16.09	do	Sub, E,	Trr	Reported yield 100 gpm. Water reported at 40, 55, and 70 ft.
	321	do	do	1958	100	5	20	Pc	1,840	14,53	do	N	Ν	Do.
	322	do			70	5		Pc	1.837	17.20	do	J. E. 1	N	Reported yield 20 gpm.
	323	do	Robert Higgins	1958	100	5	20	Pc	1,845	22.90	do	J, E, 1	Irr	Reported yield 40 gpm. Water reported at 40, 55. and 70 ft.
	324	do	do	1958	100	5	20	Pc	1,855	37.54 4	do	Sub, E, 3/4	Irr	Reported yield 50 gpm. Water reported at 40. 55, and 70 ft.
	325	Merkel Independent School District	do	1967	90	6	90	Pc	1,968	20.00	May 14, 1970	Sub, E	lrr	Reported yield 60 gpm. Water reported at 35 36, 54-56, and 67-69 ft. Casing perforated at 40-85 ft. $\underline{3}$
	326	do	do	1950	70	8	30	Pc	1,967			J, E. 2	N	Reported weak well. Water reported at 30. 54, 66 ft (strongest zone).
*	327	do	do	1967	92	6	92	Pc	1,968	18.17	May 14, 1970	Sub, E	Irr	Reported yield 50 gpm. Water reported at 54-56 and 67-70 ft. Casing perforated at 50-90 ft. 3
*	328	do	dø		110	8	30	Pc	1,972	17.81	do	Sub, E, 2	Irr	Reported yield 50 gpm. Water reported at 40, 62, 86 (strongest zone), and 105 ft.
	329	do	do		90	8	30	Рc	1,975	19,22	do	J, E	N	Reported yield 30 gpm.
				I										

					CASI	NG				TER LEVEL			
WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-29-40-401	W. R. Scott		1937	225	6	225	Psa, Pc	2,085	64.7	May 8, 1970	с, w	D, S	Water reported at 85 ft (weak) and 180 ft (main supply). Slotted liner from 185 to 225 ft. Open hole from surface to 100 ft.
» 501	W. B. Toombs Estate		1929	65			Pc	1,954	40.9 11.39	Aug. 28, 1939 May 19, 1970		N	Dug well. Well 4. <u>8</u>
* 502	Mrs. Fannie Latimer			40			Pc	1.941	13.8 6.46	Aug. 28, 1939 May 19, 1970		N	Dug well. Well 5. 8
* 503	F. I. Toombs			80	5	20	Pc	1,938	43.0	May 20, 1970	J, E, 3/4	s	
* 601	H. O. Boney	Higgins & Malone	1950	110	7 3	20 30	Pc	1,876	12.22 11.20 16.56 16.97	Oct. 17, 1969 Mar. 16, 1970 Sept. 16. 1970 Jan. 15, 1971	Sub, E, 2	Irr	Measured yield 41 gpm on July 29, 1970. Formerly Merkel municipal well. last used as such in July 1955. Observation well. Water reported at about 28 and 43 ft with main supply reported at 65 and 85 ft. J
602	do	do	1950	110	7		Pc	1,876			N	N	Formerly Merkel municipal well, last used as such in July 1955. Reported yield more than 50 gpm. Water reported at about 28 and 43 ft with main supply reported at 65 and 85 ft. 7
603	do	do	1950	110	7		Pc	1,877			N	N	Do.
604	do	do	1950	110	7		Pc	1,877			N	N	Do.
* 605	Connie Mack Seymore	Robert Higgins	1967	108	6	20	Pc	1,878	11.1	Oct. 20. 1969	Sub, E, 3	Irr	Measured yield 53 gpm on July 3, 1970. Main water reported from shale breaks at 60 to 70 ft and 80 ft. Occasional water reported from sand and gravel at 12 ft. Casing slotted at 12 ft. <u>7</u>
* 606	Stanley Toombs	Stanley Toombs	1962	120	7		Pc	1,899	12.4	Nov. 5, 1969	T, E, 5	Irr	Reported yield 45 gpm. Water reported from grave at 11, 16, and 18 ft and shale breaks below at unknown depths. "Cyp" water reported at 85 ft and below.
* 607	do	do		80	6	30	Pc	1,901	12.1	Nov. 5. 1969	J, E. 3/4	D	
k 608	do	do	1959	125	11		Pu	1,901	13.8	do	T, E, 5	Irr	Reported yield 90 gpm. Water reported from grave at 11. 16. and 18 ft. "Gyp" water reported at 85 ft and below.
∞ 609	Mrs. Odis Griffin	Robert Higgins	1968	100	5	100	Pc	1,895			Sub. E. 1/2	D	Reported yield 30 gpm. Water reported at 38-39, 54-55, 67-68, and 79-81 ft. Casing perforated at 35-95 ft. 3
610	do	do	1967	120	6	120	Pc	1,895			J, E, 3/4	D	Reported yield 15 gpm. Water reported at 40-41, 62-63, and 78-79 ft. Casing slotted at 40-80 and 85-115 ft. <u>3</u>
* 701	Charles Rancier			52	7		Psa	2,065	18.65	May 19, 1970	с, w	s	
702	du		1962	65	4		Psa	2,055	18,74	dø	с , w	5	
703	B. E. Perkins	Robert Higgins	1961	55	5	20	Psa	2,047	14.74	do	J, E, 1/3	D, S	Reported yield 8 gpm. Water reported at 38 ft (weak) and 45 ft (main supply),
* 801	L. B. Hester		1916	34			Pc	1,941	23.40	Dec. 5, 1969	н	D, S	Weak well. Water reported from clay. Reported producing from open hole.
* 802	do	L. B. Hester	1956	29			Qa1	1,901	18.87	do	N	N	Dug well. Weak well. Water reported from five zones, each 8 to 10 inches thick.

	T	1	1		CASI	NG			[WA	ma Le	9.L		1	
WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING I'NI T	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)		DATE OF ASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* X₩-29-40-90	L. B. Hester		1950	40	6	40	Qal	1,902	14.49	Dec.	5, 1969	N	N	Reported strong well. Water reported encountered in sand and gravel at 22 to 30 ft.
* 90	? Tom Wallace			70	5		Po	1.912	47.9	May	5, 1970	с, w	s	
90	do do			46	5		Qal	1,903	22.01		do	N	N	
* 90	L. B. Hester			Spring			Pc	1,915	+		do	Flows		Estimated flow 1 to 2 gpm.
47-30	W. C. Perkins		1945	165	8		Psa	2,180	44.30	Dec.	11, 1969	с, w	N	Reported strong well. Water reported from sand near bottom.
* 60	L. A. Cook		1910	25	6	25	Кf	2,458	13.85 13.82	Dec. Jan,		N	N	Reported weak well.
60	do		1912	40	6		Ka?	2,459	13.59 12.65		12, 1969 13, 1971	N	N	Reported very weak well. Water reported at 30 ft.
60	do		1958	260	6	260	Ка	2,460	12		dø	С, Е, 1	D, S	Water reported from sand at approximately 200 ft below the top of the red beds.
* 60	do			Spring			Κf	2,439	+	Dec.	12, 1969	Seeps		Reported never to have been dry. Water seeps from base of white limestone.
* 90	Elm Cattle Co.			280	4		Ka	2,448				с, w	s	
* 90:	do			Spring			Kf	2,438	+	Jan.	16, 1970	Seeps		Reported to fail during prolonged drought.
* 90:	do			Spring			Kf	2,406	+		do	Flows		Good spring. Flow in excess of 5 gpm.
* 904	do			Spring			Κf	2,400	+		do	Flows		Estimated flow 10 gpm.
* 90	do			Spring			KÍ	2,440	+		do	Seeps		
* 48-20	B. H. Riney			20			Qal	1,966	5.30	Nov.	12, 1969	J, E, 1/3	D	Dug well. Water reported from break in clay.
20:	do	B. H. Riney	1938	13			Qa1	1,968	7,57		do	N	N	Dug well, reported weak. Water reported from break in clay.
201	L. B. Hester	A. L. Hicks	1969	60	5	60	Pc	1,945	25	Aug.	25. 1969	c, w	s	Reported yield 12 gpm. Water reported from clay. Casing slotted at 30 to 60 ft. 3
204	Jimmie Guthrie			20			Qal	1,966	7.68	Mar.	13, 1970	Cf, E, 2	S, Irr	Dug well. Reported yield 100 gpm from sand and gravel.
205	do				5		Pc	2,003				с, w	N	Reported yield 3 gpm.
* 206	do			Spring			Qu	1,980	+	Mar.	13, 1970	Flows	S, Irr	Flows about 3 gpm from pink sand and predominately limestone gravel, 10 ft bolow surrounding land surface.
401	W. C. Perkins		1949	50	8		Ka?	2,462				N	N	Reported weak well. Caved at about 19 ft.
402	do		1950	40	6		Ka?	2,460				Ј, Е, 1	D	Reported strong well.
* 403			1930	39			Ka?	2,459	14.73 14.15	Dec. Jan.		с, w	s	Do.
404	do		1930	85	6		Ka?	2,470				N	N	Reported weak well.
405	do			39	7		Ka?	2,475				Ν	N	Reported very weak well.
* 406	do		1950	100	6		Ka?	2,456	20.21 4 17.63 4		11, 1969 13, 1971	с, w	S	

	r				CASI	NC			WA	TER LEVEL			
WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
XW-29-48-601	Edgar Davis	B. H. Riney	1906	270	4		Ка	2,402	205.7	Feb. 17, 1970	C,W	S	Reported yield 15 gpm.
* 602	do		1946	230			Ка	2,387			с, w	S	Reported yield 30 gpm.
603	do	Robert Higgins	1969	314	7	310	Ка	2,453	250	Jan. 18, 1969	C, W	S	Reported yield 20 gpm. Water reported from sand and gravel at 200 to 300 ft. Casing perforated from 260 to 300 ft. 3
604	do			195			Ka	2,350			С, Е, 1	s	Reported poor well.
* 605	do		1957	260	6	260	Ка	2,380			C, E, 1/2	D	Reported yield 30 gpm. Water reported from 160, 192, and 220 ft. One joint of slotted pipe in each of the water-producing zones.
* 701	W. C. Perkins			Spring	-		Kf	2,418	+	Dec. 11, 1969	Flows		Reported to stop flowing in dry weather. Estimated flow 1 gpm from limestone.
702	Elm Cattle Co.			300	4		Ka	2,430			с, w	D, S	Reported yield 7 gpm.
* 703	do			Spring			Кf	2,382	+	Jan. 16, 1970	Flows	N	Estimated flow 10 gpm.
* 704	do			Spring			Кt	2,355	+	do	Seeps	••	
* 705	do			260	4		Ка	2,343			с, w	D, S	Reported yield 7 gpm.
801	Edgar Davis		1961	135	7	135	Qal, Ka	2,280	14.3 14.05	Feb. 19, 1970 Jan. 13, 1971	Sub, E, 5	Irr	Reported yield 30 gpm. Water reported at 110 ft. Casing slotted from 110 to 130 ft.
802	do		1961	115	8	115	Ка?	2,260	54.9 55.4	Feb. 13, 1970 Jan. 13, 1971	Sub, E, 5	Irr	Reported yield 40 gpm. Water reported at 105 ft. Casing slotted from 105 to 115 ft.
803	do	Robert Higgins	1961	115	8	115	Qal, Ka	2,255	9.4 9.35	Feb. 13, 1970 Jan. 13, 1971	Sub, E, 5	8	Reported yield 80 gpm. Water reported at 95 ft. Casing slotted from 95 to 115 ft.
804	do	**	1961	95	8	95	Ka?	2,255	38.6 39.30	Feb. 13, 1970 Jan. 13, 1971	Sub, E, 5	Irr	Reported yield 70 gpm, Water reported from 45 ft and sand at 80 to 95 ft. Casing slotted at 45 ft and 80 to 95 ft.
805	do		1930	160			Ка	2,342	140		с, w	S	Reported good well.
806	do	Edgar Davis	1950	335	6	335	Ka	2.447			c.w	S	Reported yield 25 gpm, Water sand reported at about 315 ft.
* 807	do			Spring			Kf	2,350	+	Feb. 13, 1970	Seeps		
* 808	do			Spring			Кſ	2,375	+	do	flows		Estimated flow 0.2 gpm.
809	Sam R. Cox, Jr. Estate		1946	120	5	120	Ка	2,324	73.9 74.02	Feb. 18, 1970 Jan. 16, 1971	с, w	s	Reported strong well.
901	Edgar Davis			100	4	100	Ka?	2,322	85	Feb. 13, 1970	C, W	S	Reported yield 15 gpm, Sand reported at 85 ft. Casing slotted from 85 to 100 ft.
902	do		1960	300	10		Ка	2,346			c, w	S	Reported yield 30 gpm. This is an oil test plugged back and completed as a water well.
903	Sam R. Cox, Jr. Estate			175	5	175	Ka	2,391	162.2 156.00	Feb. 18, 1970 Jan. 16, 1971	C, W	S	Reported strong well.
55-601	W. L. Murphy			80	6		Ka	2,275	45.5 45.48	Mar. 13, 1970 Jan. 12, 1971	C.W	s	Reported good well.
* 602	do		1946	75	7	75	Ka	2,275	41.0 36.83	Mar. 13, 1970 Jan. 12, 1971	C, W	D, S	Reported good well. Water reported from sand.

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				окрен	CAS	140	ł	ALTITUDE	DELOW WA	TER LETTER	-		
WELL	ØWNER	DRILLER	DATE COMPLETED	OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING FNIT	OF LAND SURFACE (ft)	LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
∴ XW-29-55-0			1946	75	7	75	Ка	2,281	27.45 22.84	Mar. 13. 1970 Jan. 12, 1971	c, w	S	Reported good well.
k (04 do			35			Ка	2,279	2.30 7.19	Mar. 13, 1970 Jan. 12, 1971	c. w	s	Dug well. Reported to pump dry during drought.
÷ (02 William H. Lynn		1921	140	18	80	Реа	2,163	37.3 35.73	Feb. 23, 1939 Nov. 17, 1969	ς,Ψ	s	Reported yield 8 gpm from sand and gravel at 80 ft. Well caved and was re-drilled. Well 156
56-1	01 Virgil Sears		1930	60	6	60	Ka?	2,284	40 13.50 12.26	Feb. 28. 1939 Nov. 13, 1969 Jan. 12, 1971	c.w	Ν	Nug well. Reported good well. Well 147. 8
- 1	02 Elm Cattle Co.			Spring			Кf	2,398	+	Jan. 16, 1970	Sceps		
. 1	03 do			Spring			Кf	2,393	+	do	Seeps		
1	04 do	R. O. Kilpatrick	1931	300	4		Ка	2,400			c, w	ŝ	Keported yield 7 gpm.
1	05 do			Spring			Kf	2,359	+	Jan. 15, 1970	Flows		Estimated flow 5 gpm.
1	do do			Spring			Кf	2,410	+	do	Seeps		
1	07 do			Spring			Kf	2,356	+	do	Seeps		
1	06 do			300	4		Ka	2,435			с, w	s	Reported yield 7 gpm.
1	09 do			Spring			К£	2,397	+	Jan. 15, 1970	Seeps		
1	10 Edgar Davis			Spring			Кf	2,393	+	Feb. 19, 1970	Secps		Reported to fail during drought.
2	Dl Evelyn B. McGehee			Spring			Кf	2,360	+	Nov, 5, 1969	Flows	N	Reported to flow 20 gpm. Water from a depth of 8 ft. Spring 146. &
2	Dick Sears			68	6	42	Ka?	2,440	38.90	Nov. 13, 1969	с, w	s	
2)3 Edgar Davis		1948	160	5		Ka	2,379	140	Feb. 13, 1970	c, w	N	Reported good well.
2	do do			Spring			Kf	2,380	+	do	Flows		Estimated flow 10 gpm.
2	oh 5			Spring			Kf	2,380		do	Flows		Estimated flow 5 gpm.
2	16 Sam R. Cox, Jr. Estate	~~	1931	151	6		Ka	2,450	65	Feb. 28, 1939	J, E	D, S	Reported yicld 20 gpm. Water reported from 60 f An old oil test drilled in the 1930's. Well 144. 8
20			1954	90	5	90	Ka?	2,427	60 16.6 12.45	Aug. 10, 1961 Feb. 18, 1970 Jan. 16, 1971	C, W	S	Reported good well. Pipe reported perforated at bottom 20 ft.
20	8 do			Spring			ĸſ	2,381	+ .	Feb. 18, 1970	Flows		Cottonwood Spring estimated flow 10 gpm. Reported not to have failed during the last 30 years.
30	1 A. P. Tice, Guardian		1961	125	5		Ка	2,321	81.8 82,42	Feb. 18, 1970 Jan. 15, 1971	c, w	s	Reported strong well.
30				Spring			Kf	2,317	+	Feb. 18, 1970	Flows		Estimated flow 10 gpm.
30	3 do			125	6		Ka	2,383			с, w	s	Reported strong well.
30	4 Sam R. Cox, Jr. Estate	Continental Oil Co.	1950	280	5	280	Ка	2,432	179.6	Feb. 18, 1970	с, w	S	Reported good well. This is an old core hole. Water sand reported at 250 to 280 ft. Perforated casing from 250 to 280 ft.

Table 5Records o	f Selected Water	• Wells and Springs	in Taylor County	and Adjacent AreasContinued
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					CASI	NG				TER LEV	6L			
WELL	OWNER	DRILLER	DA TE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)		ATE OF SUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* X₩-29-56-501	A. C. Sears		1937	200	16	200	Ka	2,340	80.17 78.83		13, 1969 12, 1971	c, w	N	
* 502	Mrs. Clyde Sears, Sr.	Robert Higgins	1959	72	6	70	Ka	2,263				с, w	D, S	Water reported from sand.
* 503	Lail Ranch		1930	90	5		Ka	2,321				с, ₩	s	Reported good well.
* 504	do			Spring			Kf	2,338	+	Mar.	10, 1970	Flows		Estimated flow 15 gpm.
* 601	do			9 0	5		Ka	2,309				с, w	S	Reported strong well.
* 701	Leon Shedd	Robert Higgins	1968	80	5	80	Psa	2,148	14.38	Oct.	23, 1969	J, E, 1-1/2	D	Yield reported 3 gpm. Some water reported from sand and gravel at 11 to 19 ft. Main water reported from sand and gravel at 30 to 38 ft, and possible water trom sand at 62 to 64 ft. Casing slotted from 38 to 78 ft. 3
* 702	Shep Community Center		1913	90	6		Psa	2,170	13.9 13.81	Feb. Oct.	24, 1939 22, 1969	с, w	D	Water reported from sand and gravel. Well 160. $\underline{\beta}$
* 703	Shep Church of Christ			20			Psa	2,148	13.4 12.15		10, 1939 22, 1969		N	Well 162. 84
* 704	W. C. Bradshaw		1920	22			Psa	2,117	19.0 17.15		24, 1939 17, 1969	J, E, 1/2	D, S	Dug well. Water reported from sand and gravel at 21 ft. Well 171. 8
* 801	Mrs. H. A. Sheppard		1950	125	6	125	Pc	2,195				c, w	D	
802	Alton Roberts			90	5		Ka	2,288	79.2	Mar.	10, 1970	с, w	S	Water reported from sand.
* 901	Lail Ranch		1909	48	5		Ка	2,143	33.5 19.48	Jan.	do 12, 1971	с, w	S	Reported strong well.
* 902	do			90	5		Ka	2,230				с, w	S	Reported good well.
903	Alton Roberts		1950	60	5		Ka	2,212	59.8	Mar.	10, 1970	с, w	N	Water reported from sand.
* 64-301	do		1950	50	5	•	Ka	2,175	21.4		do	с, w	S	Do.
* 30-25-702	H. B. Robertson	Robert Higgins	1968	70	6	23	Pc, Pvb	1,838				Sub, E, 1/2	D	Reported yield 30 gpm. Water reported at 28 to 29 ft (seep), 43 to 44, and 62 to 63 ft.
* 703	do		1904	120	6		Pc, Pvb	1,837	20	Dec.	5, 1969	c, w	S	Reported yield 10 gpm.
* 704	do	Robert Higgins	1948	80	6	25	Pc, Pvb	1,830	11.3		do	J, E	D	Reported yield 15 gpm. Water reported at about 44 and 63 ft.
* 705	Robert Higgins	do	1961	90	11	60	Qs, Pc	1,806	9.75 4	Мау	6, 1970	Sub, E, 5	Irr	Reported yield 100 gpm. Water reported at 20 to 38 ft from sand and gravel, and at 54, 68, and 85 ft from clay. Casing perforated from 20 to 60 ft.
* 706	do	do	1948	80	6	80	Qs, Pc	1,810	9		do	J, E, 3/4	D	Reported yield 60 gpm. Water reported from gravel and sand at 20 to 38 ft and from clay at 54 and 68 ft. Casing perforated from 20 to 60 ft.
* 707	do	do	1948	40	7	40	Qs	1,810	9		do	с, w	S, Irr	Reported yield 30 gpm. Water reported at 20 to 38 ft from gravel. Casing perforated at 15 to 40 ft.
708	do	do	1954	70	7	25	Qs, Pc	1,821	13.28		do	N	N	Reported yield 30 gpm. Water reported at 35 ft from sand and gravel, and at 48 ft and 70 ft from clay.

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	WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
	709	Orin Higgins	Robert Higgins	1963	25	6	25	Qs	1,800	4.74	May 3, 1970	н	S	Reported yield 10 gpm. Water reported at 25 ft from sand and gravel. Perforated casing from 10 to 25 ft.
	711	do	do	1963	70	7	70	Qs, Pc	1,807	3.83	May 6, 1970	Sub, E, 2	Irr	Reported yield 60 gpm. Water reported from sand and gravel at 20 to 40 ft and from clay at 51 and 70 ft. Perforated casing from 30 to 70 ft.
		do	do	1952	90	7	60	Qs, Pc	1,807			J, E, 1	D, S	Reported yield 60 gpm. Water reported from sand and gravel at 20 to 40 ft and from clay at 51 and 73 ft. Perforated pipe from 40 to 60 ft.
"	712	do			40	5		Pc	1,808	4.57	May 6, 1970	с, w	S, Irr	
	713	do	Robert Higgins	1954	70	7	20	Qs, Pc	1,808	4.9	do	J, E, 1-1/2	S, Irr	Reported yield 45 gpm. Water reported from gravel at 28 ft and from clay at 53 and 64 ft.
	714	do	do	1955	80	7	80	Qa, Pc	1,809	5.39	đo	N	N	Reported yield 60 gpm. Water reported at 25 ft from gravel and at 50 and 61 ft from clay. Perforated casing from 40 to 80 ft.
	715	Bill Black	do	1964	38	7	38	Qs	1,808	5.84	May 7,1970	J, E, 1/2	D	Reported yield 20 gpm. Water reported at 18 and 31 ft. Perforated casing from 23 to 38 ft.
		do	do	1967	69	7	38	Qs, Pc	1,802	4.10	do	Sub, E, 3	Irr	Measured yield 41 gpm on June 26, 1970. Water reported at 8 to 38 ft from sand and gravel and at 52 to 53 ft. Perforated casing from 22 to 35 ft. $\frac{3}{2}$
*	27-706	H. E. Neas	Johnson & Henderson	1966	33	12	33	Qa1	1,650	11.43	Apr. 6, 1970	Sub, E, 6	Irr	Reported initial yield 260 gpm. Casing slotted at 27 to 30 ft.
	707	do			18			Qal	1,652	9.87	do	N	N	Dug well.
*	708	City of Abilene	Jack Leonard	1969	32	5	32	Qa 1	1,667	15.0	Apr. 20, 1970	N	ļ/	Reported fair well. Water reported from sand and gravel at 26.5 to 30.5 ft. Perforated casing at 25 to 31 ft. $\underline{3}$
	709 710	do	do	1969	34	5	34	Qal	1,666	15.45	do	N	<u>1</u>	Reported fair well. Water reported from sand and gravel at 12 to 33 ft. Perforated casing from 16 to 34 ft. 3
Î	711	do do	do	1969	15	5	15	Qal	1,660	11.13	do	N	<u>l</u> y	Reported poor well. Water reported from sand and gravel at 11.2 to 13.8 ft. Perforated casing from 9 to 15 ft. $\underline{\mathcal{Y}}$
			do	1969	26	5	26	Qa1	1,661	16.78	do	N	Ţ	Reported fair well. Water reported from sand and gravel at 9 to 23 ft. Perforated casing from 16 to 25 ft. 3
*	712	do	do	1969	32	5	32	Qal	1,662	18.65	do	N	Ţ	Reported fair well. Water reported from gravel with sand at 29.2 to 30.2 ft. Perforated casing from 26 to 32 ft. 3
	713	do	do	1969	32	5	32	Qa1	1,662	11,10	do	N	<u>l</u> i	Reported excellent well. Water reported from sand and gravel at 23 to 31 ft. Perforated casing from 17 to 29 ft. $\underline{3}$
*	714	do	do	1969	34	5	34	Qa1	1,664	12.54	do	N	Ŀ	Reported excellent well. Water reported from sand and gravel at 22.5 to 32.8 ft. Perforated casing from 20 to 32 ft. \underline{y}
	715	do	do	1969	37	5	37	Qal	1,666	14.49	do	N	у	Reported excellent well. Water reported from gravel with some sand at 32.4 to 36.7 ft. Casing perforated from 31 to 37 ft. 3
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	WELL	OWNER	DRILLER	DATE. COMPLETED	OEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-	-30-27-716	City of Abilene	Jack Leonard	1969	38	5	38	Qal	1,667	14.39	Apr. 20, 1970	N	Ţ,	Reported good well. Water reported from sand with some gravel at 15.4 to 27.5 ft. Casing perforated from 20 to 35 ft. <u>3</u>
	717	do	do	1969	41	5	41	Qal	1.671	19.82	do	N	<u>1</u>	Reported good well. Water reported from sand and gravel at 33.6 to 38.8 ft. Casing perforated from 34 to 40 ft. 3
	718	do	Trinity Engineering Testing Corp.	1969	37	5	37	Qal	1,665	17.70	do	N	Ţ	Reported good well. Water reported from sand at 16.8 to 17.5 ft and sand and gravel at 28 to 30 ft. Casing perforated from 26 to 32 ft. Well was cored. 3
*	719	do	do	1969	36	5	36	Qa1	1,666	17.15	do	N	Ŀ	Reported fair well. Water reported from sand and gravel at 30.5 to 35.8 ft. Casing perforated from 29 to 35 ft. Well was cored. 3
*	720	do	do	1969	23	5	23	Qa1	1,665	15.87	do	N	Ŀ	Reported fair well. Water reported from sand and gravel at 15 to 21.2 ft. Casing perforated from 15 to 21 ft. Well was cored. 3
	721	do	do	1969	30	5	30	Qa1	1,664	15.48	do	N	y	Reported poor well. Water reported from sand and gravel at 26 to 28.8 ft. Casing perforated from 24 to 30 ft. Well was cored. 3
#	912	Mrs. W. W. Reed		1929	31			P1	1,726	11,95	Apr. 7, 1970	Sub, E, 3/4	S	Dug well. Reported good well.
*	913	do			30			P1	1,727	11.77	do	c, w	s	Do.
	914	do			30			P1	1,735	17.83	do	N	N	Do.
*	33-101	R. F. Perry	Robert Higgins	1968	35	5	35	Qal, Pc	1,779	10	Sept. 22, 1968	Sub, E, 1/2	D	Reported yield 60 gpm. Water reported from gravel at 12 to 15 ft and from sand at 28 to 30 ft. Casing slotted at 11 to 33 ft. <u>3</u>
*	201	do	do	1963	42	7		Qal, Pc, Pvb	1,775	5.39 4.30 10.30 6.85	Oct. 17, 1969 Apr. 15, 1970 July 20, 1970 Jan. 5, 1971	Sub, E, 3	Irr	Yield reported 100 gpm. Water reported from gravel and sand at 11 to 16. and 22 to 28 ft, and at 38 to 39 ft. Casing slotted from 15 to 40 ft.
*	501	Virgil Patterson	Robert Higgins	1961	42	6	42	Pvb	1,822	9.71	May 20, 1970	J, Е, 1/2	D	Reported yield 7 gpm. Water reported at 24 ft.
	502	do			38	4	38	Pvb	1,820	21.13 4	do	с, w	S	Reported yield 5 gpm. Casing perforated from 8 to 38 ft.
*	503	do			30	6		Pvb	1,821	4.68	do	N	N	
*	504	do			50	7		Pvb	1,835	11,59	do	C, W, J, E 3/4	D	
	505	do						Pvb	1,831	4.84	do	с, w	s	
*	506	R. D. Ely		1944	60	6		Pv	1,804	14,98	June 13, 1970	с, W	s	Reported yield 3 gpm in 1947. Water reported between 30 and 40 ft.
*	601			1900	35			Qal, Pv	1,792	13.2 1.04	Apr. 24, 1939 Apr. 14, 1970	N	N	Dug well. Well 22. g
	602	Mrs. A. V. Teaff			35			Qal, Pv	1,827	14.8 1.13	June 6, 1939 June 15, 1970	N	N	Dug well. Well 36. 👌 Water reported salty.
*	603	do			31			Qal, Pv	1,829	3.3 2.81	June 6, 1939 June 15, 1970	с, w	N	Dug well. Well 37. <u>B</u>

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	WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
XW	- 30 - 33 - 604	Johnny Teaff			45	б		Qal, Pv	1,829	12.1 4.63	June 6, 193 June 15, 197	9 J, E, 0 1/2	N	Well 35-A. 8 Water reported too salty for domestic use.
*	605	do			42			Qal. Pv	1,827	9.0 .46	June 6, 193 June 15, 197		N	Well 35. 8
*	34-301	Mrs, Ramantha Dubbs	R. L. McKelvy	1965	32	5	32	Qa1	1,698	12.87	Apr. 10, 197	0 Cf, E, 1/2	D	Reported adequate water for yard use. Casing perforated from 20 to 32 ft. Red sand reported at 22 to 26 ft and gravel at 26 to 27 ft. $\underline{3}$
*	302	Southwest Enterprises			28	7	28	Qa1	1,692	9.50	Apr. 14, 197	0 C, W	N	Water reported at 28 ft.
*	303	do			24			Qa1	1,690	18 9.27	Aug. 14, 193 Apr. 14, 197	9 J.E	N	Dug well. Water reported at 24 ft. Well 28. <u>8</u>
*	304	do	Jack Leonard	1969	33	16	33	Qal	1,693	11.65	do	Sub, E, 1-1/2	Irr	Reported yield 60 gpm. Water reported from gravel at 24 to 30 it. Casing slotted from 25 to 33 ft. <u>3</u>
	305	do	do	1969	34	16	34	Qa1	1,692	11,45	do	Sub, E, 1-1/2	Irr	Reported yield 90 gpm. Water reported from gravel at 23 to 31 ft. Casing slotted from 26 to 34 ft. 3
	306	Southwest Enterprises	do	1969	34	16	34	Qa1	1,692	11.47	do	Sub, E, 1-1/2	Irr	Reported yield 50 gpm. Water reported from gravel at 26 to 32 ft. Casing slotted from 26 to 34 ft. <u>3</u>
*	307	dø	do	1969	32	7	32	Qa1	1,689	9.87	do	Sub, E, 1-1/2	Irr	Reported yield 70 gpm. Water reported from gravel at 24 to 30 ft. Casing slotted from 24 to 32 ft. $\underline{3}$
*	401	J. C. Barley		1947	58	6		Pv	1,791	4.56	do	N	N	Water reported at 34 ft.
*	501	J. R. Stuard	Jack Leonard	1969	33	9	33	Qa1	1,720	10.21 4	Apr. 16, 193	0 R, E, 1/3	D	Reported yield 8 gpm. Water reported from sand and gravei at 14 to 26 ft. Casing slotted from 25 to 33 ft. <u>3</u>
π	502	Richard L. Bowman	do	1969	32	9	32	Qal	1,738	14.47	do	Sub, E, 1/2	D	Reported yield 25 gpm. Water reported from grave at 18 to 26 ft. Casing slotted from 26 to 32 ft. 3
*	601	Mrs. M. R. Caton						Par?	1,762	5.90	Apr. 3, 197	0 N	N	Dug well.
	602	W. L. Callan			39	5		Qal	1,745	17.32	do	Cf, E	D	
*	603	Raymond J. Smith	G-M Drilling	1965	30	9	30	Qa1	1,713	14.55	Apr. 10, 197	0 Cf, E, 3-1/2	Ind	Reported yield 20 gpm. Water reported from sand and gravel at 13 to 22 ft. Casing perforated from 13 to 23 ft.
*	801	Gordon Asbury, Jr.	Jim Rae	1969	45	4	45	Qa1	1,807	30.00	May 6, 19	0 N	N	Estimated yield 3 to 4 gpm. Water reported from gravel at 26 to 28 ft.
*	802	do	McCarrell & Sons	1968	51	6	51	Qa1	1,805	24.25	do	N	N	Reported yield 7 gpm. Water reported from gravel at 33 to 35 ft; gravel also reported at 28 to 33 ft. 3
*	803	do			39			Qa1	1,799	19.1 16.96	Mar. 13, 193 May 6, 19		D, S	Dug well. Well 92. <u>8</u>
*	901	Richard W. Sharp, Jr.	Jack Leonard	1969	33	13	33	Qa1	1,783	12.22	May 13, 19	0 Sub, E	Irr	Reported yield 70 gpm. Water reported from gravel at 18 to 29 ft. Casing slotted from 29 to 33 ft. 3
*	902	do	do	1969	29	13	29	Qa1	1,780	13.21	do	Sub, E	Irr	Reported yield 20 gpm. Water reported from sand and gravel at 13 to 22 ft. Casing slotted from 25 to 29 ft. 3

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WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)		ATE OF SUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
XW-30-35-101	A. F. McCarty			30	5	30	Qal	1,694	28.30	Apr.	10, 1970	с, w	D	Water reported from gravel. Casing perforated from 20 to 30 ft.
201	Charles G. Sanders	R. L. McKelvy		60	5	60	Par	1,686	3.0	Apr.	6, 1970	с, w	s	Reported yield $1/2$ gpm. Casing slotted from 56 to 60 ft.
202	J. D. Self			60	6		Par	1,682	31,09		do	c, w	S	Reported weak well.
301	V. B. Reeves		1910	31			P1	1,764	Dry 16.99	July Apr.	12, 1939 7, 1970	с, w	N	Dug well. Reported fair well. Water reported a 29 to 31 ft. Well 137. g
401	E. L. Ganey		1945	15			Qal	1,690	10,54	Apr.	8, 1970	с, w	s	Reported fair well.
402	R. P. Haam			14			Qal	1,709	5.11		do	Cf, E, 1/2	D	Dug well. Reported to have never been pumped dry.
403	do			19			Qal	1,712	12.13		do	Cf, E, 3/4	D	Dug well.
404	do			14			Qa 1	1,710	8,40		do		N	Do,
601	Taylor County			20			P1	1,771	2.9 1.50		28, 1939 7, 1970	N	N	Dug well. Well 132. Bj
602	B. W. Brewer			16			P1	1,776	+		do	c, w	S	Dug well.
701	I. N. Deaton			24			Qa 1	1,735	14.40	Apr.	8, 1970	Cf, E, 1/3	D	Do.
702	J. E. Burk	J. E. Burk	1957	69	6	69	Qal, Par	1,747				с	N	Water reported at 20 ft from gravel. Gravel also reported at 4 and 40 ft. Casing perforate from 49 to 69 ft.
703	đo	do	1958	74	7	74	Qel, Par	1,744	6.65	Apr.	9, 1970	N	N	Water reported at 20 ft from gravel. Gravel also reported at 4 and 40 ft. Casing perforat from 54 to 74 ft.
704	đo	do	1958	69	6	69	Qal, Par	1,746	9.11		do	с, w	N	Reported yield 3 barrels per day. Septic tank is 8 ft east of well. Water reported at 20 ft gravel reported at 4 and 40 ft. Casing perforated from 49 to 69 ft.
705	do	do	1955	64			Qal, Par	1,746	9.49		do	Cf, E, 1/3	N	Dug well to 34 ft. Reported weak well. Septic tank is 10 ft southeast of well.
41-201	W. G. Drummond	Robert Higgins	1966	108	6	108	Pc, Pv	1,965	44.4	June	16, 1970	Sub, E, 5	S, Irr	Reported yield 70 gpm. Casing slotted from 48 to 52 ft and near bottom.
202	do		1930	120	4	30	Pc, Pv	1,967	23.5		do	с, w	s	
203	White's Mines, Inc.	Robert Higgins	1966	145	6	143	Pc, Pv	1,980	79.3 <u>4</u>	June	17, 1970	Sub, E, 3	Ind	Reported yield 50 gpm. Water reported from re- sand at 60 to 61 ft (tight) and 129 to 132 ft Casing slotted from 50 to 80 and 100 to 140 fr
204	do	Jack Leonard	1969	136	5	136	Pc, Pv	1,980	123.10 <u>4</u>		do	Sub, E, 3	Ind	Reported yield 50 gpm.
301	M. D. Richards			40			Q a 1	1,910	36.5 8.80	Mar. Dec.	6, 1939 4, 1969	с, w	N	Dug well. Reported to have failed frequently. Water reported from sand and gravel. Well 48.
302	W. G. Drummond		1930	22			Qa 1	1,880	9.3 6.94		6, 1939 16, 1970	J, E, 1	D, S	Dug well. Reported yield 30 gpm. Water report from sand and gravel. Well 47. By
401	Edgar Davis	Robert Higgins	1969	270	6	270	Ka	2,387				с, w	s	Reported yield 20 gpm. Water reported at 240 Casing slotted from 235 to 270 ft.

Table 5Records of Selected Water Wells	and Springs in Taylor County and Adjacent AreasContinued	

	r		T			CASI	NG				ER LEVEL		1	
	WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
x	W-30-41-402	Edgar Davis	Robert Higgins		240			Ka?	2,324			c, w	s	Reported poor well.
	501	W. G. Drummond		1956	124	4	42	Pv	2,040	27.2	June 16, 1970	J, E, 1/2	s	Reported yield ll gpm. Main water reported at 42 ft.
*	701	Edgar Davis	West Central Drilling Co.		220	9		Ka	2,304			с, w	s	Reported good well. A converted oil test, reportedly drilled in the late 1940's.
	702	do		1948	220	8		Ka	2,306			с, w	s	Reported yield 20 gpm. Water reported at 195 to 200 ft.
*	703	do			Spring			Ka	2,227	+	Feb. 17, 1970	Flows		Estimated flow 0.2 gpm. Water from sand.
*	802	Fred White	Robert Higgins	1959	145	6	145	Ka	2,230	85	Aug. 7, 1970	C, W	D, S	Water reported at 85 ft. Well screen from 115 to 145 ft.
*	42-201	Farr Estate	Jack Leonard	1965	44	12	44	Qal	1,821	18.18	Dec. 20, 1969	Cf(2); E,2(2)	lrr	Water reported from sand and gravel at 20 to 41 ft. Measured yield 46 gpm July 3, 1970. Casing perforated from 40 to 44 ft. Two centrifugal pumps and two motors in this well. $\underline{7}$
	202	do	do	1946	43	10	43	Qal	1,821	26.71	do	T, G, 20	Irr	Water reported from sand and gravel. Reported yield 100 gpm. Well screened from 39 to 43 ft.
*	203	do	do	1945	45	12	45	Qa1	1,824	30.68	do	Sub, E, 3	Irr	Water reported from sand and gravel at 32 to 42 ft. Measured yield 51 gpm July 3, 1970. Casing perforated from 41 to 45 ft. 7/
*	204	do	do	1947	43	8	43	Qal	1,822	24.61	do	Sub, E, 2	D, Irr	Water reported from sand and gravel at 30 to 40 ft. Reported yield 75 gpm. Perforated casing from 38 to 43 ft.
	205	W. T. Ohlhausen			32	6	32	Qal	1,825	21.08	May 13, 1970	J, E, 3/4	D, S	Dug well to 26 ft. Reported yield 400 gpm. Water reported at 20 ft from sand and gravel.
*	206	do	Henderson & Johnson	1965	32	12	32	Qal	1,821	9.49	do	т, е, 15	lrr	Reported yield 400 gpm. Water reported at 12 ft and 32 ft (main supply), from sand and gravel. Casing perforated at 12 to 32 ft.
*	207	V. L. Ohlhausen	V. L. Ohlhausen	1964	11			Qu	1,893	6,98	do	J, E, 1/3	D	Dug well. Water reported from gravel at 8.5 ft. Perforations in bottom ring.
*	208	J. L. Ohlhausen	City of Abilene	1927	38			Qa 1	1,841	Dry 17.75	Mar. 23, 1939 May 13, 1970	N	N	Dug well. Reported yield 100 gpm. Well 105. &
*	209	Leonard Camp	Johnson & Henderson	1967	44	11	44	Qal	1,812	25.34	do	J, E, 1	D	Reported yield 145 gpm. Water reported from sand and gravel at 31 to 42 ft. Slotted casing at 30 to 44 ft. <u>3</u>
	301	W. G. White			180	7		Par	1,845	107.5	Apr. 9, 1970	N	N	Well reported has not been dry in 24 years.
	401	Bill Allen			65			Ка	2,150	32.60 32.00	Dec. 15, 1969 Feb. 24, 1971	c, w	s	Dug well. Water reported above red beds.
	402	do	Higgins & Malone	1952	205	6	205	Ка	2,287	171.1 169.5	Dec. 15, 1969 Feb. 24, 1971	c, w	S	Water reported above red beds. Perforated casing from 170 to 200 ft.
	403	do	do	1950	190	6	190	Ка	2,309	102.65	Dec. 15, 1969	C, W	s	Water reported above red beds. Perforated casing from 95 to 110 and 170 to 185 ft.
	404	do	do	1950	65	6	65	Ка	2,178	51.47 50.6	Dec. 15, 1969 Feb. 24, 1971	с, w	D, S	Water reported above red beds. Casing perforated from 60 to 65 ft.

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		ļ			DEPTH	CAS	ING				TER LEVE	L			
	WELL	OWNER	DRILLER	DATE COMPLETED	OF	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)		TE OF UREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* X1	7-30-42-501 502	L. D. Robinson	Henderson & Johnson	1966	42	11	42	Qa 1	1,641	13	Dec.	17, 1969	T, E, 10	LL	Water reported from gravel and sand at 32 to 39 ft. Measured yield 193 gpm June 26, 1970. Casing slotted from 30 to 42 ft. 32 $T_{\rm c}$
	502	J. E. McCarty	J. E. McCarty	1957	41	12	41	Qa 1	1,861	18	Dec.	19, 1969	Cf, E, 7-1/2	D, S, Irr	Dug well. Water reported from sand and gravel topped at 32 ft. Reported yield 300 gpm. Casing slotted from 26 to 41 ft.
±		L. D. Robinson		1952	23			Qa 1	1,841	11.36	Dec.	17, 1969		N	Dug well. Water reported from gravel.
a	504	A. B. Thornton			35			Qal	1,845	19.98	J a n,	28, 1970	J, E, 3/4	D. S	Dug well. Reported yield 200 gpm. Water reported from sand and gravel.
ĸ	701	W. L. Marshall, Jr.	Jack Leonard	1967	50	10		Qa 1	1,845	18.44		do	т, е, 10	Irr	Reported yield 350 gpm. Water reported from sand and gravel topped at 26 ft. Well screene from 46 to 50 ft.
	701				19			Qa 1	1,921	14.30	Feb.	12, 1970	N	N	
	801	do Santa Fe Railroad			12			Qa 1	1,918	3.59		do	N	N	
	43-201			1909	30			Qa 1	1,915	13.97	Mar.	27, 1970	Т, Е, 5	Р	Dug well, serviced by two vertical turbine pumps which together are reported to produce approximately 140 gpm.
	43-201	Bob E. Warren		1964		5		Par	1,859	11.45	Apr.	2, 1970	Cf, E, 1/3	D	Reported yield 5 gpm.
	202	J. Willard Vinson		1909	35			Par	1,820	24.1 4.21		26, 1939 2, 1970	N	N	Dug well, Water reported from sand, Well 124.
	203	Roy Manahan	Roy Manahan	1935	30			Qa1	1,780	4.31		do	J, E, 1	D, S	Dug well. Reported yield 40 gpm, Water reported from 2 to 3 ft of sand topped at 22 ft.
	601	Gene Franklin			25			Qa1	1,858	5.20	May	12, 1970	c, w	N	Dug well.
	602	do		1905	20			Ka	2,012	13.67 13.53		do 14, 1971	J, E, 1/2	D	Dug well. Water reported from sand at approximately 18 ft. Perforation in bottom ring.
	701	Miss Beth Fletcher		1942	256	7	256	Ка	2,270	250	Mar. 2	25, 1970	C, W	S	Reported good well. Perforation reported in bottom 2 joints of casing.
	702	Roy Manahan	D. W. Thompson	1963	280	7	280	Ka	2,265	230	Apr.	2, 1970	c, w	s	Reported yield 30 gpm. Water reported from sand at 245 to 262 ft. Casing perforated at 246 to 280 ft. 3
	703	do			260	5		Ка	2,275	225.9 220.15	d Jan. 1		c, w	D, S	Reported good well.
	801	Miss Beth Fletcher		1891	25			Par	2,045	21.1 21.87	Mar. 2 Jan. 1		Cf, E, 1/2	D, S	Dug well. Reported strong well. Water reported from gravel.
	802	do			Spring			Par	2,035	+	Mar. 2	6, 1970	Flows		Estimated flow 1 gpm, Reported to go dry in severe drought.
	803	do			Spring			Ka	2,080	+	đ	0	Seeps		Reported to never go dry.
	804	Roy Manahan	McCarrell & Son	1960	260	6	260	Ка	2,272	226.8 220.95	Apr. 2 Jan. 14	2, 1970 4, 1971	с, w	s	Reported good well.
	49-101	A. P. Tice, Guardian			Spring			Кf	2,280	+	Feb. 18	8, 1970	Seeps		
	102	do			145	5		Ка	2,288	124.1 116.65	Feb. 17 Jan. 19		с, w	s	Reported strong well.

Table 5Records of Selected Water	Wells and Springs in	nTaylor County and Adjacent Ar	easContinued

				DUDO	CAS	INC				TER LEVEL	-		
WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-30-49-10:		Jim Rea Drilling	1969	60	6	60	Qa1	2,130	15.95 19.86	Mar. 26, 1970 Jan. 13, 1971	Sub, E, 1/2	D, S	
104				28	7	28	Qa 1	2,090	12	Mar. 26, 1970	с, w	s	Water reported from 5 ft of gravel topped at 16 ft.
* 105				Spring			Qa 1	2,078	+	do	Flows		Estimated flow 15 gpm.
* 201		Robert Higgins	1962	52	6	52	Qa 1	2,090	32.5 32.6	do Jan. 13, 1971	J, E, 1/2	D, S	Water reported from sand at about 20 to 38 ft. Casing slotted from 20 to 30 ft.
401	Arthur Sears Estate			294	5		Ka	2,409	181.85	Jan. 15, 1971	c, w	s	Reported yield 1/2 gpm. Reported crooked hole.
402	do			< 250	5		Ka	2,413	196.6 191.18	Mar. 5, 1970 Jan. 15, 1971	C, W	s	Reported good well.
403	do			Spring			Kf	2,260	+	Mar. 5, 1970	Flows		Estimated flow 25 gpm.
601	W. L. Marshall, Jr.			Spring			Ka	2,100	+	Jan. 29, 1970	Flows		
602	do			17			Ka	2,090	8.47 9.17	do Jan. 13, 1971	C, W	D, S	Estimated flow 5 gpm. Dug well.
603	do			31			Ka	2,118	21.94 22.82	Jan. 29, 1970 Jan. 13, 1971	с, w	s	Do.
604	do			22			Ka	2,108	14.21 16.02	Jan. 29, 1970 Jan. 13, 1971		N	Do.
605	H. R. Roberts		1955	90	5	90	Ка	2,176	32.7 36,07	Mar. 10, 1970 Mar. 21, 1971	c, w	s	Seismic hole.
606	do			90	8	90	Ka	2,211				N	Water reported from 20 to 25 ft and possibly 70 to 80 ft,
607	do			Spring			Kf	2,195	+	Mar. 10, 1970	Seeps		Reported good spring,
901	do		1960	15			Ka	2,101	2.16 1.64	do Mar. 21, 1971	Cf, E, 1	D, S	Dug well, Reported strong well. Water from sand at 8 to 9 ft.
902	do		1923	20			Ка	2,098	0.20	Mar. 10, 1970 Mar. 21, 1971	N	N	Dug well. Water reported from sand at 10 ft.
50-101	Buck Wielder	Buck Wielder	1959	20			Ka	2,018	15.5	Oct. 2, 1959		N	Dug well, Destroyed,
102	W. L. Marshall, Jr.		1964	40	8	40	Qa 1	2,065	25.0	Mar. 27, 1970	J, E, 1	D, S	Water reported from sand and gravel topped at 20 ft. Reported yield 40 gpm. Casing slotted from 25 to 35 ft.
103	R. Y. Buchanan	Jack Leonard	1967	25	8		Qal	2,017	8.9	Nov. 13, 1969	Cf, E,	Irr	Water reported from sand and gravel.
104	do	do	1965	26	12		Qa 1	2,017	9.1	do	Cf, E,	Irr	Do.
105	do						Qal	2,017	9	do	Cf, E, 1/2	D	Dug well. Water reported from sand and gravel.
106	Ed Brown Estate	Jack Leonard	1964	25	12		Qal	2,018	7.5	do	Cf, E,	Irr	Water reported from sand and gravel.
107	do	do	1964	25	12		Qal	2,018	6.3	do	Cf, E,	Irr	Do.
108	do	do	1964	25	12		Qa 1	2,018	6.3	do	Cf, E,	Irr	Do.

	1	I			CASI	NG			WA	TER LEVEL			· · · · · · · · · · · · · · · · · · ·
WELL	OWNER	DRILLER	DATE Coripleted	DEPTH OF WELL (ft)	DIAM~ ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-30-50-109	Ed Brown Estate	Jack Leonard	1964	25	12		Qa1	2,018	5,8	Nov. 13, 1969	Cf, E, 5	Irr	Water reported from sand and gravel.
* 110	do		1958				Qal	2,013	4.8	do	N	N	Dug well. Water reported from sand and gravel.
* 111	R. L. Rode			36			Qal	1,952	16.69	Nov. 20, 1969	Cf, E, 1/2	U	Dug well.
112	do	Jack Leonard	1962	24	12	24	Qa l	2,021	11.54	do	Cf, E, 1-1/2	lrr	Reported yield 100 gpm. Water reported from sand and gravel topped at 16 ft, Well has separate pumping equipment, on same meter with XW-30-50-113 and XW-30-50-114.
113	do	do	1963	24	12	24	Qa 1	2,019	10.97	do	Cf, E, 1-1/2	Irr	Reported yield 100 gpm. Water reported from sand and gravel copped at 16 ft. Well has separate pumping equipment. on same meter with XW-30-50-112 and XW-30-50-114.
* 114	do	do	1963	24	12	24	Qal	2,020	11.35	đo	Cf, E, 1-1/2	Irr	Reported yield 100 gpm. Water reported from sand and gravel topped at 16 ft. Well has separate pumping equipment, on same meter with XW-30-50-112 and XW-30-50-113.
115	Mrs. Grady Clark	do	1964	23	12	23.0	Qal	2,018	6.46	Dec. 18, 1969	Cf, E, 1-1/2	Irr	Water reported from 7 ft of sand and gravel topped at 13 ft, Reported yield 200 gpm. Casing slotted from 19 to 23 ft.
116	do	do	1964	22	12	22	Qa 1	2,018	5.56	Dec. 18, 1969	Cf, E, 1-1/2	Irr	Water reported from 7 ft of sand and gravel topped at 13 ft. Reported yield 250 gpm. Casing slotted from 18 to 22 ft.
117	do	do	1964	22	12		Qal	2,018			N	N	Water reported from 7 ft of sand and gravel topped at 13 ft. Reported yield 200 gpm, Casing slotted from 18 to 22 ft.
118	do			22	••		Qal	2,018	7.50 6.10 9.64 9.44	Dec. 18, 1969 Apr. 15, 1970 Sept. 16, 1970 Jan. 15, 1971	N	N	Dug well. Observation well.
* 119	Ned Newman	Jack Leonard	1965	42	5	42	Qal	2,064	29.52	Dec. 18, 1969	Sub, E, 1/3	S	Water reported from sand and gravel at 38 to 39 ft. Reported yield 20 gpm. Casing perforated from 32 to 42 ft.
* 120	R. L. Rode	Buck Wielder		21			Qal	2,023	10.40	Jan. 13, 1970	J, É	s	Dug well. Water reported from sand and gravel.
* 121	W. L. Marshall, Jr.		1938	24			Qa 1	2,018	17.9 5.84	June 23, 1939 Jan. 30, 1970	J, E	D	Dug well. Well 206. <u>B</u> r
* 122	Graham Brothers	Jack Leonard	1960	25	18	25	Qal	2,018	6.08	J a n. 28, 1970	Cf, E, 1-1/2	Irr	Water reported from thin sand and gravel. Casing perforated at 20 to 25 ft.
* 123	Bea Newman	Jim Rea Drilling	1969	50	5	50	Qa 1	2,055	30.9	Mar. 27, 1970	2/	D, Irr	Water reported from sand and gravel. Well is pumped by equipment on well XW-30-50-124.
* 124	do	Jack Leonard	1966	57	6	57	Qa 1	2,055			J, E, 1	D, Irr	Keported yield 12 gpm. Water reported from sand and gravel. Equipment on this well also pumps XW-30-50-123.
* 201	Robert Knott	do	1957	24	12	24	Qal	2,005	5.22	July 24, 1970	N	N	Water reported from sand and gravel at 15 to 21 ft. Casing perforated from 20 to 24 ft.
202	W. L. Marshall, Jr.		1910	22			Qa1	2,007	12 6.52 <u>4</u> у	Oct. 3, 1959 Jan. 20, 1970	Cf, J, E, 1-1/2, 3/4	D, Irr	Dug well. Reported yield 100 gpm. Water reported from sand and gravel at 10 to 20 ft.

Γ			[CAS	ING			WA	TER LEVEL			
	WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITODE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
	XW-30-50-203	W. L. Marshall, Jr.	W. L. Marshall, Sr.	1952	22			Qal	2,006	12	Oct. 3, 1959	Cf, J, E, 1-1/2, 1	D, Irr	Dug well. Reported yield 200 gpm. Water reported from sand and gravel at 10 to 20 ft.
	2 04	do	W. L. Marshall, Jr.	1953	22			Qa 1	1,999	12 4.17	do Jan. 30, 1970	Cf, J, E, 1, 1/2	D, Irr	Reported yield 100 gpm. Water reported from sand and gravel at 10 ft.
	205	do	do	1952	22	8	22	Qal	2,006	12 4.87	Oct. 3, 1959 Jan. 30, 1970	Cf, E, 1-1/2	Irr	Dug well. Located in livestock pen. Reported yield 100 gpm. Water reported from sand and gravel at 10 to 20 ft. Casing slotted from 12 to 22 ft.
	206	do	do		22	12	22	Qa 1	2,005	12 4.56	Oct. 3, 1959 Jan. 30, 1970	Cf, E, 1-1/2	Irr	Dug well. Reported yield 100 gpm. Water reported from sand and gravel at 10 to 20 ft. Casing slotted from 12 to 22 ft.
,	207	do		1953	23			Qal	2,000	12 4.56	Oct. 3, 1959 Jan. 30, 1970	Cf, J, E, 1-1/2, 1/2	D, Irr	Reported yield 250 gpm. Water reported from sand and gravel at 10 to 20 ft.
*	208	do	W. L. Marshall, Jr.	1952	24	12	24	Qa 1	2,004	12 4.37	Oct. 3, 1959 Jan. 30, 1970	Cf, E, 1-1/2	Irr	Reported yield 100 gpm. Water reported from sand and gravel at 10 to 20 ft. Casing slotted from 14 to 24 ft.
	209	do	do	1955	22	12	22	Qal	1,998	12 3.93	Oct. 3, 1959 Jan. 30, 1970	Cf, E, 1-1/2	Irr	Reported yield 150 gpm. Water reported from sand and gravel at 10 to 20 ft. Casing slotted from 12 to 22 ft.
*	210	do	do	1955	22	12	22	Qa1	1,997	12 3.45	Oct. 3, 1959 Jan. 30, 1970	Cf, E, 1-1/2	Irr	Do.
*	211	B. L. Standard	Leonard Street	1956	23	14	23	Qe1	1,997	14.0 3.89	Sept. 23, 1959 Nov. 20, 1969	Cf(2), E, 1-1/2, (2)	Irr	Reported yield 300 gpm. Water reported from send and gravel at 17 to 23 ft. Casing slotted from 18 to 22 ft. Two centrifugal pumps and two motors in this well. 3
*	212	do		1914	23			Qa 1	1,998	14 2.57	Sept. 23, 1959 Nov. 20, 1969	Cf(2), E, 1-1/2, (2)	Irr	Dug well. Reported yield 225 gpm. Water reported from sand and gravel at 17 to 23 ft. Two centrifugal pumps and two motors in this well. 39
*	213	Ed Brown Estate		1885	33			Qa 1	2,008	26 13.93	Sept. 23, 1959 Nov. 13, 1969	Cf, E, 5	Irr	Dug well. Reported yield more than 200 gpm. Water reported from sand extending from land surface to 33 ft.
*	214	do	Jack Leonard	1957	20	14		Qal	1,979	12 3.05	Sept. 23, 1959 Nov. 13, 1969	2	lrr	Reported yield more than 200 gpm. Water reported from sand and gravel, Well on manifold system with XW-30-50-222 and XW-30-50-223.
	215	Ada Robertson	do	1957	20	12	20	Qa1	1,990	14.4 6.04	Oct. 7, 1959 July 22, 1970	Cf, E, 1-1/2	Irr	Reported yield 75 gpm. Water reported from sand at 14 ft and gravel at 18 to 19 ft. Casing perforated from 14 to 20 ft.
+	216	do	do	1957	20	12	20	Qa1	1,984	14 6.17	Oct. 7, 1959 July 22, 1970	Cf, E, 5	Irr	Reported yield more than 200 gpm, Water reported from sand at 14 ft and "creek rock" at 18 to 20 ft, Well screened from 16 to 20 ft.
*	217	W. L. Roberts	do	1958	24	12	24	Qa1	1,993	12.2 3.23	Oct. 9, 1959 Dec. 16, 1969	Cf, G	Irr	Water reported from sand and gravel at 12 to 24 ft. Casing perforated from 22 to 24 ft.
*	218	Tuscola Water District No. 1		1922	34			Qa1	1,978	Dry 20 15	June 23, 1939 Apr. 18, 1946 Sept. 23, 1959	N	N	Dug well. Abandoned public supply well. Well 217. ϑ Last pumped down June 23, 1939.

Table 5Record	s of	Selected	Water	Wells	and	Springs	in	Taylor	County	and	Adjacent	AreasC	ontinued
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					CASI	NG				TER LEVEL			
WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
XW-30-50-219	Ed Brown Estate	Jack Leonard	1965	29	12		Qal	2,009	13,53	Nov. 13, 1969	Sub, E, 7-1/2	D, S, Ind	Reported yield 100 gpm. Water reported from sand and gravel.
* 220	do	do	1965	20	12		Qal	2,001	4.0 <i>4</i> /	do	Sub, E, 7-1/2	D, S, Inđ	Do.
221	B. L. Standard	Leonard Street	1957	21	10		Qal	1,998	2.0	Nov. 20, 1969	Cf. E, 1	Irr	Reported yield 125 gpm. Water reported from sand and gravel at 16 to 20 ft. Casing slotted from 17 to 21 ft.
222	Ed Brown Estate	J a ck Leonard	1958	20	12		Qal	1, 979	3.3	Nov. 13, 1969	Cf, G	Irr	Reported yield more than 200 gpm. Water reported from sand and gravel. This well, XW-30-50-214, and XW-30-50-223 on manifold system.
223	do	do	1958	20	12		Qa 1	1,979	3.3	Nov. 14, 1969	2/	lrr	Reported yield more than 200 gpm. Water reported from sand and gravel. Well on manifold system with XW-30-50-222 and XW-30-50-214.
224	W. I. Roberts	do	1949	26			Qa1	1,981	7.54	Dec. 16, 1969	Cf, E, 3	D	
* 225	B. L. Standard	do	1959	21	10	17	Qel	1,998	1,16	Nov. 20, 1969	Cf, E, 1	Irr	Reported yield 125 gpm. Water reported from sand and gravel at 18 to 21 ft. Well screened from 17 to 21 ft.
* 226	do		1885	20			Qal	2,004	5.51	do	Cf, E, 1-1/2	D, Irr	Dug well. Reported yield 80 gpm. Water reported from sand and gravel.
* 227	Dan McCall		1968	18	6	18	Qal	2,013	8	Dec. 18, 1969	J, E, 3/4	D	Water reported from sand and gravel topped at 15 ft. Reported yield 40 gpm. Casing perforated from 15 to 18 ft.
228	Graham Brothers		1905	18			Qal	1,998	.98	Jan. 28, 1970	N	N	Dug well.
* 229	do		1957	21	18	21	Qa 1	1,998	1,18	do	N	N	Water reported from sand and gravel at 16 to 21 ft. Casing perforated from 16 to 21 ft.
* 230	do		1957	21	18	21	Qa1	2,003	1.93	đo	Cf, E, 1	Irr	Reported yield for short periods 100 gpm. Water reported from sand and gravel at 16 to 21 ft. Water pumped from this well to well XW-30-50-231. Casing perforated from 16 to 21 ft.
231	do		1957	21	16	21	Qal	2,001	16 1.25	Sept. 23, 1959 Jan. 28, 1970	Cf, E, 5	lrr	Reported yield 250 gpm. Water reported from sand and gravel at 16 to 21 ft. Casing perforated from 16 to 21 ft. 3
232	Oscar Little		1928	21			Qa 1	2,006	4.40	Mar. 26, 1970	J, E, 1/3	D	Dug well. Reported yield 55 gpm. Water reported from sand and gravel.
233	do	Ed Chapman		21	2	21	Qa 1	2,008	3.68	do	Cf, E, 2	D	Reported yield 55 gpm. Water reported from sand and gravel topped at 15 ft. Casing perforated from 14 to 21 ft.
234	Ada Robertson			22			Qa 1	1,992	2.33	July 22, 1970	N	N	Dug well.
235	do	Elmer Sandell	1952	22	30	22	Qa 1	1,993	5.79	July 22, 1970	Cf, E, 5	Irr	Dug well. Reported yield 125 gpm. Water reported from sand at 14 ft and gravel at 18 ft.
236	Robert Knott	Jack Leorard	1957	24	12	24	Qal	2,005	5,21	July 24, 1970	N	N	Water reported from sand and gravel at 16 ft. Casing perforated from 20 to 24 ft.

						CASI	NG			WA	TER LEVEL			
Г 	WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
XW-3	30-50-237	Robert Knott	Jack Leonard	1957	24	18	24	Qal	2,005	4.76	July 24, 1970	N	N	Water reported from sand and gravel at 16 ft. Casing perforated from 20 to 24 ft.
*	301	C. T. Runyan			20			Qal	1,967	3.75	Jan. 27, 1970	N	N	Dug well. Water reported from sand and gravel.
*	501	W. L. Marshall, Jr.		1957	20	12	20	Qa 1	1,989	13.78 3.89	Oct. 7, 1959 Jan. 30, 1970	Cf, E, 5	Irr	Reported yield 200 gpm. Water reported from sand and gravel topped at 14 ft. Casing slotted from 10 to 20 ft.
*	502	do		1957	20	12	20	Qal	1,985	13.8 4.67	Oct. 7, 1959 Jan. 30, 1970	Cf, E, 3	lrr	Reported yield 250 gpm. Water reported from sand and gravel at 10 to 20 ft. Casing slotted from 10 to 20 ft.
*	503	do		1958	22	12	22	Qa 1	1,982	13.6 4.23	Oct. 7, 1959 Jan. 30, 1970	Cf, E, 3	Irr	Reported yield 150 gpm. Water reported from sand and gravel at 16 to 22 ft. Casing slotted from 12 to 22 ft.
	504	Ed Graham		1959	24	14	24	Qa 1	1,980	14.9 11.9	Sept. 23, 1959 July 22, 1970	N	N	Water reported from sand and gravel. Casing perforated from 18 to 24 ft.
*	505	Tuscola Water District No. l		1920	28			Qa 1	1,972	16 15.0 6.52	Apr. 18, 1946 Sept. 23, 1959 Oct. 22, 1969	Sub, E, 7-1/2	Р	Dug well. Water reported from 8 ft of sand and gravel topped at 20 ft, Reported yield 100 gpm.
	506	R. M. McCall	Elmer Sandell	1959	22			Qal	1,978	14.5 6.35	Oct. 7, 1959 Nov. 17, 1969	Cf, G	Irr	Dug well. Reported yield 400 gpm. Water reported from gravel topped at 14 ft. Casing perforated from 14 to 22 ft. <u>3</u>
*	507	Tusco la Water District No. 1		1953	25		•	Qal	1,965	15.0 3.90	Sept. 23, 1959 Jan. 28, 1970	Cf, E, 5	Р	Dug well. Reported yield 100 gpm. Water reported from sand and gravel at 20 to 25 ft.
*	508	Ned Newman			24			Qa1	1,970	2.08	Dec. 18, 1969	Sub, E, 1-1/2	D, lrr	Dug well. Water reported from sand and gravel. Measured yield 51 gpm June 25, 1970. Centrifuga pump with 5-hp motor is used for irrigation. \underline{J}
*	509	R. M. McCall		1957	23			Qa 1	1,978	6.34	Nov. 17, 1969	Cf, E, 3/4	D, S	Reported yield 400 gpm. Water reported from gravel at 12 ft. Casing perforated from 11 to 23 ft.
	510	do	Jack Leonard	1964	24	18	25	Qa 1	1,977	5.80 5.30 9.54 9.04	do Apr. 15, 1970 Sept. 16, 1970 Jan. 15, 1971	2	Irr	Observation well. Water reported from gravel at 12 to 24 ft. Casing perforated from 13 to 25 ft. Well is pumped by equipment on well XW-30-50-506.
*	511	O. T. Loudamy	do	1969	26	13	26	Qa1	1,974	7.47	Dec. 2, 1969	Cf, E, 7-1/2	Irr	Measured yield 86 gpm June 25, 1970. Water reported from sand and gravel at 17 to 25 ft. Casing perforated from 20 to 26 ft. \underline{J}_j
*	512	do	do	1965	26	18	26	Qa 1	1,976	7.97	do	J, E, 1	D	Reported yield more than 250 gpm, Water reported from sand and gravel at 17 to 25 ft. Casing perforated from 20 to 26 ft.
	513	Ned Newman			25			Qal	1,973	5,40	Dec. 18, 1969	N	N	Dug well. Water reported from sand and gravel.
*	514	J. O. Egger		1964	21	14	21	Qal	1,979	8.32	Jan. 27, 1970	J, Cf, E, 3/4, 5	D, Irr	Reported yield 100 gpm. Water reported from sand and gravel. Casing perforated from 13 to 21 ft.
*	515	C. C. Allmand	Jack Leonard	1965	22	12	22	Qa 1	1,970	2.44	Jan. 26, 1970	Cf, E, S	Irr	Reported yield 125 gpm. Water reported from sand and gravel at 15 ft. Casing perforated from 15 to 20 ft.
	516	do	do	1965	25	12	25	Qa1	1,971	3.2	do	Cf, E, 1	Irr	Reported yield 50 gpm. Water reported from sand and gravel at 18 to 20 ft. Casing perforated from 18 to 22 ft.

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	WELL	(WNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-3	30-50-517	C. C. Allmand			22			Quel	1,971	6.10	Jan. 26, 1970	ūf, E, 1/3	0, 8	Dug well, Reported yield 30 gpm, Water reported from sand and gravel at 16 to 18 ft.
*	518	do	Jack Leonard	1964	28	12	28	Qe 1	1,975	10.35	do	Cf, E, 5	Irr	Reported yield 200 gpm. Water reported from sand and gravel at 22 to 27 ft. Casing perforated from 23 to 28 ft.
*	519	do		1957	34	12		Qa l	1,978	11.86	do	Cf, E, 1	lrt	Reported yield 25 gpm. Water reported from sand and gravel at 30 ft. Casing perforated from 29 to 32 ft.
*	520	do	Jack Leonard	1964	24	12	24	Qal	1,971	7,30	do	Cf, E, 7-1/2	S, Irr	Reported yield 200 gpm. Water reported from sand and gravel at 16 ft. Casing perforated from 17 to 22 ft.
*	601	Noble Touchstone	Mr. Hall	1957	24	16	24	Qal	1,961	14.4 5.83	Oct. 2, 1959 Dec. 3, 1969	Cf, E, 20	Irr	On manifold system with well XW-30-50-522. Reported yield 250 gpm, Water reported from sand and gravel at 15 to 23 ft. Casing perforated from 16 to 24 ft.
*	602	K. C. Roberson		1958	24	16	24	Qal	1,960	17.0 6.97	Oct. 1, 1959 Dec. 1, 1969	Cf, E, 1	S, Irr	Measured yield 61 gpm July 1, 1970. Water reported from sand and gravel at 14 to 22 ft. Casing perforated from 17 to 22 ft. \underline{J}
*	603	do	Jack Leonard	1958	30	16	30	Qa 1	1,961	17.0 7.43	Oct. 1, 1959 Dec. 1, 1969	Cf, E, 7-1/2	Irr	Measured yield 256 gpm June 24, 1970. Water reported from sand and gravel at 14 to 29 ft. Casing perforated from 23 to 30 ft. <u>7</u> ;
*	604	R. J. Marshall		1891	23			Qal	1,945	6.53	Jan. 26, 1970	Cf(2); E, 1-1/2(2)	D	Dug well. Water reported from sand and gravel. Two centrifugal pumps and two motors in this well.
	605	do		1891	20			Qal	1,946	8,12	do	Cf(2); E, 1-1/2, 5	S	Dug well. Reported yield 200 gpm. Water reported from sand and gravel. Previously used for irrigation. Two centrifugal pumps and two motors in this well.
*	606	C. A. Fomby	C. A. Fomby	1955	26			Qal	1,939	8 4.9 3.20 8.23 8.10	Oct. 5, 1959 Nov. 14, 1969 Apr. 15, 1970 Sept. 16, 1970 Jan. 15, 1971	R, E, 5	Irr	Dug well, Observation well. Reported yield more than 300 gpm. Water reported from sand and gravel at 14 to 26 ft. Casing perforated from 14 to 26 ft. Municipal supply well until approximately 1966. $\frac{3}{2}$
*	607	do	do	1952	22			Qa 1	1,939	9 5.1	Oct. 5, 1959 Nov. 14, 1969	Cf, E, 2	D	Dug well. Reported yield more than 200 gpm. Water reported from sand and gravel topped at 11 ft. Casing perforated from 11 to 22 ft.
*	608	do	Jack Leonard	1958	26	18	26	Qa 1	1,937	9 5.1	Oct. 5, 1959 Nov. 14, 1969	Cf, E, 7-1/2	Irr	Reported yield more than 300 gpm. Water reported from sand and gravel at 11 to 25 ft. Casing perforated from 12 to 26 ft.
*	609	do	Layne Texas Co.	1961	44	7	44	Qa1	1,938			Sub, E, 2	Р	Reported yield 50 gpm. Water reported from sand and gravel at 12 to 24 ft. Well screened from 12 to 24 ft.
	610	do	do	1960	44	7	44	Qa1	1,938			Sub, E, 2	Р	Do.
w	611	do	Jack Leonard	1960	26	16	26	Qal	1,935	7.1	Nov. 14, 1969	Cf, G, 48	Irr	Reported yield more than 500 gpm. Water reported from sand and gravel at 11 to 25 ft. Casing perforated from 11 to 26 ft.
	612	Loy Stockton	do	1967	25	12		Qa 1	1,956	8.53	Dec. 18, 1969	Cf, E, 10	Irr	Reported yield 350 gpm. Water reported from sand and gravel topped at 15 ft. Screened from 21 to 25 ft.

		1			CASE	NC:				TER LEVEL	{	ł	
WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
XW-30-50-613	Loy Stockton	Jack Leonard	1965	25	12		Qa1	1,954	8.17	Dec. 18, 1969	Cf, E, 7-1/2	Irr	Reported yield 400 gpm. Water reported from sand and gravel topped at 15 ft. Casing perforated from 20 to 25 ft.
614	C. A. Fomby		1939	18			Qal	1, 939			N	N	Dug well. Water reported from sand and gravel at 11 ft.
615	Ovalo Water Development	H. B. Coggins		24			Qal	1,920	19	Apr. 18, 1946		Ind	Dug well. Formerly Ovalo public supply well; Last used as such in 1958. Used occasionally for industrial purposes.
616	H. M. Landers		1892	24			Qa1	1,954	8.21	Dec. 3, 1969	Cf, E, 1-1/2	Irr	Dug well. Reported yield 90 gpm. Water report from sand and gravel. Casing perforated from 18 to 24 ft.
617	do		1953	26			Qal	1,954	7.54	Dec. 3, 1969	N	N	Reported yield 30 gpm. Water reported from sand and gravel.
618	do			25			Qal	1,954	7.90	đo	J, E, 1/3	D	Dug well. Water reported from sand and gravel.
619	do	Mr. Hall	1956	26	24	26	Qa1	1,953	8.2	do	Cf, E, 1-1/2	Irr	Reported yield 140 gpm, Water reported from sand and gravel. Casing perforated from 17 to 26 ft.
620	Noble Touchstone	Jack Leonard	1963	24	12	24	Qal	1,967	8.17	do	N	N	Reported yield 100 gpm. Water reported from sand and gravel at 16 to 23 ft. Casing slotte from 17 to 24 ft.
621	do	Mr. Hall	1956	21	24	21	Qal	1,963	7.07	do	N	N	Reported yield 150 gpm. Water reported from sand and gravel at 15 to 20 ft. Casing perforated from 13 to 21 ft.
622	do	do	1956	21	24	21	Qa1	1,962	7.0	do	2/	ĺrr	Reported yield 200 gpm, Water reported from sand and gravel at 15 to 20 ft. Casing perforated from 13 to 21 ft. On manifold system with well XW-30-50-601.
623	C. O. Swindle & Van Boozer	Jack Leonard	1966	21	8	21	Qal	1,963	6.13	Dec. 18, 1969	Cf, E, 1-1/2	Irr	Reported yield 105 gpm. Water reported from sand and gravel at 11 to 20 ft. Casing perforated from 13 to 21 ft.
624	Noble Touchstone	do	1954	28			Qal	1,963	5.62	Dec. 3, 1969	Cf, E, 1/2	n	Reported yield 50 gpm. Water reported from sa and gravel at 16 to 27 ft. Casing perforated from 20 to 28 ft.
625	R, J. Marshall		1891	20			Qa1	1,946	6.8	Jan. 26, 1970	с, ₩	N	Dug well. Reported strong well. An irrigation well that has not been used in 4 or 5 years. Water reported from sand and gravel at 20 ft.
626	Thurman Marshall			21			Qal	1,943	4.90	Jan. 27, 1970	Cf(2); E, 1-1/2(2)	D, Irr	Dug well. Reported yield 100 gpm. Water reported from sand and gravel. Two centrifuga pumps and two motors in this well.
627	K. C. Roberson			18			Qal	1,954	5.43	Dec. 1, 1969	N	N	Dug well. Reported yield 100 gpm. Water reported from sand and gravel at 10 ft.
628	do	Jack Leonard	1966	36	8	36	Qal	1,958	8.84	do	Cf, E, 10	Irr	Measured yield 580 gpm July 22, 1970. Water reported from sand and gravel at 9 to 34 ft. Casing slotted from 24 to 36 ft. 6/7
629	do	K. C. Roberson	1945	22			Qal	1,964			Cf, E, 1/2	Π	Dug well. Reported yield more than 20 gpm. Water reported from sand and gravel at 15 to 19 ft.

[CASI	NG			WA	TER LEVEL	1		
	WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
	XW 30-50-630	K. C. Roberson	Ronnie Roberson	1968	18		18	Qa 1	1,963			N	N	Dug well. Well filled in to 10 ft. Cased from 10 to 18 ft. Reported yield 20 gpm. Water reported from sand and gravel at 12 to 18 ft. Casing perforated from 12 to 18 ft.
	* 631	đo			25			Qa1	1,965	9.90 7.60 11.29 11.59	Dec. 1, 1969 Apr. 15, 1970 Sept. 16, 1970 Jan. 15, 1971	N	N	Dug well. Water reported from sand and gravel at 15 ft. Observation well.
	632	Tom Vaughn	Jack Leonard	1961	27	12	27	Qal	1,965	9.68	Dec. 2, 1969	J, E, 3/4	D	Reported yield 40 gpm. Water reported from sand and gravel at 14 to 26 ft. Casing perforated from 21 to 27 ft.
	633 634	do	do	1964	23	12	23	Qal	1,960			Cf, E, 1-1/2	Irr	Measured yield 127 gpm July 1, 1970. Water reported from sand and gravel at 14 to 22 ft. 7/
	634	do	do	1959	25	12	25	Qal	1,962	10.06	Dec. 2, 1969	Cf, E, 5	Irr	Reported yield more than 400 gpm. Water reported from sand and gravel.
	636	do	do do	1966	25	8	25	Qal	1,960	8.0	do	Cf, E, 10	Irr	Reported yield 500 gpm. Water reported from sand and gravel at 15 to 24 ft.
				1957	23	12	23	Qal	1,961	12.5 4.43	Sept. 23, 1959 Dec. 2, 1969	2	N	Reported yield 40 gpm, Water reported from sand and gravel at 12 to 22 ft, Casing perforated from 17 to 23 ft. Pumped by equipment on wells XW-30-50-638 and 639.
	637	do	do	1958	23	12	23	Qe 1	1,961	12.0 4.89	Sept. 23, 1959 Dec. 2, 1969	2/	Irr	Reported yield 300 gpm, Water reported from sand and gravel at 12 to 22 ft, Casing perforated from 17 to 23 ft, Funged by equipment on wells XW-30-50-638 and 639.
	638	do		1956	23	12	23	Qa 1	1,961	12.4 4.66	Sept. 23, 1959 Dec. 2, 1969	Cf, E, 20	Irr	Reported yield 300 gpm. Water reported from sand and gravel at 12 to 22 ft. Casing perforated from 17 to 23 ft.
	639 640	do C. T. Runyan		1956	25	12	25	Qal	1,961	13.4 5.81	Sept. 23, 1959 Dec. 2, 1969	Cf, E, 1-1/2 2/	N	Reported yield more than 125 gpm. Water reported from sand and gravel at 15 to 24 ft. Casing perforated from 19 to 25 ft.
ĺ	641	do	 Jack Leonard		25			Qal	1,968	5.77	Jan. 27, 1970	N	N	Dug well. Reported yield 20 gpm. Water reported from sand and gravel.
	642	1		1965	25	12	25	Qal	1,964	3.98	đo	Cf, E, 7-1/2	lrr	Reported yield 150 gpm. Water reported from sand and gravel at 20 to 24 ft. On manifold system with XW-30-50-642, 643, and 644.
		do	do	1966	25	12	25	Qal	1,962	3.35	do	2/	Irr	Reported yield 20 gpm. Water reported from sand and gravel at 20 to 24 ft. On manifold system with well listed next above.
	643	do	do	1965	25	12	25	Qal	1,965	5.73	do	Cf, E, 1 <u>2</u> /	Irr	Reported yield 40 gpm. Water reported from sand and gravel at 20 to 24 ft. On manifold system with well listed next above.
	644	do	do	1966	25	10	25	Qa1	1,967	6.57	do	Cf, E, 1-1/2 2/	Irr	Do.
	645	do			22			Qal	1,963	3,93	do	Cf, E, 2	D	Dug well. Reported yield 75 gpm. Water reported from sand and gravel at 20 ft.
	646	Floyd Tate	Jack Leonard	1966	25	15	24	Qa1	1,967	7.43	Mar. 26, 1970	Cf, E, 1	Irr	Water reported from sand and gravel topped at 13 ft. Casing slotted from 14 to 24 ft.

	1			DEPTH	CAS	ING				TER LEVEL	4		
WELL	OWNER	DRILLER	DATE COMPLETED	OF	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
XW-30-50-647	I. N. Wilkinson		1930	27			Qa 1	1,951	4.21	June 18, 1970	J, E, 1	D	Dug well. Water reported from sand.
648			1931	27			Qal	1,946	10.08	do	N	N	Dug well. Reported strong well.
649		Mr. Riddle	1960	24	12	24	Qa1	1,938	5.59	do	N	N	Reported strong well. Water reported from same
650			1920	25			Qa1	1,939	10,13	do	с, w	D, S	Dug well. Water reported from sand.
651	K. C. Roberson	Texas Water Development Board	1970	30			Qa1	1,958	11.11 10.99	Nov. 17, 1970 Dec. 15, 1970	N	N	Observation well for aquifer test conducted well XW-30-50-628. Casing removed from hole.
652	do	do	1970	27			Qal	1,958	9.10 10.93	Nov. 18, 1970 Dec. 15, 1970	N	N	Do.
653	do	do	1970	30			Qal	1,958	7.60 11.07	Nov. 18, 1970 Dec. 15, 1970	N	N	Do.
801	T. A. Bufford			22	9		Ka	2,073	10.83	June 17, 1970	J, E	D, S	
802	do			23			Ка	2,053	6.08	do		N	 Dùg well.
51-201	Loyd Rippy			102	5		Ка	2,110	100	Mar. 18, 1970	с, w	s	Reported good well.
202	Louise Shapard			97	5		Ka	2,125	93	Mar. 16, 1970	C, E, 1/2	s	
203	do			97	5		Ka	2,125	79.3 77.10	Mar. 18, 1970 Jan. 14, 1971	Sub, E, 1-1/2	D	Reported good well.
204	do			104	5		Ka	2,170	50.60 48.0	Mar. 18, 1970 Jan. 14, 1971	c, w	S	Do.
205	Clark Estate			87	4		Ka	2,244			c, w	s	Do.
206	Louise Shapard			151	4		Ка	2,263	140.9 135.7	Mar. 18, 1970 Jan. 14, 1971	c, w	s	
207	Lloyd Rippy			45			Ка	2,116	37.9 38.46	Mar. 18, 1970 Jan. 14, 1971	с, w	N	Dug well.
208	Louise Shapard			Spring			Кf	2,275	+	Mar. 18, 1970	Flows		Estimated flow 5 gpm.
209	do			Spring			Kf	2,150	+	do	Flows		Estimated flow 10 gpm.
301	do		1956	102	5		Ка	2,265	75.0 80.05	do Jan. 14, 1971	с, w	S	Reported good well. Originally drilled as an oil test.
302	Clark Estate			118	5		Ka	2,155	116.0 110.2	Mar. 16, 1970 Jan. 14, 1971	c, w	s	Reported good well.
303	do			Spring			K£	2,176	+	Mar. 16, 1970	Flows		Estimated flow 5 gpm.
401	A. S. Harker			15			Qa1	1,983	5.52	Feb. 9, 1970	Cf, E, 1/2	D	Dug well. Reported yield 50 gpm. Owner reports rapid alkali contamination. Water reported from sand and gravel at 7 ft.
402	do	Lester Johnson	1962	16	7	16	Qa 1	1,976	7.15	do	2/	Irr	Dug well. Water reported from sand and gravel at 7 ft and 16 ft. Not used extensively since 1962. Casing slotted from 8 to 16 ft. Well is pumped by equipment on well XW-30-51-403.
403	do	do	1962	16	10	16	Qa 1	1,976	7.05	do	Cf, E, 2	Irr	Dug well. Water reported from sand and gravel at 7 ft and 16 ft. Not used extensively since 1962. Casing slotted from 8 to 16 ft.

Table 5 Records of	Selected Water	Wells and Springs	in Taylor County	and Adjacent	AreasContinued
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WE	LL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-30	- 51-404	A. S. Harker	Lester Johnson	1960	16			Qal	1,975	6.62	Feb. 9, 1970	Cf, E, 1-1/2	Irr	Dug well, Reported yield 70 gpm. Water reported from sand and gravel at 7 fr and 16 fr. Not used extensively in 3 to 4 years. Casing slotted from 14 to 16 ft.
t	405	Roy L. Willis	Jack Leonard	1965	50	12		Ka	2,053			Sub, E, 1/2	D	Water reported from sand and gravel at 43 to 50 ft. Well screened from 42 to 50 ft. 39
:	406	do	do	1965	51	12		Ka	2,053	30.9 30.45	Mar. 18, 1970 Jan. 14, 1971		D	Well screened from 43 to 51 ft.
	407	I. N. Wilkinson			22			Qa1	1,937	16.13	June 18, 1970	N	N	Dug well.
	408	do			25			Qa1	1,929	16.22	do	с, w	S	Dug well. Reported very good well. Water reported from sand.
	409	do			27			Qal	1,922	19.45	do	N	N	Dug well.
	501	Roy L. Willis		1887	45			Ka	2,059	29.3 28.1	Mar. 18, 1970 Jan. 13, 1971		D, S	Do.
r	601	Marvin Rutland	Hayhurst Water Well Drilling	1969	101	6	101	Ка	2,098	76.65 79.6 4;	June 18, 1970 Jan. 14, 1971		D, S	Reported yield 4 gpm. Water reported from san at 80 to 104 ft. Casing slotted from 75 to 101 ft. 3
	602	do			72	6		Ка	2,090	70	June 18, 1970	C, E, 1/2	D	Reported yield 4 gpm.
ł	701	Seburn Monroe		1951	20			Qal	1,881	9.0 7.15	Oct. 5, 1959 Oct. 22, 1969		N	Dug well. Reported yield about 30 gpm. Water reported from sand and gravel at 9 to 20 ft. Formerly a municipal supply well; not used since 1970.
	702	do		1951	25			Qal	1,883	9.3 <u>4</u> /	do	T, E, 7-1/2	N	Dug well. Water reported from sand and grave. Formerly a municipal supply well; not used since 1970.
	703	G, N. Reid	Jack Leonard	1965	18	6 12	10 18	Qal	1,882	9.24	Nov. 19, 1969	2/	D, Irr	Reported yield 55 gpm. Water reported from sa and gravel at 13 to 17 ft. Casing perforated from 8 to 18 ft. Pumped by equipment on well XW-30-51-704.
	704	do	do	1965	18	6 12	10 18	Qal	1,882	9.18		Cf, E, 1-1/2	Irr	Reported yield 55 gpm. Water reported from sa and gravel at 13 to 17 ft. Equipment at this well also pumps wells XW-30-51-703 and XW-30-51-705. Casing perforated from 6 to 18 ft.
	705	do	do	1965	18	6 12	10 18	Qal	1,883	9.34	Nov. 19, 1969	<u>2</u> j	D, Irr	Reported yield 55 gpm. Water reported from sand and gravel at 13 to 17 ft. Casing perforated from 6 to 18 ft. Pumped by equipment on well XW-30-51-704.
r	706	do	do	1965	18	6		Qal	1,881	9,38 8.0 9,98 9,84	do Apr. 15, 1970 Sept. 16, 1970 Jan. 15, 1971		N	Water reported from sand and gravel at 13 ft. Observation well.
•	70 7	Malcolm Anderson			30			Qal	1,896	15.48	Jan. 27, 1970	Cf, E, 5	Irr	Dug well. Reported yield 300 gpm. Water reported from sand and gravel.
•	708	Wayne Allen		1917	22			Qa 1	1,895	15.9 7.87	May 11, 1939 June 18, 1970	J, E	D	Dug well. Water reported from sand and grave Well 226. 8
	901	Marvin Futland	Hayhurst Water Well Drilling	1968	100	6	100	Ка	2,050	73.2	do	с, w	s	

Table 5Records of Selected Water Wells and Springs in Taylor County and Adjacent AreasContinue		Table 5Records	of	Selected	Water	Wells	and	Springs	in	Taylor	County	and	Adjacent	AreasContinue	٤d
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				DEPTH	CAS	TNG				TER LE	VEL	1	[
WELL	OWNER	DRILLER	DA TE COMPLETED	UF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)		DATE OF ASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
* XW-30-57-101	L. F. Pennington		1938	20			Qa 1	2,037	13.8 12.82	July Nov.	27, 1939 25, 1969	c, w	D, S	Dug well. Reported strong well. Water reported from sand and gravel. Well 186. 8/
* 102	F. A. Bradshaw			20			Qa1	2,007	14.8 11.96	July Nov.	27, 1939 21, 1969	Cf, E, 1/2	0, S	Dug well. Reported to have never gone dry. Well 192. &
301	Billy McCasland		1925	24			Pc	2,011	3.39	June	17, 1970	Ј, Е, 1/3	D	Dug well. Water reported from sand and gravel at 16 ft.
						Calla	han County							
BX-30-36-101	Dr. John L. Estes		1930	21			P1	1,775	17.6	Mar.	5, 1971	c, w	S	Dug well. Water from fractures in limestone.
44-402	Doyle Lenz	L. E. Hayhurst	1968	56	6	56	Ka	2,010	37 35.5	July Jan.	5, 1968 8, 1971	C, W	D, S	Reported yield 4 gpm. Reported specific capacity 0.4 gpm/ft. Casing perforated from 35 to 53 ft. 3/
405	Ervin Welch	do	1963	30	6	30	P1	1,908	11.2	Mar.	1, 1971	c, w	s	
703	Frank D. Chrane	do	1969	66	6	66	Ka	2,061	51 51,85	July Jan.	16, 1969 8, 1971	J, E, 1/2	s	Reported yield 10 gpm. Reported specific capacity 1 gpm/ft. Casing perforated from 50 to 66 ft. 3;
704	Earl Zimmerle	do	1968	131	5	131	Ка	2,145	97	Apr.	14, 1968	Sub, E, 1/2	S	Reported yield 14 gpm. Reported specific capacity 4.79 gpm/ft. Casing slotted from 111 to 131 ft. 3/
705	Annie Mosier	do	1968	51	5	51	Ка	2,010	30 29.29	Aug. Feb.	13, 1968 5, 1971	J, E, 3/4	D	Reported yield 10 gpm, Reported specific capacity 1 gpm/ft. Casing perforated from 30 to 51 ft, 3/
52-101	C. W. Carter	C. W. Carter	1949	121	6	120	Ka	2,090	85.62	Dec.	3, 1970	Sub, E, 3/4	D, Irr	Reported yield 12 gpm. Sand and gravel at 80 to 120 ft, 3 /
102	do	do	1950	110	6	110	Ка	2,085	82,39		do	Sub, E, 1	D, Irr	Reported yield 14 gpm. Sand and gravel at 80 t 110 feet. Casing slotted from 87 to 110 ft. $3f$
105	S. O. Barton	L. E. Hayhurst	1969	130	5	130	Ka	2,100	20 20.07	July Feb.	29, 1969 8, 1971	Sub, E, 3/4	D, S	Reported yield 15 gpm. Specific capacity 0.75 gpm/ft. Casing slotted from 20 to 30 and 100 to 120 ft. $3_{\rm c}$
106	R. D. Whitford		1920	50			Ka	2,040	33.10	Mar.	1, 1971	c, w	D, S	Dug well. Reported yield 8 gpm. Water reported from sand and gravel at 35 to 50 ft.
401	Stella Johnson	Jack Barnes	1960	112	7 13	112 82	Ka	2,080	52	June	24, 1961	Sub, E, 2	N	Formerly supplied Oplin missile site. Reported yield 8 gpm. Well screened from 82 to 112 ft.
402	do	do	1960	112	7 13	112 82	Ka	2,104	82 82		24, 1961 11, 1971	Sub, E, 2	N	Do.
403	do	do	1960	112	7 13	112 82	Ка	2,100	76	Jan.	7, 1971	Sub, E,	N	Do.
406	John Armor	Mr. Rogers	1950	101	6	101	Ка	2,080	72,14	Mar.	1, 1971	J, E, 1/2	D, S	
407	Roy Armor		1950	90	6	90	Ка	2,090	60,80		do	c, W	D, S	Reported yield 8 gpm. Seep reported at 40 ft, and water-bearing sand at 70 to 88 ft.
701	Luther McCrea		1924	16			Ка	2,005	11.01 9.91		6, 1940 6, 1971	N	N	Dug well. Well 434 <u>9</u> . Water-bearing sand at 11 to 16 ft.
702	Lowell Johnson			49			Ка	2,025	29.49	Jan.	6, 1971	J, E, 1/3	D, S	Dug well. Water from sand and gravel.

			1		CASI	ING			WAT	TER LE	VEL	T		
WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)		DATE OF ASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
					Call	ahan Co	unty (Cor	tinued)		ĺ				
BX-30-52-703	Lowell Johnson	L. E. Hayhurst	1970	70	5	70	Ka	2,038	42.33	Jan.	6, 1971	C, W	s	Reported yield 5 gpm. Specific capacity 0.5 gpm/ft. Casing slotted from 47 to 70 ft. $\underline{3}$
						JÓNE	S COUNTY							
* PY-29-31-901	Mrs. Donnie Redus			91	6		Psa	1,908	16.2 14.0	July Dec.	30, 1953 1, 1967	с, w	s	Reported strong well. Well J-11. 5
902	Mark M. Williamson	Ed Chapman	1966	20	18	20	Psa	1,905	10.4		do	Cf, E, 5	Irr	Reported yield 137 gpm on original test; 50 gpm in 1967. Water reported from sand and gravel at 15 to 19.5 ft. Casing slotted from 16 to 20 ft.
* 903	do	do	1966	20	18	20	Psa	1, 906	10.5	-	do	Cf, E, 5	Irr	Reported yield 134 gpm on original test; 50 gpm in 1967. Water reported from sand and gravel at 16 to 19.5 ft. Casing slotted from 16 to 20 ft.
* 32-701	Douglas Reddin				7		Рс	1,853	15.9	Jan.	5, 1968	с, W, Ј, Е, 1/3	D, S	Reported strong well.
* 801	Forest Black			35	6		Pc	1,799	10.9		do	J, E, 1/3	D, S	Reported fair well. Water has "gyppy" taste.
* 802	Woodrow Rogers			32			Рс	1,802	3.1		do	с, w	Q	Dug well. Reported fair well. Reported contaminated by salt water.
803	do			60	6		Pc	1,804	5.8		do	с, w	N	
* 901	Bill Tarpley	Robert Higgins	1962	60	6	20	Pc	1,806	18	Dec.	19, 1967	J, E, 1/3	D, S	Reported yield 40 gpm. Water reported from sandy clay at 29, 31, and 53 ft.
* 902	Otis Foster	do	1963	60	6	30	Pc	1,804			do	с, ₩	s	Do.
903	S. C. Herring, Jr.			45	6		Pc	1,788	21.0		do	с, w	s	Reported strong well,
* 904	do		1960	37	4		Pc	1,785	5.9		do	N	N	Core test.
* 905	Forest Black	Robert Higgins	1951	64	7	35	Pc	1,789	4.7	Jan.	5, 1971	N	N	Unused industrial well.
906	Le Clair Operating Company Inc.			5,957	7 5	4,644 5,730		1,778	1,200	Apr.	26, 1968	Sub, E, 100	N	Reported yield more than 278 gpm. Brine supply well for secondary recovery of oil.
* 701	E. L. Tarpley			50	6		Рc	1,784	12,9	Dec.	19, 1967	J, E, 1/2	D	
* 801	Union Texas Petroleum			125	12		Qs, Pvb	1,807	23.35 14 <u>4</u>	Aug. Jan.	18, 1960 4, 1968	T, E, 5	Ind	Reported yield 35 gpm. Water reported from gravel at 18 to 22 ft (minor source, and water of poor quality), and from red clay with blue streaks between 22 and 125 ft. Well K-22, 5/
* 802	do			125	10		Qs, Pvb	1,819	12.89		do	т, Е, З	Ind	Reported yield 30 gpm, Well K-19, 5/Well on standby.
803	do			125	10		Qs, Pvb	1,817				N	N	Reported yield more than 10 gpm. Water reported from red clay with blue streaks. Well K-18, \underline{S}
804	do			115	10		Qs, Pvb	1,812				N	N	Reported yield more than 10 gpm. Well K-15. $\underline{5}j$
805	do			125	10		Qs, Pvb	1,808				N	N	Reported weak well. Water reported from red clay with blue streaks. Well K-21. 5/

			1			CAST	NG			WA	TER LEVEL	J		
	WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
P	-30-25-806	Union Texas Petroleum			125	10		Qs, Pvb	1,811			N	N	Reported yield 35 gpm. Water reported from red clay with blue streaks. Well K-23. 5/
*	807	J. H. F. Jones			115	6	20	Qs, Pvb	1,800	9.47	Dec. 10, 1968	J, E, 3/4	D	Reported good well. Water reported at 79.5 ft.
*	901	Fred Shotwell			90	6		Qs	1,733	10,05	Nov. 30, 1967	С, Е, 1/2	D	Reported strong well.
*	902	Mrs. H. Arnwine			40			Qs	1,710	38.64 9.86	July 13, 1953 Nov. 30, 1967	C, W, J, E, 1/2	D, S	Dug well. Reported fair well. Well K-13. \S
	903	do			60			Qs	1,709	6.23	Jan. 25, 1968	c, w	s	Dug well. Well K-14. 5/
*	904	C. T. McCormick			15			Qs	1,744	4.4	Jan. 3, 1968	с, н	N	Dug well. Unused cistern with holes in bottom.
	905	J. David Proctor			60	6		Qs	1,726	12.65	.Tan, 14, 1969	N	N	
*	906	D. H. Reddin			15			Qs	1,758	8.70	do	с	N	Reported good well.
*	26-701	G. P. Arnwine	Robert Higgins	1966	60	7 6	33 60	Qs	1,695	14,99	do	J, E, 1/2	D, S	Reported yield 8 gpm. Water reported at 20 to 21 ft from sand and gravel at 18 to 25 ft. Casing perforated from 15 to 30 and 35 to 55 ft.
*	702	J. David Proctor			60			Pv	1,678	19.4	Jan. 4, 1968	N	N	Reported very weak well.
*	703	do	Ed L. Chapman	1964	24	13	24	Qal	1,681	8.38	do	J, E, 1	D, S	Reported yield more than 25 gpm. Water reported from sand and gravel at 18 to 22 ft. Casing slotted from 20 to 24 ft.
	704	do	do	1964	24	13	24	Qa1	1,687	8	Jan. 4, 1968	с	N	Reported yield more than 25 gpm, Water reported from sand and gravel at 16 to 22 ft. Casing slotted from 20 to 24 ft.
*	705	do	do	1964	24	11	24	Qal	1,670	9.9	do	N	N	Reported yield 35 gpm. Water reported from sand and gravel at 17 to 22 ft. Casing slotted from 20 to 24 ft.
*	706	do			72	8		Pv	1,678	12.0	do	N	N	
*	27-701	0. T. Daugherty			30			Qs	1,662	12.8	Dec. 20, 1967	с, w	D	Dug well. Reported very weak well.
*	702	Luther Weeks	Luther Weeks	1910	35			Qal	1,642	11.67	do	C,W,J,E, 1/2	D, S	Dug well. Reported very strong well. Water reported from sand and gravel at 30 ft.
	703	do	do		24			Qal	1,638	10	do	N	N	Dug well. Water reported from sand and gravel at 4 to 24 ft. Reported very strong well.
	704	do	do		24			Qal	1,638	10	do	N	N	Dug well. Water reported from sand and gravel at 4 to 24 ft. Reported very strong well.
	705	David S. Ramsey	G-M Drilling Co.	1965	80	9	31	Qa 1	1,642	20	Mar. 22, 1965	R, E	S	Reported yield 0.75 gpm, Sand and gravel reported at 9 to 15 ft. Water reported from gravel at 17 to 26 and 49 to 55 ft.
*	901	Tony P. Vaughn		1911	27			Qa1	1,718	13.7	Sept. 20, 1967	J, E, 1/3	D	Dug well. Reported fair well.
*	902	do			26			Qa 1	1,708	13.9	do	J, E, 1/2	D	Dug well. Reported strong well, Owner believes contaminated by salt water.
*	903	do			15			Qa1	1,713	12.9	Sept. 19, 1967	J, E, 1/3	D	Dug well. Water believed contaminated by sewage.
*	904	J. M. Foster		1910	30			Qa 1	1,706	13.1	Sept. 20, 1967	J, E, 1/3	N	Dug well. Reported strong well. Possibly contaminated.

				1	1	CASI	NG			WAT	ER LEVEL			
	WELL	OWNER	DRILLER	DATE COMPLETED	DEPTH OF WELL (ft)	DIAM- ETER (in.)	DEPTH (ft)	WATER BEARING UNIT	ALTITUDE OF LAND SURFACE (ft)	BELOW LAND- SURFACE DATUM (ft)	DATE OF MEASUREMENT	METHOD OF LIFT	USE OF WATER	REMARKS
PY	-30-26-905	R. T. Bynum			21			Qau	1,701	12.Ū	do	N	N	Dug well. Reported strong well.
*	906	do			26			Qal	1,701	15.4	do	J, E, 1/2	D, S	Dug well. Reported strong well. Water believed unfit for human consumption.
	907	do		1917	18			Qal	1,708	12.5	do	R, E, 1/2	N	Dug well. Reported fair well.
*	908	do			24			Qal	1,710	9.7	đo	J, E, 1/2	D, S	Dug well. Water believed unfit for human consumption.
*	909	J. B. Watts			21			Qal	1,711	16.93 15.4	July 29, 1953 Sept. 26, 1967	R, E, 1/3	N	Dug well. Well M-3. 5/
	910	Mrs. H. M. McBeath	Ed Chapman	1966	26	24	26	Qal	1, 714	10.99	do	J, E, 1/3	N	Reported strong well. Water reported from sand and gravel at 12 to 24 ft. Sand reported at 4 to 12 ft. Perforated casing from 21 to 25 ft. Water reported unfit for human consumption.
	911	Schkade Brothers Drilling Co.	M & M Water Wells	1966	35	7	35	Qal	1,710	15	Sept. 20, 1967	J, E, 1/2	Ind	Reported yield 7 gpm. Sand reported at 5 to 14 ft, sand and gravel at 14 to 25 ft, and water-bearing gravel at 25 to 32 ft. Casing perforated from 20 to 35 ft supply well for water flood.

NOLAN COUNTY

UA-29-39-901				50	4		Psa	2,130	50	Oct. 28, 1960	C, W	s	Water reported from Permian sandstone.		
55-901	L. O. Lynn			60	6		Psa	2,252	32	Nov. 1, 1960	с, w	s	Do.		
1 1															

* For chemical analysis of water see Table 7. j: Observation well used in connection with solid waste disposal or sanitary landfill system for the city of Abilene.

Run by equipment on another well.

รึ For driller's log of well see Table 6.

4 Pumping level. 5 Winslow, A. S.;

Winslow, A. S.; Doyel, William W. and Gaum, Carl H., 1954, Ground-Water Resources of Jones County, Texas: Texas

Board of Water Engineers Bulletin 5418, p. 1-29.

Aquifer test conducted on this well; see text for resulting data. 6/

Power yield test conducted on this well; see Table 4 for resulting data.

Smith Hoyt A., and others, 1940, Records of wells and springs, record of earthen tanks, tables of drillers and test hole logs, partial analyses of water from wells, springs and lakes, and map showing locations in Taylor County, Texas: Texas Board 8

tygs, parties analyses of water from weits, springs and takes, and map showing total tons in taylor obdity, least team used of Water Engineers duplicated report, 38 p. 9 Mueller, Carl B. and others, 1940, Records of wells and springs, tables of drillers and test hole logs, partial analyses of water

from wells and springs, and map showing locations in Callahan County, Texas: Texas Board of Water Engineers duplicated report, 44 p.

		THICKNESS {ft}	DEPTH (ft)			THICKNESS (ft)	DEPTH (ft)
	Well XW-29-32-9	907			Well XW-29-40-312	-Continued	
	vner: Jarrett E. V			Water (stron	g)	2	57
C	Driller: Robert H			Clay		10	67
Soil		2	2	Water		2	69
Clay and caliche		18	20	Clay		24	93
Red clay		30	50				
Water		2	52		Well XW-29-4	10-317	
Clay		15	67		Owner: Joe		
Water		2	69		Driller: Rober	t Higgins	
Clay		11	80	Soil		5	5
	Well XW-29-32-	908		Gravel		3	8
O	wner: Jarrett E.V	Villiams		Clay		33	41
	Driller: Robert H	liggins		Water		1	42
Soil		6	6	Clay		27	69
Clay		20	26	Water		3	72
Water		2	28	Clay		7	79
Clay		26	54	Water		2	81
Water		2	56	Clay		19	100
Clay		12	68				
Water		2	70		Well XW-29-	40-325	
Clay		10	80	c	wner: Merkel Indepen Driller: Robe		
	Well XW-29-39	-601		Soil		3	3
	Owner: Jack B			Clay		12	15
	Driller: A. L. H		-	Gravel		7	22
Top soil		3	3	Clay		12	34
Sand and gravel		6	9	Lime		1	35
Red clay		13	22	Water		1	36
Green sandy clay		2	24	Clay		18	54
Red clay		36	60	Water		2	56
				Clay		11	67
	Well XW-29-40			Water		2	69
C)wner: Jarrett E. Driller: Robert			Clay		21	90
Soil		6	6		Well XW-29	-40-327	
Caliche		12	18		Owner: Merkel Indeper		t
Red clay		12	30		Driller: Robe		-
Water		1	31	Soil		3	3
Clay		24	55	Clay		12	15

	THICKNESS (ft)	DEPTH (ft)	
Well XV	1-29-40-327—Continued		
Gravel	9	24	
Clay	10	34	
Lime	1	35	Soit
Clay	19	54	Red clay
Water	2	56	Green clay
Clay	11	67	Red clay
Water	3	70	
Clay	22	92	

Well XW-29-40-609

Owner: Mrs. Odis Griffin Driller: Robert Higgins

Soil	1	1
Caliche	18	19
Clay	19	38
Water	1	39
Clay	15	54
Water	1	55
Clay	12	67
Water	1	68
Сіау	11	79
Water	2	81
Сіау	19	100

Well XW-29-40-610

Owner: Mrs. Odis Griffin Driller: Robert Higgins

Soil	2	2
Caliche	6	8
Clay	32	40
Water	1	41
Clay	21	62
Water	1	63
Clay	15	78
Water	1	79
Clay	41	120

		(NESS DEP (ft) (ft	
Well	XW-29-48-203		
	er: L. B. Hester er: A. L. Hicks		
		3 3	3
	3	5 38	3
ву		1 39	ð

21

60

Well XW-29-48-407

Owner: Ford Butman Driller: Robert Higgins

Soil	1	1
Sandy clay	19	20
Sandstone	30	50
Water (sand?)	1	51
Clay	19	70

Well XW-29-48-603

Owner: Edgar Davis Driller: Robert Higgins

Soil	3	2
3011	3	3
Lime	197	200
Sand (dry)	78	278
Sand and gravel (water)	22	300
Clay basin	14	314

Well XW-29-55-302

Owner: E. B. Yeatts Driller: Joe Whitworth

Yellow lime	100	100
Blue lime	95	195
Brown sand (water)	30	225
Pink shale	15	240

Well XW-29-56-701

Owner: Leon Shedd Driller: Robert Higgins

Soil	3	3
Clay	8	11

	THICKNESS (ft)	DEPTH (ft)
Well XW-29-56-701-	Continued	
Sand and gravel	8	19
Clay	11	30
Sand and gravel (water)	8	38
Clay	24	62
Sand (water?)	2	64

Well XW-30-25-702

16

80

Clay

	Owner: H. B. Robertson Driller: Robert Higgins	
Soil	4	4
Clay	24	28
Seep	1	29
Clay	14	43
Water	1	44
Clay	18	62
Water	1	63
Clay	7	70

Well XW-30-25-716

Owner: Bill Black Driller: Robert Higgins

Sandy clay	3	3
Clay	5	8
Gravel and sand (water)	30	38
Clay	14	52
Water	1	53
Clay	16	69

Well XW-30-27-708

Owner: City of Abilene Driller: Jack Leonard

Red clay, damp	2	2
Red sand, clayey, fine to medium- grained, damp	2	4
Red clay, very silty, damp from 7 to 8.5 feet	9	13
Sand, clayey, fine-grained, moist	1.5	14.5
Red clay, silty, scattered gravel to 1/2 inch from 14.5 to 17.5 feet,		
wet from 17.5 to 20.4 feet	12	26.5

	THICKNESS (ft)	DEPTH (ft)
Well XW-30-27-708-0	Continued	
Red Sand, clayey, coarse-grained, gravelly	4	30.5
Shale, red to gray variegated	1.2	31
Limestone, light gray, very fine- crystalline to dense	0.3	32

Well XW-30-27-709

Owner: City of Abilene Driller: Jack Leonard

Red clay, silty	12	12
Sand, clean, medium-grained, moist, slight clay binder at 18 feet	10	22
Sand, coarse-grained, small gravel	5.6	27.6
Sand, gravel, unconsolidated, wet	2.9	30.5
Gravel, small to coarse	2.5	33
Limestone, gray-buff, dense, with some variegated shale	1	34

Well XW-30-27-710

Owner: City of Abilene Driller: Jack Leonard

Red sand, clayeγ	9.8	9.8
Limestone, boulder, gray, dense to very finely-crystalline	1.4	11.2
Sand, gravel (small)	2.6	13.8
Shale, silty, white to very light gray	0.8	14.6
Limestone, gray to medium gray, mottled	0.4	15

Well XW-30-27-711

Owner: City of Abilene Driller: Jack Leonard

Red clay, sandy to very sandy	9.5	9.5
Sand, fine to medium-grained, loose	13	22.5
Sand, gravel	0.5	23
Shale, silty, white to very light gray	1.6	24.6
Limestone, gray to buff, dense with gray shale laminae	1.2	25.8

	THICKNESS (ft)	DEPTH (ft)		THICKNESS (ft)	DEPTH (ft)
Well XW-30-27	-712		Well XW-30-27-716-	-Continued	
Owner: City of A			Red clay, silty, plastic	0.5	24.5
Driller: Jack Le	onard		Tan sand, loose	3	27.5
Red clay, silty, soft, sandy (coarse) from 18 to 18.4 feet, also from 21 to 21.6 feet with small gravel	29.2	29.2	Limestone, tan to buff, finely granular, shale laminae	5.3	32.8
Gravel with sand and clay	1	30.2	Red shale, gray to green variegated	5	37.8
Red clay, very plastic	1.4	31.6	Well XW-30-2	7-717	
Red shale	0.6	32.2			
			Owner: City of Driller: Jack Lo		
Well XW-30-27	-713		Road fill	6	6
Owner: City of A				Ū	-
Driller: Jack Le	onard		Red clay, silty, plastic, slightly sandy from 32.4 to 33.6 feet	27.6	33.6
Red clay, silty, plastic, with sand and gravel admixed from 21.3 to 23.0 feet	23	23.0	Tan sand, fine to medium-grained, loose	2.1	35.7
Sand, coarse, with gravel	8	31.0	Gravel with sand	3.1	38.8
Shale, red, gray variegated	0.8	31.8	Siltstone, soft, white to gray	0.7	39.5
			Shale, gray to buff, plastic	0.7	40.2
Well XW-30-27 Owner: City of / Driller: Jack Le	Abilene		Limestone, gray to buff, fine- granulated to very finely crystalline	0.5	40.7
Red clay, silty, plastic	22.5	22.5	Well XW-30-2	7-718	
Sand, coarse to medium grained,			Owner: City of	Abilana	
clayey, gravelly from 26 to 32.8 feet	10.3	32.8	Driller: Trinity Engineering		on
Shale, red, gray variegated	5.7	38.5	.		
Well XW-30-27	7-715		Red clay, silty, became moist at 9 feet, permeability test at 15.0 feet	16.8	16.8
Owner: City of Driller: Jack Le			Red sand, coarse, unconsolidated, water	0.7	17.5
Red clay, silty, plastic	32.4	32.4	Red clay, soft, wet, permeability test at 19.5 feet	2.5	20.0
Gravel, small, with some coarse sand	4.3	36.7	Red clay, firm, scattered gravel	8.0	28.0
Limestone, pale tan, buff, fine-	0.7	37.4	Sand, soft, water	1.5	29.5
granulated to very fine crystalline	0.7	57.4	Gravel, small with yellow and tan clay	0.5	30.0
Well XW-30-2	7-716		Shale, red-green variegated	1.0	31.0
Owner: City of Driller: Jack L			Limestone, with clay layers, cored 33.0 to 37.0 feet	6.0	37.0
Red clay, silty, plastic, sandy from 12.8 to 15.4 feet	15.4	15.4			
Tan sand, medium-grained, gravelly from 17.5 to 24 feet	8.6	24.0			

	•			ounty-continued	
	THICKNESS (f1)	DEPTH (ft)		THICKNESS (ft)	DEPTH (ft)
Well XW-30-2	7-719		Welt X	(W-30-33-101	
Owner: City of Driller: Trinity Engineering	Abilene Testing Corporatio	on		: R. F. Perry Robert Higgins	
Red clay, sandy (fill)	4.2	4.2	Soil	2	-
Red clay, silty, sandy to 5.0 feet, became moist at 10.0 feet			Clay	10	2
	7.8	12.0	Gravel (water)	3	12
Red sand, clayey, moist	1.5	13.5	Clay		15
Red clay, silty, moist, permeability test at 15.0 feet	2.5	16.0	Red Sand (water)	13 2	28 30
Red sand, clayey, wet	1.0	17.0	СІау	5	35
Clay, silty, soft, wet	2.5	19.5			
Red clay, silty, sandy	11.0	30.5	Well XV	V-30-34-301	
Gravel, sand	5.3	35.8		. Rematha Dubbs	
Limestore, gray, granular	0.1	35.9	Dritler: F	R. L. McKelvy	
			Red sand	22	22
Well XW-30-27	720		Gravel	4	26
Owner: City of A				1	27
Driller: Trinity Engineering T	esting Corporation	1	Red clay	5	32
Red clay, silty to 11.5 feet, sandy 10.6 to 11.5 feet, became moist			Well XW	/-30-34-304	
at 11.5 feet	15.0	15.0	0		
Sand, with clay lenses	5.5	20.5		nwest Enterprises ack Leonard	
Gravel, sand, clay	0.7	21.2	Top Soil	3	
Limestone, gray, dense to very finely crystalline	1.0	22.2	Clay		3
Shale, gray, variegated	0.8		Gravel	21	24
	0.0	23.0	Red bed	6	30
				3	33
Well XW-30-27-7	21		Well XW	-30-34-305	
Owner: City of At Driller: Trinity Engineering Te	oilene sting Corporation			west Enterprises ack Leonard	
Red clay, silty, with sandy clay			Top sail	3	3
lenses	10.0	10.0	Clay	20	23
Red clay, soft, moist, sandy to 11.0 feet			Coarse gravel	8	31
	5.0	15.0	Red bed	3	34
Red clay, moist, somewhat firmer than the above to 20.0 feet, and soft below 20.0, scattered					34
small gravel to 20.0 feet	11.0	26.0	Well XW-	30-34-306	
Sand, coarse-grained, gravel	0.5	26.5	Owner: Southv Driller: Ja	west Enterprises ck Leonard	
Sand, gravel	2.3	28.8	Top soil		_
Shale, gray variegated	1.2	30.0	Clay	3	3
			- /	23	26

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	THICKNESS (ft)	DEPTH (ft)		THICKNESS (ft)	DEPTH (ft)
Well XW-30-34	-306—Continued		Well XW-30-34	-802-Continued	
Gravel	6	32	Water-bearing gravel	2	35
Red bed	2	34	Shale	16	51
Well XW	-30-34-307		Well XW	-30-34-901	
	west Enterprises ack Leonard			ard W. Sharp, Jr. ack Leonard	
Top soil	3	3	Top soil	2	2
Red clay	21	24	Caliche	10	12
Gravel	6	30	Red clay	6	18
Red bed	2	32	Coarse gravel	11	29
			Red shale	4	33
Well XW	-30-34-501				
	l. R. Stuard ack Leonard		Well XW	-30-34-902	
				rd W. Sharp, Jr.	
Red clay	14	14		ack Leonard	
Sand and gravel	12	26	Top soil	3	3
ned bed	7	33	Sandy clay	10	13
Mall XM	-30-34-502		Sand and gravel	9	22
			Red shale	7	29
	hard L. Bowman lack Leonard		Well XW-	30-41-203	
Red clay	18	18		te's Mines Inc.	
Coarse gravel	8	26	Driller: Ro	bert Higgins	
Red shale	6	32	Soil	2	2
			Gravel	6	8
Well XW	-30-34-603		Clay	20	28
	mond J. Smith		Sandy clay	32	60
Driller:	G-M Drilling		Red sand (water), tight	1	61
Clay	13	13	Clay	68	129
Sand and gravel	9	22	Red sand (water)	3	132
Red and blue clay	8	30	Well XW-	30-42-209	
Well XW	-30-34-802			onard Camp on & Henderson	
	don Asbury, Jr. cCarrel & Son		Top soil, red	2	2

28

33

Red dirt

Red bed

Sand and gravel

.

29

11

2

31

42

44

28

5

Shale

Gravel

	THICKNESS (ft)	DEPTH (ft)		THICKNESS (ft)	DEPTH (ft)
v	Vell XW-30-42-501		Well XW	-30-50-231	,
	ner: L. D. Robinson : Henderson & Johnson			aham Brothers ler: —	
Red soil and dirt	32	32	Soil	8	8
Sand and gravel	7	39	Caliche	8	16
Red bed	3	42	Sand and gravel	5	21
w	/ell XW-30-43-702		Red bed	_	21
	ner: Roy Manahan er: D. W. Thompson		Well XW-	30-50-503	
Soil	2	2		Marshall, Jr. er: —	
Lime	80	82	Soil		
Sand and shale	163	245	Caliche	5	5
Sand (water)	17	262	Gravel	11	16
Red shale	18	280	Red bed	6 _	22 22
W	ell XW-30-50-211		Well XW-3	30-50-506	
	her: B. L. Standard ler: Leonard Street		Owner: R. Driller: Elr		
Soil	6	6	Soil	5	5
Caliche	11	17	Caliche	9	14
Sand and gravel	6	23	Gravel	8	22
Red bed	_	23			
			Well XW-3	0-51-405	
	ell XW-30-50-212		Owner: Ro Driller: Jac		
0111	Driller: -		Soil		
Soil	6	6	Sand and gravel	30 13	30
Caliche	11	17	Gravel and sandy clay	7	43
Sand and gravel	6	23	Rock	7	50
Red bed	_	23	Well XW-3	-	50
We	II XW-30-50-213		Owner: Marv Driller: Hayhurst Broth	vin Rutland	
Owner	r: Ed Brown Estate		Top soil	-	
	Driller: -		Caliche	1	1
Sand	33	33	Sand	1 12	2
Red bed	_	33	Purple and white clay	66	14 80

	THICKNESS (ft)	DEPTH (ft)		
Well XW-30-51-6010	Continued			
Sand (water)	24	104		
Red bed	4	108		
Well XW-30-51-701 Owner: Seburn Monroe Driller: —				
Soil	4	4		
Red clay	5	9		
Sand and gravel	11	20		
Red bed		20		

The following lithology logs are from three test holes cored and drilled by the Texas Water Development Board for use as observation wells in connection with an aquifer test conducted on well XW-30-50-628.

Text Hole XW-30-50-651

(00000)				
Soil, light to dark brown, clayey, some white caliche	3.5	3.5		
Clay, light to dark brown, orange, white, with some white caliche and fine to medium gravel, thin sand streaks in bottom 2.5 feet	5.5	9		
Sand, coarse, light orange and white with much coarse gravel	1.5	1 0.5		
Lost	0.5	11		
(Drilled)				
Gravel, coarse, mostly limestone with small vari-colored quartz pebbles	2	13		
Gravel, as above, with coarse sand	14	27		
Shale, blocky, red, with some gravel as above	3	30		
Test Hole XW-30-50-652				

(Drilled)

(Cored)

Soil, light to dark brown, clayey, with light orange to dark brown clay	5	5
Clay, orange	5	10
Gravel, fine, with coarse to very coarse sand	5	15

Test Hole XW-30-50-652Continued					
Gravel, coarse	10	25			
Shale, red, with gravel as above	2	27			

DEPTH

(ft)

THICKNESS

(ft)

Test Hole XW-30-50-653

(Drilled)			
Soil, light to dark brown, clayey, with orange clay in the bottom	5	5	
Claγ, orange	5	10	
Gravel, fine, mostly limestone with some chert, and coarse sand	10	20	
Gravel, as above	3.5	23.5	
Shale, red	6.5	30	

The following are lithology logs of the upper part of the hole of selected oil tests used for subsurface control. (See Table 10)

Well XW-29-48-810

E. Davis No. 1 E. Davis NW/4 Sec. 296, Blk. 64, H&TCRR Survey Elevation 2401 Derrick Floor

Missing	10	10
Lime	70	80
Lime, shaley	10	90
Lime	55	145
Sand, fine to medium-grained, porous	5	150
Conglomerate, sandy	40	190
Sand, limey	15	205
Conglomerate, porous	65	270
Red shale	-	270

Well XW-29-56-111

Condor No. 1 Stokes Sec. 257, Blk. 64, H&TCRR Survey Elevation 2388

Soil	10	10
Lime	45	55
Shale and lime	65	120
Clay	10	130

THICKNESS DEPTH

THICKNESS	DEPTH
(ft)	(ft)

	(ft)	(ft)
Well XW-29-56-11	1–Continued	
Sandy lime	10	140
Shale	7	147
Lime	8	155
Shale	10	165
Clay	30	195
Sand and lime	15	210
Clay	15	225
Shale, gray	160	385

Well XW-30-43-901—Continued

Caliche, shale	15	55
Red shale	25	80
Sand	15	95
Lime	40	135
Red shale	5	140
Sand	45	185
Shale	. –	185

Well XW-30-43-902

West Central No. 3-A Chrane Sec. 9, Blk. 7, SPRR Survey Elevation 2120 (estimated)

Caliche	25	25
Red bed and sand	70	95
Sand	25	120
Gravet	10	130
Red shale	-	130

Well XW-30-43-903

Humble No. 2 Mrs. V. J. Kemper Sec. 14, Blk. 7, SPRR Survey Elevation 2239 Ground

Lime	5	5
Caliche	20	25
Lime	55	80
Sand	15	95
Shale	25	120
Sand	37	157
Shale	13	170
Sand	60	230
Gravel	12	242
Lime	-	242

Well XW-30-51-210

J. N. Burnham No. 1 Amyz Sec. 26, Blk. 6, SPRR Survey Elevation 2160

Soil	15	15
Gravel	5	20
Red bed	2	22

Well XW-29-56-112

R. P. Fisher No. 1 Elm Cattle Co. Sec. 275, Blk. 64, H&TCRR Survey Elevation 2465 Derrick Floor

Missing	100	100
Lime, buff, earthy	100	200
Lime and sand	5	205
Lime	10	215
Sand	5	220
Lime and sand	25	245
Lime	10	255
Sand, some lime	50	305
Dolomite		3 0 5

Well XW-29-56-505

Bert Fields No. 1 Sears Sec. 223, Blk. 64, H&TCRR Survey Elevation 2340

Soil	5	5
Lime	65	70
Sand (water at 100 feet)	30	100
Shale, gray	20	120
Sand (water in base)	60	180
Shale, red	—	180

Well XW-30-43-901

	West Central No. 1 W. O. Black Sec. 3, Blk. 7, SPRR Survey Elevation 2191 Ground	
Lime	15	
Lime and clay	25	

15

40

	THICKNESS (ft)	DEPTH (ft)		THICKNESS (ft)	DEPTH (ft)
Well XW-30-51-21	0-Continued		Well XW-30	-51-304	
Sand	8	30	West Central Drilli	-	
Shale	15	45	Sec. 23, Blk. 6, SPRR Survey Elevation 2194 Ground		
Lime	5	50	Lime	78	78
Red bed	10	60	Red bed	5	83
Lime	50	110	Sand	17	100
Red bed	30	140	Lime and shale	40	
Sand (water)	5	145			140
Red bed	_	145	Sand	10	150
			Lime and shale	15	165
			Sand, gravel (water)	53	218
			Red bed	-	218

Table 7,--Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas

Analyses are in milligrams per liter unless otherwise noted, except Percent sodium, Sodium-Adsorption Ratio (SAR), Residual Sodium Carbonate (RSC), Specific Conductance, and pR. Analyses were performed by the Texas Department of Health Resources except as indicated by footnote.

neeren nebentette	
	Pl, Lueders Formation; Par, Arroyo Formation; Pv, Vale Formation; Pvb, Bullwagon Dolomite Memeber of Vale Formation; Fc, Choza Formation; Fcm, Merkel Dolomite Member of Choza Formation; Fsa, San Angelo Formation; Ka, Antlers Formation; Kf, Fredericksburg Group; Qs, Seymour Formation; Qu, Undivided Quaternary Surficial Deposits; Qal, Alluvium.

	WELL	AQUIFER	DEPTH OF WELL (FT)		TE OF LECTION	SILICA (S10 ₂)	IRON (Fe)	CAL- CIUM (Ca)	MAGNE - SIUM (Mg)	SOD- IUM (Na)	POTAS- SIUM (K)	BICAR- BONATE (HCO3)	SUL- FATE (SO ₄)	CHLO- RIDE (C1)	FLUO- RIDE (F)	NI- TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDUCTANCE (MICROMHOS AT 25°C)	pll	PER- CENT SOD- IUM	SAR	RSC
																		4,250	1,880	4,850	7.6	44.7	7.0	0.0
	XW-29-31-904	Psa	28	May	4, 1970	12		259	301	700		410	2,100	670	8.2	0.4			760	2,200	7.7	41.1	3.9	.0
	906	Psa, Pcm	80		do	13		138	100	243		282	610	275	3,1	11		1,530	1,070	3,300	7.7	45.0	5.3	.0
	32 - 709	Pc	100	Nov.	9, 1968	29		137	177	404		440	830	475	2.8	77			1,070	2,920	7.4	34.0	3.4	.0
5/	714	Psa	23	1	do	31		132	184	257		377	492	540	3.4	110		1,930	1,090	3,000	7.5	35.1	3.6	.0
- 5/	720	Psa	26	ł	do	29		130	191	276		377	520	540	1.8	110		1,980		6,250	7.2	43.2	7.7	.0
	721	Psa	40	May	4, 1970	20		460	340	890		401	2,180	1,270	2.8	16		5,400	2,550	2,000	7.5	26.8	2.2	.0
	907	Pc	80	Nov.	4, 1969	16		220	89	155	3	2.04	780	162	.9	24	1.5	1,550	910		7.6	34.7	2.4	.0
	909	Pc	40	Nov.	6, 1969	7		89	70	125		211	215	257	.6	24		890	510	1,490	1	41.0	3.7	.0
	39-301	Psa	85	May	4, 1970	21		130	94	227		414	391	302	1.2	40		1,410	710	2,080	7.6	34.4	2,4	.0
	601	Psa	60	May	8, 1970	37		78	82	129		458	135	120	2.0	154		960	530	1,440	7.9		2.3	.0
	602	Psa	97		đo	17		109	50	118		338	297	102	.8	< .4		860	478	1,270	7.8	34.9	2.4	.0
	902	Psa	130	May	19, 1970	17		98	67	128	3	414	202	158	.9	28	.5	910	520	1,410	7.4	34.7	1.7	.0
	905	Psa	130		do	18		122	52	88	2	367	216	122	.4	3.5	.4	800	520	1,210	7.5	26.8		.8
	906	Psa	33		do	21		82	17	44	< 1	390	33	10	.6	1.5	i .4	402	276	632	7.8	25.7	1.2	.0
	907	Psa	90		do	18		112	22	121	< 1	288	166	117	2.1	57	.4	760	370	1, 157	7.4	41.5	2.7	
	908	Psa	125		do	17		86	48	69	4	326	147	99	.6	< .4	.4	630	413	999	7.5	26.4	1.5	0.
	40-105	Psa	33	Nov.	5, 1969	19		59	62	190		306	278	203	2.0	< .4	•	960	402	1,520	7.7	50.7	4.1	.0
	201	Pc	33		. 15, 197	1		375	181	391	5	304	1,560	407	1.1	90	2.2	3, 170	1,680	3,650	7.5	33.5	4.1	.0
	202	Pc	80		do	8		114	75	140		22	620	183	.8	< .0	4	1,150	590	1,660	6.3	33.9	2.5	.0
	202		55	May		D 29		135	78	74		410	222	163	1.2	30		930	660	1,420	7.4	19.7	1.3	
	203	Pc	90	,	do			373	187	336		306	1,280	650	1.0	< .	4	2,980	1,700	3,540	7.0	30.1	3.6	
			100	Oct	. 20, 196	9 27		136	107	100		410	302	121	2.4	189		1, 190	780	1,700	7.4	21.8	2.0	
	301		100		do	16		58	36	27		342	30	18	.9	14.	0	368	293	620	7.6	16.6	6.8	
	303		100		do	13		29	14	20		356	< 4	30	.7	< .	4	325	131	677	7.1	25.4	7.8	
	307							540	82	154		205	1,570	126	.9	39		2,630	1,700	2,820	7.4	16.5	1.6	.0
	312	1	93	Nov				112	44	61	2	284	241	51	.8	43	.6	720	462	988	7.6	22.3	1.2	
	313		98	Feb		20		76	55	120		377	121	136	1.7	68		790	416	1,220	7.5	38.6	2.6	
	315	Pc	100	1	do	24		/*					1				·							

ŀ	ÆLL	AQUIFER	DEPTH OF WELL (FT)		ATE OF LLECTION	SILICA (S10 ₂)	IRÓN (Fe)	CAL- CIUH (Ca)	MAGNE - SIUM (Mg)	SOD- IUM (Na)	POTAS- SIUM (K)	BICAR- BONATE (HCO ₃)	SUL- FATE (SO ₄)	CHLO- RIDE (C1)	FLUO- RIDE (F)	NI- TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDUCTANCE (MICROMHOS AT 25°C)	pН	PER- CENT SOD- IUM	SAR	RSC
XW	-29-40-319	Pc	110	May	7, 1970	15		570	89	190		198	1,740	107	1.0	26		2,840	1,790	2,950	7.3	18.8	2.0	0.0
	320	Pc	100		do	18		91	45	82		346	138	94	.7	15	• •	650	413	1,064	7.2	30.1	1.8	.0
	374	Pr	túö		đo	19		23	48	62		355	112	81	.6	53	••	640	429	1,002	7.5	24.0	1.3	.0
	327	Pc	92	May	14, 1970	22		160	75	97	3	326	257	165	.7	176	0.5	1,120	708	1,640	7.5	. 22.9	1.6	.0
	328	Pc	110		do	21		113	71	94	2	383	143	179	.7	53	.4	870	570	1,400	7.6	26.2	1.7	.0
	401	Psa, Pc	225	May	8, 1970	13		111	69	110		364	297	135	.6	< ,4		920	560	1,390	7.6	29.9	2.0	.0
¥ 5/	501	Pc	65	Aug. May		36		70 600	28 383	87* 630	60	451 580	48 1,390	18 1,740	 1,0	38 11	.7	511 5,100	287 3,060	6, 330	7.3	30,3	4.9	
<u>y</u> y	502	Pc	40	Aug. May	. 28, 1939 19, 1970	17		532 610	275 290	446* 387		12 265	2,742 2,600	400 437	.3 1.1	< 20 14	 5.7	4,401 4,490	2,460 2,720	4,570	 7,5	23.6	3.2	
	503	Pc	80		20, 1970	18		425	186	283	5	303	1,000	760	1.0	58	1.4	2,890	1,830	3, 770	7.5	25.2	2.9	
	601	Pe	110	1	. 17, 1969	25	< 0.02		45	63	5	377	48	78	1.0	96	.4	640	420	1,010	7.6	24.2	1.3	
	601	Pe	108	1	, 20, 1969	18	69.0	342	63	132	4	273	1,020	74	1.3	10.0	1.1	1.870	1,110	2.070	7.2	20.4	1.7	
	606	Pc	120	1	. 5, 1969			98	84	114		470	133	194	1.7	40		920	590	1,500	7.6	29.6	2.0	
	607	Pc	80		do	28		72	79	137		421	101	198	3.0	94.5		920	510	1,460	7.5	37.0	2.6	
	608	Pc	125		do	24		103	80	164		434	145	252	2.0	99		1,080	590	1,730	7.8	37.8	2.9	
	609	Pc	100	May	18, 1970	20		132	122	143	4	323	127	392	1.0	2 1 2	1.0	1,310	830	2,030	7.8	27.0	2.2	
	701	Psa	52	May		13		229	30	194	6	364	300	362	.8	< .4	.8	1,320	700	1,990	7,6	37.5	3.2	
	703	Psa	55		do	27		161	305	453	3	540	1,160	640	2.8	6.5	1.6	3, 080	1,660	4,000	7.8	37.2	4.8	-
	801	fc	34	Dec	. 5, 1969	18		82	42	95		334	111	66	.7	134		710	377	1,067	7.5	35.4	2,1	
	902	Pc	70	May	5, 1970	21		75	43	85		310	36	164	1.0	31.0		610	367	1,030	7.5	33.6	1,9	· ·
	904	Pc	Spring		do	17		92	47	67		348	129	104	1.1	2.0		630	423	1, 013	7.6	25.7	1.4	· ·
<u>3</u> 5	55-902	Рва	140	Feb	. 8, 1939 . 17, 1969			210 174	146 119	286* 265		2 32 334	777 650	530 382	1.5 2.5	< 20 < .4		2,063 1,770	1, 125 925	2,500	7.3	38.4	4.0	
	56-701	Psa	80		. 23, 1969	26		134	79	237		365	302	264	3.2	2 5 2		1,480	660	2,100	8.0	44.0	4.0	.
	702	Psa	90	Feb	. 24, 1939 . 22, 1969			80 96	47 41	141* 137		256 323	294 220	130 98	1.4	< 20 75.0		818 840	394 407	1,260	7.8	42.2	2.9	
3 5	703	Psa	20	Feb				61 88	36	198* 169		366 394	187 154	84 134	3.0	149 143.0		895 960	303 413	 1,420	7.6	47.1	3.5	
34 54	704	Psa	22	Feb	. 24, 1939	(139 88	75	199* 150		366 456	71 60	70 269	2.5	765		1,499 910	657 500	1, 550	7.6	39.4	2.9	
				Nov	7. 17, 1969				27	136		411	243	139	1,6	18.5	j	940	510	1,410	7.3	36.8	2.6	.
	801	Pc	125		d0	17		158 146	65	84	7	315	117	245	.5	114.8		960	630	1,540	7.6	22.2	1.5	.
	30-25-702		70	Dec	z, 5, 1969	22	.16	254	86	99		254	620	2.02	.7	83		1,490	990	1,990	7.3	17.9	1.4	
	703		120 80		do do	22		97	51	124		238	204	177	.8	84		880	452	1,360	7.5	37.3	2.5	.
	704	Pc, Pvb		Me				73	100	186		472	256	170	2.4	122		1,160	590	1,700	7.7	40.5	3.3	
5	712 27-912		40	Apr	r, 7,1970			580	193	540		182	458	1,960	.9	70		3,910	2,230	5,200	7.2	34.4	5.0	
1	2, 744	1																	l			<u> </u>	1	

Table 7.--Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

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DEPTH CAL-MAGNE -SOD-BICARsπ.-CHLO-FLUO-POTAS-NT-DIS-TOTAL SPECIFIC PER OF DATE OF SILICA TRON CTIM STIM LUM SIUM BONATE FATE RIDE RIDE TRATE BORON SOLVED HARDNESS CONDUCTANCE CENT WELL AQUIFER WELL COLLECTION (S102) (Fe) (Cat) (Hg) (Na) (K) (HCO₂) (\$0,) (C1) (F) (NO2) (B) SOLTES AS CaCO3 (MTOBONHOE p!! SOD RSC SAR (\mathbf{PT}) AT 25°C) TIM 5/ XW-30-27-913 P1 30 Apr. 7, 1970 17 451 - -139 461 - -170 382 1,480 0.6 85 - -3,100 1,700 4,700 7.1 37.1 4.9 0.0 33-501 Pvb 42 May 20, 1970 20 --196 143 337 < 1 329 580 550 1.1 143 0.7 2,130 1.080 3,020 7.7 40.4 4.5 .0 503 Pvb 30 do 17 --150 78 317 2 350 333 453 .9 120 .6 1.640 700 2,470 7.6 49.6 .0 5.2 504 Pvb 50 do 19 - -123 52 182 2 306 206 206 .8 176 .6 1.120 520 1,690 7.6 43.1 3.5 .0 506 Pv 60 June 13, 1970 13 403 248 730 4 320 1,080 1,510 1.2 54 2.3 4,200 2.030 5,290 7.2 43.8 .0 7.0 34-401 Ρv 58 Apr. 14, 1970 17 • • 53 86 451 950 419 179 3.0 . 4 - -1.680 489 2,350 8.1 66.7 5.73 8.9 601 Par? - -Apr. 3, 1970 15 55 104 176 - -510 127 287 2.7 14 --1,030 560 1,730 40.3 7.9 3.2 .0 35-201 Apr. 6, 1970 Par 60 11 68 128 221 630 155 287 3.2 143 - -1,330 690 2,080 40.9 7.8 3.7 .0 202 Par 60 do 16 --157 570 85 510 720 650 1.2 3.5 - -2,460 860 3.450 8.2 59.1 8.7 .0 301 Р1 31 July 12, 1939 - -- -342 52 126 - -20 - -551 - -Apr. 7, 1970 20 - -780 293 1,750 - -242 600 4.320 . 9 143 8,030 3,160 10,500 7.1 54.5 13.5 .0 601 P1 20 June 28, 1939 ---114 40 75* --293 2.02 116 .. < 20 - -691 450 Apr. 7, 1970 12 - -186 67 230 < 265 --357 496 .9 1,430 740 2,280 40.3 7.5 3.7 . Û 602 P1 16 do 21 174 67 ---250 - -426 297 415 2.1 29 1.460 --710 2,250 7.3 43.4 4.1 .0 41-201 Pc, Pv 108 June 16, 1970 23 ---93 52 94 2 307 240 98 .7 8.5 447 .5 760 1,128 7.5 31.2 1.9 .0 204 Pc, Pv 136 June 17, 1970 18 - -349 75 240 5 214 1,090 257 .9 5.5 1.5 2,150 1,180 2,610 7.4 30.5 9.6 .0 43-201 Par Apr. 2, 1970 --15 --124 86 253 - -399 297 406 1.1 29 - -1,410 670 2,180 7.6 45.2 4.3 .0 202 Par 35 May 25, 1939 26 13 118* 122 85 98 - -60 - -463 118 - -Apr. 2, 1970 21 - -101 89 337 - -409 275 409 185 5.7 2,400 ---1,620 620 7.6 54,1 5.9 .0 801 Par 25 Mar. 25, 1970 12 < 0.02 109 26 36 < 1 345 70 56 27 .5 • 2 510 378 808 7.7 17.3 .0 .8 802 Par Spring Mar. 26, 1970 30 173 . . 34 130 - -488 108 248 < .7 .4 --960 570 1,500 7,9 33.2 2.4 .0 57-301 Pc 24 June 17, 1970 34 174 - -83 510 5 442 463 690 2.4 65 2,240 780 7.7 .6 3,260 58.4 7.9 .0 Creataceous System 29-47-601 Kf 25 Dec. 12, 1969 16 99 ---35 59 ---318 58 109 .7 41.0 570 391 933 7.2 24.7 1.3 .0 604 Kf Spring do 11 - -78 26 12 1 318 19 21 .7 28 0.1 353 301 596 7.5 7.7 .29 .0 901 Ка 280 Jan. 16, 1970 8 ---58 27 31 312 ---46 13 < 1.2 337 259 20,5 . 4 555 7.8 .8 .0 902 Кf Spring do 13 - -69 22 33 ---284 37 31 .7 15 361 264 598 8.0 21.3 . 9 .0

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Table 7Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent AreasConti
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See footnotes at end of table.

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WELL	AQUIFER	DEPIH OF WELL (FT)	DATE OF COLLECTION	SILICA (S10 ₂)	IRON (Fe)	CAL- CIUM (Ca)	HAGNE - SIUM (Mg)	SUD- IUM (Na)	POTAS- SIUM (K)	BICAK- BONATE (HCO3)	SUL- FATE (SO ₄)	CHLO- RIDE (C1)	FLUO- RIDE (F)	N1- TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDUCTANCE (MICROMHOS AT 25°C)	рН	PER- CENT SOD- IIM	SAR	RSC
XW-29-48-701	Kf	Spring	Dec. 11, 1969	11		80	25	20		338	20	22	0.6	14		359	302	573	7.7	12.5	4.9	0.0
703	Kf	Spring	Jan. 16, 1970	9		75	26	11		326	20	13	.7	6.5		322	296	537	7.8	7.4	.3	.0
704	Kf	Spring	do	9		89	26	9		346	23	14	.6	14		355	329	575	7.7	5.6	.2	.0
705	Ka	260	do	8		60	36	52		370	83	18	1.2	< .4		440	300	713	7.5	27.2	1.3	.07
807	Kf	Spring	Feb. 13, 1970	8		70	33	12		348	24	19	.6	< .4		338	312	578	7.7	7.4	.3	,0
808	Kf	Spring	do	9		84	28	8		360	20	13	.4	4.5		344	326	583	7.7	5.0	.2	.0
55-602	Ka	75	Mar. 13, 1970	16		88	14	23		305	39	20	.5	6.5		358	277	577	7.3	15,2	.6	.0
603	Ка	75	do	11		102	11	9		282	22	20	.3	39		353	302	580	7.4	5.9	.2	.0
604	Ka	35	do	7		78	14	7		276	23	8	.3	< .4		273	252	460	7.7	5.8	.2	.0
56-101	Ka?	60	Nov. 13, 1969	11		79	20	7		314	16	10	.5	3.5		302	274	510	7.6	5.4	.1	.0
102	Kf	Spring	Jan. 16, 1970	10		68	19	12		279	14	15	.6	5.5		2 82	247	475	7.8	9.2	.3	.0
103	Kf	Spring	do	6		69	21	9		290	14	12	.6	5.5		281	208	477	7.8	6.9	.2	.0
104	Ka	300	Jan. 15, 1970	10		71	25	15	1	307	20	23	.7	4.8	0,1	322	280	557	7.5	10.4	.4	.0
105	Κf	Spring	do	8		67	27	11		299	20	21	.7	8.5		311	277	519	7.7	7,8	.3	.0
106	Kf	Spring	do	9		71	19	9		284	13	16	.3	7.0		284	256	474	7.9	6.9	.2	.0
107	Kf	Spring	do	5		75	19	7	• -	300	17	9	.5	2.0		283	267	475	7.7	5.2	. 2	.0
108	Ka	300	do	10		84	21	26		271	23	63	.5	21		382	297	652	7.8	16.0	.7	.0
109	Kf	Spring	do	15		96	30	21		381	28	37	.5	17		4 32	364	718	7.4	11.3	.5	.0
110	K£		Feb. 19, 1970	10		84	31	9		390	12	14	.6	3.5		357	339	608	7.6	5.4	.2	.0
<u>3</u> ; <u>5</u> , 201	Kf	Spring	Feb. 28, 1939 Nov. 5, 1969	13		84 72	22 22	8* 12		336 312	13 12	19 13	.6	< 20 4.5		311 303	299 269	512	7.6	8.8	 .3	.0
202	Ka?	68	do	12		67	18	11		275	10	13	.6	10.5		278	242	470	7.9	8.7	.3	.0
2 04	K£	Spring	Feb. 13, 1970	10		72	22	10		311	12	12	.6	3.5		296	270	506	7.8	7.6	.3	.0
205	Kf	Spring	do	9		85	37	11		415	20	15	.5	2.0		384	367	646	7.9	6.2	.3	.0
<u>3 5</u> / 206	Ка	151	feb. 28, 1939 Feb. 18, 1970	 13		39 63	21 17	18* 16	< 1	226 267	11 12	18 16	.6	< 20 9.5	.1	218 279	183 230	 474	 7.7	12.9	5	.0
207	Ка?	90	do	15		62	18	11		260	6	17	.5	12.0		270	232	459	7.8	9.7	.3	.0
208	Kf	Spring	do	12		72	22	8		307	10	13	.5	2.0		291	271	500	7.9	6.2	.2	.0
<u>1</u> / <u>5</u> / 301	Ka		Aug. 10, 1961 Feb. 18, 1970	11 11		61 89	18 23	14* 17		262 333	9.2 34	16 27	.5 .5	12 10.5		2 71 377	226 316	477 622	7.0 7.7	12 10,5	.4	
302	Кſ	Spring	Feb. 18, 1970	12		65	32	22		345	23	23	.6	< .4		348	292	584	8.1	14,1	.6	.0
303	Ка	125	do	10	- ~	110	45	22		382	112	53	1.2	1.5		540	458	859	7.6	9.5	.5	.0
304	Ка	280	do	8		67	31	40		338	68	28	1.2	< .4	- •	409	294	675	7.7	22.8	1.0	.0
502	Ka	72	Nov. 13, 1969	11		138	6	19		310	28	44	.2	78.0		476	370	756	7.3	10.0	.4	.0
<u>5</u> 503	Ка	90	Feb. 10, 1970	11		74	25	9		328	15	10	.5	5.5		312	286	523	8.2	6,2	.2	.0
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Table 7.--Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

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Table 7Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent AreasContinued	

WELL	AQUIFER	DEPTH OF WELL (FT)	DATE OF COLLECTION	STLICA (S10 ₂)	IRON (Fe)	CAL- CIUM (Ca)	MAGNE - STIM (Mg)	SOD- TITM (Na.)	POTAS- STIM (K)	BICAR- BONATE (HCO3)	SUL- FATF (SU ₄)	CHLO- RIDF (U1)	FLUO- RIDF (F)	NI- TRATF (NU3)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS Callog	SPECIFIC CONDUCTANCE (MLUROMHUS AT 25°C)	рп	PER- CENT SOD- IUM	SAK	RĐÚ
y xw-29-56-504	Kf	Spring	Feb. 10, 1970	10		79	43	16		388	39	22	0,5	21		422	376	690	8.1	8.6	0.4	0.0
ý 601	Ka	90	do	10		74	27	14		340	31	11	.6	< .4		335	298	519	7.6	9.0	.3	.0
y 901	Ka	48	Mar. 10, 1970	12		98	28	25		406	52	13	.5	1.8		431	360	714	7.5	13.0	.6	.0
y 902	Ka	90	do	11		84	27	12		350	36	12	.5	< .4	••	355	322	595	7.5	7.7	.3	.0
64-301	Ка	50	do	18		99	29	11		375	28	14	.7	34		418	366	675	7.8	6.3	.3	.0
30-41-401	Ka	270	Feb. 17, 1970	11		112	38	14		393	110	21	.6	< ,4		500	435	787	7.4	6.6	.3	.0
701	Ка	220	do	11		90	20	15		334	44	15	.3	< .4		359	308	594	7.7	9.5	.4	.0
703	Ka	Spring	do	17		119	8	14		314	44	35	.3	11		402	333	649	7.7	8.1	.3	.0
802	Ka	145	Aug. 7, 1970	13	< 0.02	142	10	24	< 1	340	24	96	.3	< .4	0,1	476	394	806	7.7	11.6	.5	.0
43-602	Ка	20	May 12, 1970	15		107	17	14	< 1	378	32	20	.3	< .4	.1	391	337	641	7.3	8.4	.3	.0
y 703	Ka	260	Apr. 2,1970	10		96	16	35		336	50	30	.3	14		416	307	679	7.9	19.6	.9	.0
803	Ка	Spring	Mar. 26, 1970	19		118	22	66		433	50	96	.6	< .4		590	386	925	7.7	27.1	1.5	.0
49-101	Кf	Spring	Feb. 18, 1970	12		83	36	14		344	59	27	.5	< .4		401	355	668	7.3	8.0	.3	.0
102	Ka	145	do	8		95	38	14		447	17	21	2.4	< .4		415	394	722	7.4	7.3	.3	.0
Sy 401	Ka	294	Mar. 5, 1970	10		101	36	20		438	36	31	.5	6.5		457	398	763	7.4	9.8	.4	0.
y 402	Ka	> 250	do	11		85	24	7		357	21	7	.5	< .4		332	313	516	7.5	4.7	.2	.0
y 403	Kf	Spring	do	20		121	27	11		459	28	16	.3	< .4		449	413	727	7.6	5.4	.2	.0
601	Ka	Spring	Jan. 29, 1970	17		123	22	23	∼ 1	418	46	38	.6	< .4	. 1	476	396	751	7.8	11.1	.5	.0
602	Ka	17	do	20		115	25	34		451	42	29	.7	< .4		488	388	776	7.4	16,1	.8	.0
603	Ka	31	do	18		135	38	77		439	128	95	1.0	42.5		750	495	1,149	7.5	25.2	1.5 	0.
5y 605	Ka	90	Mar. 10, 1970	16		148	30	30		337	216	26	1.0	18		650	492	937	7.7	11.8	.6	0.
5y 607	Kf	Spring	do	2		85	16	24		298	32	34	.3	< .4		340	279	609	7.5	15.6	.6	0.
ý 901	Ka	15	do	15		123	18	61		472	78	38	1.0	< .4		570	382	886	7.6	25.9	1.4	.11
50-801	Ka	22	June 17, 1970	19		87	21	12	2	317	55	5	1.2	< .4	.1	358	303	558	7.7	7.5	.3	.0
51-201	Ka	102	Mar. 18, 1970	13		185	12	17		388	39	58	.3	143		660	510	922	7.4	6,7	.3	.0
203	Ka	97	do	12		105	10	12		348	16	17	.4	< .4		343	304	570	7.3	8.1	.3	.0
204	Ка	104	do	10		76	23	6		294	43	4	.7	3.0		311	285	514	7.7	4.4	.2	.0
205	Ka	87	do	13	~ -	95	21	9		342	36	11	.4	12		365	325	585	7.7	5.9	.2	0.
208	Kf	Spring	do	7		71	27	8		338	21	9	.5	5.0		315	291	506	7.7	5.5	.2	.0
209	Kf	Spring	do	7		97	8	8		310	22	8	.2	< .4		302	275	509	7.7	5.8	.2	.0
301	Ka	102	do	11		72	32	7		357	12	10	.8	< .4		321	312	550	7.3	4.4	.2	.0
302	Ka	118	Mar. 16, 1970	12		85	20	12		351	15	13	.3	< .4		330	296	554	7.4	8.3	.3	.0
303	Kf	Spring	Mar. 18, 1970	9		102	17	7		361	23	9	.4	3.5		349	325	573	7.7	4.5	.2	.0

	WELL	AQUIFER	DEPTH OF WELL (FT)	DATE OF COLLECTION	SILICA (S10 ₂)	IRON (Fe)	CAL- CIUM (Ca)	MAGNE - SIUM (Mg)	SOD- IUM (Na)	POTAS- SIUM (K)	BICAR- BONATE (HCO ₃)	SUL- FATE (SO4)	CHLO- RIDE (C1)	FLUO- RIDE (F)	NI - TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDUCTANCE (MICROMHOS AT 25°C)	рН	PER - CENT SOD- LUM	SAR	RSC
4 L	xw-30-51-405 406	Ka Ka	50 51	Mar. 18, 1970 do	12		119 	18 	22		344 	40 	54 	0.3	12 	 	446 	370	734 	7.4 	11.3 	0.5	0.0
ע	501	Ka	45	do	12		106	13	17		340	30	21	.5	10		377	320	604	7.6	10.2	.4	.0
	601	Ка	101	June 18, 197	0 14		151	13	19	< 1	327	15	61	.2	112	0,1	550	430	868	7.4	8.9	.4	U. U
	602	Ка	72	do	14		93	12	10		325	12	19	. 2	< .4		320	282	524	7.5	7.4	.3	.0
		L	1				L	1		(uaternary	System	l		L								.
	29-40-802	Qal	29	Dec. 5, 196	9 18		231	252	530		680	1,220	670	1.1	< .4		3,260	1,610	4,150	7.5	41.6	5.7	.0
	901	Qa1	40	do	20		128	137	250	3	445	630	288	1,3	9.0	1.5	1,680	880	2,340	7.4	38.0	3.7	.0
	48-201	Qal	20	Nov. 12, 196	9 24		84	107	319		570	620	134	3.4	35.0		1,610	650	2,210	7.7	51.6	5.4	.0
	206	Qu	Spring	Mar. 13, 197			127	74	225	< 1	348	422	174	2.2	176	.8	1,400	62.0	1.920	7.5	44.0	3.9	.0
	30-25-707	Qs	40	Mar. 6, 197			49	41	47		336	33	18	1.5	62		436	2 92	687	7.7	25.9	1.2	.0
5/	27-706	Oal	33	Apr. 6, 197		1.1	72	169	570	2	770	181	960	1.2	< .4	1.6	2,350	870	3,770	7.9	58.6	8.4	.0
3	708	Qal	32	Apr. 20, 197			82	112	478		630	590	415	1.2	6.5		2,010	670	2,840	7.6	60.9	8.1	.0
	710	Qal	15	do	19	. 30	83	39	31	< 1	322	18	97	.3	9.5	.3	455	368	786	7.7	15.4	.7	.0
	712	Qal	32	do	17		92	196	870		790	1,280	680	2.2	31		3, 560	1,040	4,550	7.7	64.5	11.7	0.
	714	Qa.1	34	do	16		71	193	840		/6Ŭ	1,220	640	2.5	39		3,400	970	4,370	7.8	65.4	11.8	.0
	716	Qal	38	do	16		41	75	309		710	243	156	2.0	25		1,220	413	1,840	7.9	62.0	6.7	3.47
	719	0a1	36	do	1.2		46	28	176		437	193	47	1.2	< .4		720	231	1,081	7.7	62.3	5.1	2.54
	720	Qal	23	do	16		100	235	1,010		960	1,620	710	2.6	< .4		4,170	1,220	5,030	7.6	64.3	12.6	0,
5/	34-301	Qa1	32	Apr. 10, 19	10 17		100	135	286		690	433	249	1.3	80		1,640	807	2,290	7.6	43.5	4.4	0.
5/	302	Q=1	28	Apr. 14, 19			71	56	154		560	159	91	1.2	< .4		820	409	1,270	7.5	45.0	3.3	.92
5/	303	Qal	24	do	12		28	36	177		573	111	18	2.2	< .4		670	215	1,040	7.9	64.2	5.3	5.10
5		Qal	33	do	12	4.0	28	27	250	< 1	680	72	69	1,3	< .4	1.6	800	183	1,240	8.0	74.8	8.1	7.50
5		Qal	32	do	12		23	16	219	< 1	510	152	26	2.0	< .4	1.3	700	124	1,099	7.7	79.4	8.7	5.87
	501		33	Apr. 16, 19	70 24		49	75	182		540	168	157	1.6	9.5	5	930	432	1,460	7.8	47.8	3.8	.14
	502		32	do	22		68	57	386		680	335	256	1.3	10		1,470	405	2,150	7.8	67.5	8.4	2.9
5			30	Apr. 10, 19	70 18		53	40	55		281	103	45	1.0	28		481	299	759	7.6	28.4	1.2	.0
1	801		45	May 6, 19			83	48	111		520	68	102	1,0	5.	5	700	404	1,125	7.4	37.3	2.4	.49
	802		51	do	10		33	35	148		550	15	61	1.7	< ./	4	570	226	955	7.7	58.7	4.3	4.43
з	5/ 803		39	Mar. 18, 19	39 70 29		81	42	54* 126		537 630	24 67	20 46	1.0	< 20 21		485 720	376 389	1, 110	7.4	41.3	2.8	2.5
	901	Qal	37	May 6, 19 May 13, 19	i		59	29	48		264	76	51	.5	4.	5	409	265	669	7.5	28.4	1.3	.0
			29	do 10, 10	20		77	65	126	< 1	590	108	98	.8	< .	4 .4	790	461	1,240	7.6	37.3	2.6	.5
	902		15				220	70	164		498	290	288	.6	110		1,410	840	2,050	7.5	29.8	2.6	.0
5	35-401	Qal	1 15	Apr. 0, 19																	<u> </u>		

Table 7.--Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

Table 7.--Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

	WELL	AQUIFER	DEPIH OF WELL (FT)	DAT	E OF ECTION	SILICA (S10 ₂)	IRON (Fe)	CAL- CIUM (Ca)	MAGNE - SIUM (Mg)	SOD- IUM (Na)	POTAS- SIUM (K)	BICAR - BONATE (HCU3)	SUL- FATE (SO ₄)	CHLO- RIDE (C1)	FLUO- RIDE (F)	NI- TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDUCTANCE (MICROMHOS AT 25°C)	pli	PER- UENF SOD- IUM	SAR	RS
	W-30-35-403	Qa l	19	Apr.	8, 1970	25		249	229	570		550	760	1,050	1.0	70		3,220	1,566		-	1		
Ý	701	Qal	24		do	25		82	62	192		600	154	131	1.6	68		1,010		4,470	7.4	44.2	6.3	0.
(5)	41-301	Qa 1	40	Mar.	6, 1939			150	122	694*		390	1,087	635	.7	45		2,925	461	1,550	7.6	47.5	3.9	
i <u>5</u> i	302	Qal	22		do .5, 1970	17		191 103	158	293*		659	825	260		< 20		2,051	876 1,128					-
	42-201	Qa 1	44		0, 1969	15		139	378 96	590		640	1,530	650	4.8	82	* *	3,670	1, 128	4,050	7.6	41.5	19.1	-
	203	Q a 1	45	}	lo	15	l	120	71	198		550	492	149	.8	< .4		1,360	740	1,890	7.5	36.7	3.2	
	204	Qa 1	43		io	12	0.56	83	36	284		451	434	252	.8	25		1,420	590	2,100	7.8	51.1	5.1	
	2.06	Qa 1	32		3, 1970	17		77	63	43	1	366	67	58	.9	< .4	0.3	482	356	800	7.8	20,6	.9	
	207	Qu	11		lo	19		79	17	28		560	180	53	.9	33		840	451	1,250	7.6	39.9	2.8	
5	208	Qa 1	38	Aug. 1	8, 1939			67	17	4*		344	16	17	.7	1.5		348	270	570	7.8	18.3	.7	
				May 1	3, 1970	17		118	76	167		287 560	< 10 352	3 104	.3 .7	< 20 3.5		236 1,110	235 610	1,600				-
	209	Qa1	44	6		17		44	98	164		620	168	133	1.2	15		950	510	1,490	7.5	37.5	3.0	
	501	Qa1	42	Dec. 1		15	5.6	85	67	85	2	486	153	68	.9	18	.5	730	489	1, 132	7,9	41.3	3.2	
	504	Qal	35	Jan. 24		18		112	87	127		448	344	98	.9	54		1,060	640	1,550	7.7	27.3	1.7	
	701	Qal	19	Feb. 12		13	•••	91	116	211	8	421	372	320	.6	< .4	.6	1,340	706	2,030	7.5	30.3	2.2	
	801	Qal	30	Mar. 21		13	·	95	39	28		426	31	53	.5	< .4		469	398	782	7.8 7.4	39.1	3.5 6	
	43-203	Qa1	30	Apr. 2	ľ	24		143	158	351	1	471	377	700	2.3	43	.7	2,030	1,010	3,050	7.4	13.2		
	601	Qa1		May 12		13		42	9	19	••	133	29	22	.3	19		218	140	366	7.6	43.0	15.3	
	49-103	Qal		Mar. 26		14		113	27	32	1	405	61	52	.5	< .4	.2	500	393	799	7.3	22.9	.3	
	105	Qal	Spring	d	1	14		96	26	34		343	65	54	.5	< .4		459	346	735	7.4	15,1	.7	
	201	Qal	52	de		16		129	33	44		405	84	98	.7	< .4		600	457	969	7.4	17.7	.8	
	50-102	Qa1		Mar. 27		16		154	38	206		365	348	226	.8	34		1,200	540	1,740	7.5	17.3 45.2	.9	
	105	Qal	1	Nov, 13		26	.62	165	47	138	5	325	100	348	1.0	42	-4	1,030	610	1,750	7.4	33.0	3.8	
	109	Qa1	25	dc	1	7		50	15	52		149	74	71	.5	3.0		346	185	639	6.9	38.1	2.4	•
	110	Qa1	25	đa	i	10		91	34	138		257	125	230	.7	< .4		760	366	1,310	7.1	45.1		
	111	Qal		do	1	27		124	38	170		337	178	216	1.0	67.5		990	469	1,550	7.4	45.8	3.2	•
	111	Qa1		Nov. 20.	1969	17		99	43	38		448	27	74	.6	2.0		520	425	893	7.4	16.3	3.4	•
	114	Qal	24	do		25		102	59	183		467	187	229	1,7	5.5		1,020	496	1,650	7.5	44.6	.8	
	120	Qal Qal)ec. 18,		17	.30	65	18	57	1	305	44	33	.5	20	.2	406	235	644	7.6	34,4	1.6	
	120	Qa1 Qa1		lan. 13,		20		75	34	117		406	103	75	1.3	41		670	327	1,030	7.7	43.8	2.8	•
	.21	Qa I		lune 23, Ian. 30,		21		82 147	47 108	121* 399		427 500	101 390	106 600		72		739	399					. 1
	122	Qa1	25 J	an. 28,	1970	22		132	44	168		317	157	1	1.3	35		1,950	810	2,870	7.5	51.7	6.1	
	123 124	Qal	50 M	ar. 27,	1970	16		161	40	205		316	360	296	.8	47		1,020	510	1,650	7.5	41.6	3.2	.0
	- 4 4	Qal	57											249	.8			1,250	560	1,790	7.4	44.1	3.8	.0

WELL	AQUIFER	DEPTH OF WELL (FT)	DATE OF COLLECTION	SILICA (Si0 ₂)	IRON (Fe)	CAL- CIUM (Ca)	MAGNE - SIUM (Mg)	SOD- IUM (Na)	POTAS- SIUM (K)	BICAR BONATE (HCO ₃)	SUL Fate (S04)	CHLO RIDE (C1)	FLUO RIDE (F)	NI - TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDUCTANCE (MICROMHOS AT 25°C)	рН	DER CENT SOD- TIM	SAR	RSC
XW-30-50-201	Qa 1	24	July 24, 1970	17		125	20	61	9	354	50	115	0.4	30	0.3	600	394	998	7.2	24.8	1.3	0.0
203	Qa1	22	Jan. 30, 1970	24		131	66	243		406	283	288	2.2	116.5		1,350	600	2,000	7.4	47.0	4.3	.0
2 0 5	Qal	22	do	18	2.30	138	78	326	12	428	407	375	2.3	100	.6	1,670	670	2,440	7.7	50.9	5.5	.0
207	Qal	23	do	22		111	38	130		329	131	147	1.2	121		860	435	1, 320	7.4	39.4	2.7	.0
208	Qal	24	do	16		97	39	225		379	226	237	1.3	17		1, 040	405	1,640	7.8	55.8	4.9	.0
210	Qal	22	do	25		121	51	196		378	227	229	1.2	80		1,120	510	1,680	7.3	45.4	2.9	.0
211	Qa1	23	Nov. 20, 1969	25		124	45	176	3	349	207	222	1.2	80	.5	1,060	492	1,640	7.4	43.5	3.4	.0
2 12	Qa1	23	do	25		120	50	174		357	215	207	1.8	90		1,060	510	1,640	7.4	42.9	3.4	.0
213	Qa1	33	Nov. 13, 1969	22		161	56	286		416	407	2 94	.8	75		1,510	630	2,190	7.4	49.5	4.9	.0
214	Qa 1	20	do	25		124	61	227		377	212	313	1.7	82.5		1,230	560	1,930	7.4	46.8	4.2	0.
217	Qal	24	Dec. 16, 1969	26		162	50	193		375	255	286	1.0	40		1,200	610	1,840	7.3	40.8	3.4	.0
5/ 218	Qati	34	June 23, 1939			100	40	85*		390	101	122	.9	< 20		641	415					
220	Qa1	20	Nov. 13, 1969	26	.04	151	52	179	2	325	239	285	1.1	65	.4	1,160	590	1,800	7.5	39.6	3.2	.0
225	Qa 1	21	Nov. 20, 1969	3		24	37	182		110	194	230	.7	< ,4		730	213	1,240	8.4	65.0	5.4	.0
226	Qa1	20	do	27		117	51	192		388	227	184	2.0	116		1,110	500	1,650	7.5	45.4	3.7	.0
227	Qa1	18	Dec. 18, 1969	17		177	111	550		415	620	781	2.2	70		2,530	900	3,675	7.5	57.2	8.0	.0
229	Qal	21	Jan. 28, 1970	24		116	38	122		309	116	195	1.2	54		820	445	1,330	7.6	37.4	2.3	.0
230	Qal	21	do	24		110	36	121		298	116	174	1.3	77		810	424	1.270	7.4	38.3	2.6	.0
301	Qal	20	Jan. 27, 1970	24		159	248	610		650	580	1,140	2.5	< .4		3,100	1,420	4,300	7.7	48.2	7.0	.0
/ <u>5</u> / 501	Qal	20	Aug. 3, 1960 Jan. 30, 1970	24 24		108 106	44 41	219* 232		330 423	300 270	210 195	1.1	58 37	.28	1,130 1,110	450 435	1,760 1,680	6.9 7.3	51 53.7	4.5	.0
502	Qal	20	do	25		154	55	258		395	32 1	329	1.0	44		1,380	610	2,070	7.3	47.9	4.6	.0
503	Qal	22	Jan. 30, 1970	22	. 22	111	41	211	ı	400	248	192	1.1	58	.6	1,080	447	1,640	7.6	50.6	4.4	.0
/ 5/ 505	Qal	28	Apr. 18, 1946 Oct. 22, 1969	25 27	.08	117 127	50 63	142 216	5.9 	388 387	142 246	180 275	1.0 1.5	114 112		1,030 1.260	498 580	1,900	7.0 7.3	44.9	3.9	.0
/ <u>5</u> / 507	Qal	25	Apr. 18, 1946 Jan. 28, 1970	28 25	.08	135 158	71 64	220 247	9.4	511 445	176 285	307 336	1.8	100 57		1,380 1,390	629 658	2,080	7.1 7.3	44.9	4.2	.0
508	Qa1	24	Dec. 18, 1969	26		106	48	242		444	216	250	2.1	54		1,160	463	1,770	7.4	53.2	5.0	.0
509	Qal	23	Nov. 17, 1969	24		130	45	211		393	258	218	1.0	77		1,160	510	1,750	7.6	47.5	4.1	.0
511	Qal	26	Dec. 2.1969	5		29	8	29		100	26	43	.3	< .4		191	106	357	7.0	37.2	1.2	.0
512	Qal	26	do	26		131	57	156		387	216	226	1.2	56		1,060	560	1,650	7.2	37.7	2.9	.0
514	Qa1	21	Jan. 27, 1970	25		143	47	235		405	302	199	1.2	160		1,310	550	1,700	7.4	48.0	4.4	.0
515	Qal	22	Jan. 26, 1970	26		140	62	200		412	230	273	1.3	67		1,200	610	1,800	7.6	41.7	3.5	.0
517	Qal	22	do	27		130	66	201		411	237	271	1.9	77		1,210	600	1,850	7.4	42.3	3.6	.0
518	Qal	28	do	26		148	53	227		436	274	280	1.2	51		1,270	590	1,900	7.4	45.6	3.7	.0

Table 7.--Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

| WELL | AQUIFER | DEPTH
OF
WELL
(FT) | DATE OF
COLLECTION | SILICA
(S102) | IRON
(Fe) | CAL-
CIUM
(Ca) | MAGNE -
SIUM
(Mg) | SOD-
IUM
(Na) | POTAS-
SIUM
(K) | BICAR-
BONATE
(HCO3)

 | SUL-
FATE
(SO4) | CHLO-
RIDE
(C1)
 | FLUO-
RIDE
(F) | NI-
TRATE
(NO ₃) | BORON
(B) | DIS-
SOLVED
SOLIDS
 | TOTAL
HARDNESS
AS CaCO3
 | SPECIFIC
CONDUCTANCE
(MICROMHOS
AT 25°C) | рн
 | PER-
CENT
SOD-
LUM | SAR | RSC |
|--------------|---|--|--|---|---|--|---|--|---
--
--
---|---|--|---|---
--
--
--	---
---	---
XW-30-50-519	Qa1

 | 270 | 2/0
 | | | 1 |
 |
 | | +
 | 1 | | |
| 520 | Qal | 24 | do | 27 | < 0.02 | 152 | 72 | 1 | |

 | |
 | | | | 1,300
 | 531
 | 1,910 | 7.5
 | 50.6 | 4.7 | 0.0 |
| 601 | Qa 1 | 24 | Aug. 3, 1960 | 23 | | 1 | | | 1 |

 | |
 | 1 | | 0.7 | 1,510
 | 680
 | 2,200 | 7.4
 | 46.5 | 4.5 | .0 |
| 602 | Qal | 24 | Dec. 3, 1969 | 25 | | 146 | 55 | 207 | | 407

 | 246 | 210
283
 | 1.0 | 117
62 | .23 | 1,060
1,230
 | 496
590
 | 1,660
1,870 | 7.1
7.3
 | | 3.4 | .0 |
| 603 | Oal | 1 | | | | | | | |

 | 226 | 455
 | 1.2 | 168 | | 1,560
 | 770
 | 2,390 | 7.3
 | 40.8 | 3.8 | .0 |
| | | | | 1 | | | | | | 411

 | 247 | 271
 | 1.0 | 54 | | 1,200
 | 570
 | 1,840 | 7.2
 | 43.7 | 3.7 | .0 |
| | | | | | | | | | | 405

 | 289 | 388
 | 1.4 | 210 | | 1,640
 | 886
 | 2,350 | 7.4
 | 34.1 | 3.1 | .0 |
| | ` | | | | | | 57 | 217 | | 357

 | 226 | 237
 | 2.0 | 112 | | 1,150
 | 485
 | 1,750 | 7,4
 | 49.4 | 4.3 | .0 |
| | | | | | | 149 | 70 | 266 | | 346

 | 316 | 372
 | 1.7 | 110 | | 1,480
 | 660
 | 2,230 | 7.4
 | | | .0 |
| | | | do | 20 | •• | 169 | 98 | 394 | | 403

 | 510 | 520
 | 1.9 | 110 | | 2,020
 | 830
 | 2,910 |
 | | | .0 |
| | | | do | 22 | | 142 | 72 | 263 | | 350

 | 311 | 370
 | 1.7 | 99 | | 1,450
 | 650
 | | 1
 | 1 | 1 | |
| | | 26 | do | 34 | | 100 | 58 | 190 | | 322

 | 248 | 239
 | 1.2 | 70 | | 1,100
 | 489
 | |
 | 1 | | .0 |
| | | 25 | Dec. 18, 1969 | 21 | | 165 | 62 | 226 | 3 | 397

 | 256 | 356
 | 1.0 | 62 | .5 | 1,350
 | 670
 | |
 | | | 0. |
| 615 | Qa 1 | 24 | Apr. 18, 1946
Aug. 5, 1958 | 22
 | 3.1 | 110
267 | 84
166 | 315
304 | 12 | 526
494

 | 403
417 | 280
831
 | 1.8 | 88 | | 1,660
 | 620
 | | 7.3
 | | | .0 |
| 616 | Qal | 24 | Dec. 3, 1969 | 26 | | 158 | 80 | 155 | | 290

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| 618 | Qa 1 | 25 | do | 28 | | 160 | 85 | 209 | | 320

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| 619 | Qa1 | 26 | do | 24 | | 195 | 82 | 337 | 3 | 355

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| 620 | Qa1 | 24 | do | 7 | | 39 | 10 | 26 | | 137

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| 621 | Qa 1 | 21 | do | 27 | . 10 | 198 | 70 | 217 | | 417

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| 624 | Qal | 28 | do | 20 | | 32 | 73 | 204 | |

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 | 37.7 | 3.4 | .0 |
| 625 | Qa 1 | 20 | Jan. 26, 1970 | 22 | | 121 | 81 | 161 | |

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 | 1,450 | 7.8
 | 53.7 | 4.5 | 2.02 |
| 626 | Qal | 21 | Jan. 27, 1970 | 21 | | 153 | 83 | 232 | | 403

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 | | 7.5
 | 35.5 | 2.8 | 0. |
| 627 | Qal | 18 | Dec. 1, 1969 | 27 | | 116 | 160 | 321 | | 1

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 | 2,150 | 7.4
 | 41.0 | 3.7 | .0 |
| 62.8 | Qa1 | | | 27 | | 168 | 66 | | |

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 | 950
 | 2,810 | 7.6
 | 42.5 | 4.5 | .0 |
| 631 | Qal | | | 25
18 | | 93 | 61 | 253 | < 1 | 128

 | 335 | 365
 | .9 | 85
90 | .5
.5 | 1,510
1,290
 | 690
485
 | 2,220
1,970 | 7.5
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 | 44.8
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5.0 | .0
.0 |
| 632 | Qal | 27 | | | | | | | |

 | | 1
 | .3 | 3.0 | | 174
 | 131
 | 302 | 7.2
 | 10.9 | 2.8 | .0 |
| 636 | 0a1 | | | | | | 1 | | 1 |

 | | 330
 | 1.2 | 90 | | 1,490
 | 570
 | 2,190 | 7.4
 | 53.3 | 5.4 | .0 |
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 | 284 | 266
 | .6 | 58 | | 1,250
 | 550
 | 1,870 | 7.3
 | 48.0 | 4.3 | .0 |
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 | 34 | 270
 | 1.0 | < .4 | | 1,090
 | 560
 | 1,935 | 7.5
 | 45.6 | 4.0 | 1.26 |
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 | 86 | 109
 | 2.0 | < .4 | | 540
 | 212
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 | 251 | 610
 | .9 | < .4 | | 1,430
 | 488
 | 2.350 | 8.1
 | 60.8 | 6.9 | .0 |
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 | 69 | 32
 | 3.7 | 11 | | 590
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 | 947 | 7.4
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 | 408 | 850
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Table 7. -- Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas-- Continued

	WELL	AQUIFER	DEPTH OF WELL (FT)	DATE OF COLLECTION	SILICA (S10 ₂)	IRON (Fe)	CAL- CIUM (Ca)	MACNE - SIUM (Mg)	SOD- IUM (Na)	POTAS- SIUM (K)	BICAR- BONATE (HCO ₃)	SUL- FATE (SO4)	CHLO- RIDE (C1)	FLUO- RIDE (F)	NI- TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDUCTANCE (MICROMHOS AT 25°C)	рн	PER- CENT SOD- IUM	SAR	RSC
	xw-30-50-650	Qel	25	June 18, 1970	24		77	76	362	< 1	466	368	341	2.3	54	0.9	1.530	500	2,230	7.6	61.0	7.0	0.0
	653	Qa 1	30	Dec. 14, 1970	22		166	64	258	< 1	344	353	376	1.1	80	.5	1,490	680	2,200	7.5	45.3	4.3	.0
	51-401	Qal	15	Feb. 9, 1970	18		162	34	249		255	263	439	.9	12		1,300	540	2,080	7.5	49.9	4.6	.0
	404	Qal	16	do	26	< 0.02	95	36	209	2	390	233	169	1.6	68	.5	1,030	386	1,550	7.6	53.8	4.6	.0
	408	Qal	25	June 18, 1970	24		159	68	258	2	425	316	346	1.2	80	.6	1,460	680	2,140	7.5	45.2	4.3	.0
	701	Qa 1	20	Oct. 22, 1969	25		173	166	320		460	467	650	1.9	27		2,060	1,120	3,050	7.5	38.4	4.2	.0
	706	Qa 1	18	Nov. 19, 1969	9	.62	32	63	250	3	484	121	252	2.5	13	.7	980	338	1,640	7.4	61.5	5.9	1.19
	707	Qa 1	30	Jan. 27, 1970	16		69	79	296		336	363	323	1.1	31		1,340	498	2,030	7.8	56.4	5.8	.0
3/ 5	708	Qa1	22	May 11, 1939 June 18, 1970	18		101 108	42 54	24* 63	2	427 428	81 142	32 86	1.0	< 20 3.5	.4	490 690	426 494	1,065	7.3	21.5	1.2	.0
3/5	57-101	Qa 1	20	July 27, 1939 Nov. 25, 1969	13		103	45	49		366 344	40 64	18 122	.7	< 20 22		385 590	442	 991	7.5	 19.3	1.0	.0
3/5	102	Qa 1	20	July 27, 1939 Nov. 21, 1969	16		78 109	33 57	83* 169		390 399	73 92	70 281	.6 1.4	21 50	 	550 970	330 510	1,610	 7.5	42.1	3.3	.0
										м	ultiple Aq	uifers											
	30-25-705	Qs, Pc	90	May 6, 1970	20	. 34	56	53	63	< 1	395	64	34	1.5	58	.4	540	357	854	7.6	27.7	1.4	.0
İ	706	Qs, Pc	80	do	20		61	37	39		321	44	20	1,0	75		455	306	690	7.7	21.8	1.0	.0
	710	Qs, Pc	70	do	19		118	127	205		540	439	231	1.8	30		1,440	82 0	2,050	7.5	25.3	3.1	.0
	33-101	Qal, Pc	35	Oct. 17, 1969	19		223	120	490		299	540	860	.8	97.5		2,500	1,050	3,650	7.6	51.0	6.6	.0
	201	Qal, Pc, Pvb	42	do	13		600	466	1,090		248	2,050	2,390	2.4	42.0		6,800	3,430	8,240	7.4	40.8	8.1	.0
33	601	Qal, Pv	35	Apr. 24, 1939 Apr. 14, 1970	16		220 294	156 96	197* 266		482 379	585 590	395 570	.8	72 4.5	 .8	1,862 2,040	1,191 1,130	2,880	 7.4	33.4	3.4	.0
	603	Qal, Pv	31	June 15, 1970	20		96	108	441	< 1	640	42.8	442	2.1	< .4	.8	1,850	680	2,700	7.8	58.4	7.4	.0
	605	Qal, Pv	42	do	14		246	193	540	6	285	1,080	880	.9	< .4	2.6	3,100	1,410	4,160	7.4	15.3	6.3	.0
5/	35-703	Qal, Par	74	Apr. 9, 1970	20		68	39	64		510	28	21	.5	8		500	333	799	7.6	29.4	1.5	1.68
5/	705	Qal, Par	64	do	17		72	99	374		870	187	373	1.7	< .4		1,550	590	2,410	7.9	58.0	6.7	2.58
											Callahan C	ounty											
	вх-30-44-402	Ka	56	Jan. 8, 1971	15		105	8	12	< 1	300	23	28	.3	8	.1	347	297	565	8.0	8.0	.3	.0
	703	Ка	66	do	9		111	6	12	< 1	303	19	38	.3	< .4	.1	344	300	581	7.5	8.3	.3	.0
	704	Ka	131	Feb. 5, 1971	15		139	11	11	< 1	365	58	32	.5	< .4	.1	446	392	714	7.4	5.7	. 2	.0
	705	Ka	51	do	14		90	11	29	< 1	306	24	35	.6	3.0	.1	357	272	598	7.5	18.7	.8	.0
	52-101	Ka	121	Dec. 3, 1970	11		95	21	15	< 1	337	23	33	.3	10	.1	374	323	629	7.6	9.4	.37	.0
	102	Ka	110	do	12	< ,02	91	21	18	< 1	344	20	32	.4	7	.2	370	313	615	8.0	11.3	.45	.0
	105	Ka	130	Feb. 8, 1971	13		149	11	10	< 1	405	31	32	.2	28	.2	473	420	760	7.2	4.9	.2	.0

Table 7.--Chemical Analyses of Water from Sclected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

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WELL	AQUIFER	DEPTH OF WELL (PT)	DATE OF COLLECTION	SILICA (S10 ₂)	IRON (Fe)	CAL- CIUM (Ca)	MAGNE - SIUM (Mg)	SOD- IUM (Na)	POTAS- SIUM (K)	BICAR- BONATE (HCO ₃)	SUL- FATE (504)	CHLO- RIDE (C1)	FLUO- RIDE (Г)	NI- TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLTOS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDUCTANCE (MICROWHOS AT 25°C)	рн	PER- CENT SOD- IUM	SAR	RS
BX-30-52-401 701	Ka	112	June 24, 1961		0.07	66	29	19	3.8	335	19	20	0.6	3		308	284	500		† –	+	+
/01	Ка	16	Sept. 6, 1940 Jan. 6, 1971	31		185 173	32 48	112* 176		445 455	233	150 324	2.4	< 20		949	595	589	7.2	13		
702	Ка	49	do	16		260	44	106	< 1	323	150	373	5.1	113	0.2	1,140	630	1,790	7.7	37.8	3.1	0.0
								·		Jones Co	<u>ا</u>					1,220	830	1,950	7.6	21.7	1.6	·'
PY-29-31-901	Psa	91	Dec. 1, 1967	21		479	161	520	76	590	1,400	700	<u> </u>		-ı ——	r						
903	Psa	20	do	19	1.40	254	113	337		300	610	780 560	2.2	165		3,910	1,860	4,790	7.4	37.6	5.23	-
32-701	Pc		Jan. 5.1968	19		198	2 3 2	391		394	990	640	2.4	143		2,190	1,100	3,180	7.7	40,0	4.43	
801	Pc	35	do	11		840	413	1,120		292	2,450	2,410	2.1	25		2,690	1,450	3,710	7.9	36.9	4.47	1
802	Pc	32	do	15		560	462	830		261	2,400	1,600	1.2	31.0 59		7,400	3,800	8,870	7.4	39,0	7.92	
901	Pc	60	Dec. 19, 1967	20		62	29	72		271	112	45	1.0	32		6,100	3, 300	7.310	7.6	35.3	6.27	
902	Pe	60	do	19		90	40	92		288	83	106	.7	135		510	274	795	7.6	36.4	1.90	-
904	Pc	37	do	12		180	71	140		245	560	164	1.1	- 155		710	392	1,060	7.6	33.7	2.01	
905	Pc			< .4		340	199	478		24	1,990	426	1.1	< .4		1,260 3,450	740	1,790	7.5	29.1	2.24	-
30-25-701	Pc		Dec. 19, 1967	20		199	156	570		438	1,220	383	2.0	189			1,670	4,100	6.5	38.5	5.08	-
801	Qs. Pvb		Jan. 4, 1968	27		115	72	228		285	236	327	1.7	154		2,930	1,140	3,730	7.4	52.0	7.32	
802	Qs. Pvb	125	do	19		88	70	115		455	223	85	1.5	23		850	580	2,050	7.6	45.9	4.1	
807	Qs, Pvb		ec. 10, 1968	20		145	73	195		235	67	560	.7	27.5		1,210	510	1,320	7.7	33.0	2.2	
901	Qa		ov. 30, 1967	16		133	170	820		600	1,320	660	2.5	30		3,450	660 1.030	2,100	7.5	38.9	3.3	
902 904	Qs	40	do	24		138	39	317		710	258	160	6.5	115		1,410	500	4,600	7.9	63.8	11.1	
904	Qs		an, 3.1968	24		144	172	394	-	510	560	351	5.3	500	Í	2,410	1,100	2,050	8.0	57.6	6.2	1,6
26-701	Qs	1	an. 4,1968	21		94	120	460		448	500	500	4.1	105		2,020	730	3,260	8.2	44.5	5.1	
702	Qs Pv		an. 3, 1968	15		32	26	337		560	156	208	1.2	10		1,060	188	1,710	8.3	57.9	7.4	
703	Qal	60 Ja 24	an, 4, 1968	24		166	135	560	-	550	740	580	.8	147		2.620	970	3, 700	8.1		10.7	5.4
705	Qal	24	do	18	• •	139	163	353		600	740	353	1.0	12		2.070	1,020	2,940	7.4	56.0	7.8	
706	Pv	72	do do <	3		22	47	179		310	131	166	.3	11		710	248	1,200	i	42.9	4.8	•-
27-701	Qs		1			18	110	730		210	660	810	.6	< .4		2,450	496	3,910		61.2	5.0	. 1
702	Qa1	35	c. 20, 1967 do	17		88	41	54		500	24	47	.7	10		530	390	891		23.4	14.2	
901	Qal		do pt. 20, 1967	20		165	131	261	•-	560	439	341	1.0	168		1,800	950	2,630		1	1.2	.4
902	Qal	26		18		469	161	610		168	570 1	.690	.9	105		3,710	1,830			42.0	3.7	
903	Qal		do pt. 19, 1967	21		364	119	540		200	510 1	, 300	.9	121		3,070	1,400				6.2	
904	Qal		pt. 20, 1967	19		412	130	491		176	328 1	,490	.8	90		3,050	1,570				6.3	
		90 jaej	20, 190/	11		62	17	84		142	86	130	.5	26		487	225				5.4	
															1							

Table 7.--Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

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Table 7.--Chemical Analyses of Water from Selected Water Wells and Springs in Taylor County and Adjacent Areas--Continued

WELL	AQUIFER	DEPIH OF WELL (FT)	DATE OF COLLECTION	SILICA (S10 ₂)	IRON (Fe)	CAL- CIUM (Ca)	MAGNE - SIUM (Mg)	SOD- IUM (Na)	POTAS- SIUM (K)	BICAR- BONATE (HCO3)	SUL - FATE (SO ₄)	CHLO- RIDE (C1)	FLUO- RIDE (F)	NI- TRATE (NO ₃)	BORON (B)	DIS- SOLVED SOLIDS	TOTAL HARDNESS AS CaCO3	SPECIFIC CONDICTANCE (MICROMHOS AT 25°C)	рН	PER- CENT SOD- IUM	SAR	RSC
PY-30-27-906 908 909	Qal Qal Qal	24	Sept. 20, 1967 do Sept. 26, 1967	16 20 21		131 87 85	34 43 27	150 171 249		311 422 365	129 178 247	266 173 198	0.6 1.6 1.1	29 3.0 63	 	910 880 1. 040	466 393 325	1,560 1,440 1,690	7.4 7.7 7.6	41.1 48.6 62.6	3.0 3.8 6.0	
* Sodium and pota 1/ Analysis by the 2/ Analysis by Tex 3/ Analyses by Bur 4/ Composite sampl 5/ Analysis given	U.S.Geol as Agricult eau of Indu e.	ogical Su ural Expe strial Ch	rvey. riment Station. emistry of the	Universit	y of Texa	s, and t	he U. S. G	eological	Survey.			<u> </u>										

Table 8.--Chemical Analyses of Oil-Field Brines, Taylor County

(Analyses are in parts per million except pH.)

After Rowland Laxson et al., 1960, Resistivities and chemical analyses of formation waters from the west central Texas area: West Central Texas Section of the Society of Petroleum Engineers of A.I.M.E.

PRODUCING ZONE	FIELD	AVERAGE DEPTH OF WELL (ft)	AREA SHOWN ON FIGURE 22	CAL- CIUM (Ca)	MAGNE- SIUM (Mg)	SODIUM (Na)	BICAR- BONATE (HCO ₃)	SUL- FATE (SO₄)	CHLO- RIDE (CI)	DIS- SOLVED SOLIDS	рH
				PERMIA	N SYSTEM						
Bothan Sand	Chrane	-	-	2,180	685	22,400	215	2,850	38,100	68,300	7.5
Bothan Sand	S. W. Tye	1,850	8	2,400	780	24,600	98	2,430	42,600	79,100	8.2
Noodle Creek Lime	Epley Noodle Creek	2,515	3	2,200	477	19,000	126	1,063	33,7 00	61,000	7.5
Noodle Creek	E. F. White	_	3	3,060	640	20,600	233	1,425	37,800	69,000	7.4
Tannehill	Blair	2,740	3	2,780	554	28,100	490	2,090	48,000	86,500	7.7
Saddle Creek	E, F <i>.</i> White	_	3	4,300	1,130	23,800	114	595	47,200	84,400	6.2
Flippen Lime	Cedar Gap	_	24	3,980	1, 04 0	28,300	160	0	53,600	88,100	6.5
Flippen Sand	Chrane	-	-	4,070	955	25,900	110	280	49,700	88,100	6.8
Flippen Sand	5 mi . W. View	_	_	3,440	636	23,600	258	930	43,500	76,000	7.9
Flippen	N. Tuscola	2,240	23	3,940	960	26,300	120	30	50,200	-	6.7
Flippen	N. Tuscola	2,150	23	4,336	961	30,211	49	6	57,100	-	6.1
Flippen	Wimberly	2,230		6,090	1,400	31,700	225	205	63,500	113,400	7.3
Flippen	Wimberly	2,230	_	5,446	1,361	28,950	239	260	58,400	-	6.4
Flippen	Regular	-	-	4,410	997	27,300	117	Tr.	53,000	85,800	7.2
Flippen	Regular	_	-	4,500	1,040	27,900	110	0	54,000	87,400	6.9
Flippen	Regular	_	—	4,868	1,156	30,100	120	Τr.	58,500	94,600	7.2

PRODUCING ZONE	FIELD	AVERAGE DEPTH OF WELL (ft)	AREA SHOWN ON FIGURE 22	CAL- CIUM (Ca)	MAGNE- SłUM (Mg)	SODIUM (Na)	BICAR- BONATE (HCO ₃)	SUL- FATE (SO₄)	CHLO- RIDE (CI)	DIS- SOLVED SOLIDS	рH
Flippen	Blair	2,480	3	5,310	1,045	24,000	301	375	49,000	_	6.4
Flippen	Blair	2,710	3	6,595	1,093	24,600	146	381	52,610	_	5,3
Cook Lime	Blair	2,875	3	5,500	990	26,700	160	910	53,000	92,800	7.6
Cook Sand	Ferrell	2,490		2,248	864	17,425	316	442	32,853	-	7.1
Cook Sand	12 mi. S. Merkel	_	_	3,600	1,020	28,110	325	1,330	51,7 00	94,500	7.2
Cook Sand	Potosi- Cook	1,935	26, 27	3,320	840	31,500	48	0	57,000	97,400	6.5
Cook Sand	Regular	-	-	4,700	1,120	28,500	200	0	55,500	90,000	6.8
Cook Sand	Regular	2,371	-	4,390	1,070	29,000	171	7	55,500	90,000	6.8
			PE	NNSYLVA	NIAN SYSTI	EM					
Gunsight	Wimberly	2,465	_	3,350	1,990	29,220	328	373	56,500	-	7.3
Gunsight	Wimberly	2,465	-	3,500	1,810	33,200	233	165	62,500	110,200	7.8
Serratt Sand	W. Lawn	-	30	8,300	1,770	50,000	14	0	97,000	176,200	5.4
McMillan	Lawn	2,700	30	11,480	2,624	49,335	20	81	103,660	167,220	
Palo Pinto	S. W. Tye	3,250- 3,600	8	3,520	1,120	27,600	735	1,380	54,800	92,800	6.6
Cross Cut	Herber	4,275	31	7,200	1,250	33,400	220	1,300	66,800	121,500	6.2
Palo Pinto	Reddin	2,920	7	4,830	1,108	31,790	412	1,748	59,300	-	6.6
Morris Sand	Buffalo Gap	4,342	20	10,500	2,400	43,600	220	390	91,500	164,500	6.0
Morris Sand	6 mi, W. View	_	_	14,700	1,810	38,600	112	690	90,500	159,400	6.7
Capps	Frederick- son	4,460	17	17,800	1,748	24,000	122	400	105,000	147,000	4.95
Upper Fry	Bradshaw	-	20	5,680	1,200	27,500	335	1,700	54,600	107,200	6.5
Upper Fry	Happy Valley	-	-	4,200	2,430	35,500	265	30	69,200	124,800	7.5

Table 8.-Chemical Analyses of Oil-Field Brines, Taylor County-Continued

PRODUCING ZONE	FIELD	AVERAGE DEPTH OF WELL (ft)	AREA SHOWN ON FIGURE 22	CAL- CIUM (Ca)	MAGNE- SIUM (Mg)	SODIUM (Na)	BICAR- BONATE (HCO ₃)	SUL- FATE (SO₄)	CHLO- RIDE (CI)	DIS- SOLVED SOLIDS	рН
Lower Fry	Happy Valley	-	_	6,520	1,330	37,200	190	0	72,700	131,000	6.8
Lower Fry	Jocelyn- Varn	4,680	33	6,520	1,015	33,600	130	595	65,700	120,000	6.5
Fry Sand	W. Moro	-	_	8,030	1,340	36,900	240	975	74,300	137,500	7.0
Goen Lime	Inkum	4,898	19	13,990	2,120	43,400	184	450	97,500	172,500	6.5
Jennings Sand	View E. Fry	_	17	14,650	2,130	43,100	123	740	98,000	177,600	6.7
Gardner Sand	Вох	-	11	19,500	2,830	52,200	150	108	123,000	226,900	6.6
Gardner Sand	W. Lawn	3,940	30	20,000	2,890	53,600	180	150	126,500	225,300	6.4
Gray Sand	Jocelyn- Varn	5,210	33	9,900	1,725	32,400	155	1,100	71,700	131,000	6.1
Gray Sand	Ovalo	4,190	30	12,650	1,960	39,100	110	240	88,300	158,100	6.1
Gray Sand	Ulander	4,610	30	15,000	1,930	43,000	110	400	98,200	170,900	6.0
Strawn	Atwood	4,100	30	11,145	1,067	31,934	177	389	71,677	-	6.5
Strawn	Buffalo Gap	4,250	20	9,410	2,181	39,923	167	407	84,163	_	6.9
				ORDOVICI	IAN SYSTEM	l					
Ellenburger	Blair	5,385	4	5,97 0	2,046	18,100	370	1,924	42,800	-	6.4
Ellenburger	Blair	5,490	4	4,290	788	25,700	220	560	49,600	91,200	6.9
				CAMBRIA	AN SYSTEM						
Cambrian	S. W. Lawn	5,375	30	1,816	491	24,341	529	570	41,445	-	6.9
Cambrian	Saxon- Guion	-	30	2,080	720	27,650	529	110	48,500	78,950	6.8
Hickory Sand	Saxon- Guion	5,475	30	1,484	463	21,706	651	783	36,485	-	6.9

Table 8.—Chemical Analyses of Oil-Field Brines, Taylor County—Continued

(Quantities reported in barrels)

AREA ¹ SHOWN OI		BRII PRODU(DISPO INTO F		INJEC WEL		MISCELL	ANEOUS
FIGURE 2	•	1961	1967	1961	1967	1961	1967	1961	1967
1	Cal-Ham (Palo Pinto) Cal-Ham (Strawn)	1,800 3,650	0 1,800	1800 3,650	0 1,800	0 0	0	0 0	0 0
	Area Total	5,450	1,800	5,450	1,800	o	0	0	0
2	Goodstein (Strawn)	365	o	365	0	o	0	0	0
	Area Total	365	0	365	0	0	0	0	0
3	Blair (Flippen) Blair (Shallow) Blair (Tannehill) Epley (Noodle Creek) Taylor County Regular White (Camp Colorado) White (Flippen) White (Tannehill) Area Totał	324 2,722 11,838 30 9,125 4,980 13,870 540 43,429	0 0 10,950 3,650 2,915 3,960 2,920 24,395	324 2,722 6,363 5,475 4,980 13,870 540 34,304	0 0 3,650 2,915 0 2,920 9,485	0 0 5,475 0 3,650 0 0 0 9,125	0 0 10,950 0 0 0 0 0 10,950	0 0 0 0 0 0 0 0	0 0 0 0 3,960 0 3,960
4	Blair, North (Ellenburger) Taylor County Regular Trent Area Total	427 2,200 1,000 3,627	0 0 0	427 2,200 1,000 3,627	0 0 0	0 0 0	0 0 0	0 0 0	0 0 0
5	Taylor County Regular	545	115	545	115	0	0	0	0
6	Area Total Bird Gibson Gibson (Frazier II) Patterson Patterson, South (Upper Dothan) Area Total	545 50,251 51,597 16,090 120,170 19,517 257,625	115 39,600 0 107,465 22,320 169,385	545 4,106 0 48,600 0 52,706	115 0 0 0 0 0 0	0 46,145 51,597 16,090 71,570 19,517 204,919	0 39,600 0 107,465 22,320 169,385	0 0 0 0 0 0 0	
7	Merkel Reddin Area Total	3,650 1,621,705 1,625,355	0 239,825 239,825	0 28,250 28,250	0 0 0	3,650 1,593,455 1,597,105	0 239,825 239,825	0 0 0	0 0 0
8	Dyess (Cook Sand) Dyess (Fry Sand)	23,454 2,620	12,825 3,295	10,800 2,620	1,825 1,095	0 0	11,000 1,850	12,654 0	0 350

See footnote at end of table.

Table 9.—Reported Oil-Field Brine Production and Disposal in 1961 and 1967, Taylor County—Continued

AREA ¹ SHOWN ON				DISPO		INJEC WE	TION	MISCELL	ANEOUS
FIGURE	_	1961	1967	1961	1967	1961	1967	1961	
					1307	1301	1967	1961	1967
	Dyess (Saddle Creek Sand) Dyess (Tannehill Sand) Taylor County Regular Thornton (Capps Lime) Thornton (Morris Sand)	2,146 4,754 26,480 8,030	11,000 11,000 29,905 4,015	1,800 0 19,400 8,030	0 0 4,380 4,015	0 0 3,650 0	11,000 11,000 25,525 0	346 4,754 3,430 0	0 0 0
	Tye, Southwest (Dothan Sand)	5,930 730	3,285 20,477	5,930 730	3,285 0	0	0	0	0
	Area Total	74,144	95,802	49,310	14,600	3,65 0	20,477 80,852	0 21,184	0 350
9	Taylor County Regular	3,390	10,950	3,390	0	0	10,950	0	•
	Area Total	3,390	10,950	3,390	0	0	10,950	0	0
10	Caldwell Ranch Taylor County Regular	30,789 73,000	67,437 50	0	0 0	30,789 73,000	67,437 0	0 0	0 50
	Area Total	103,789	67,487	0	0	103,789	67,437	o	50
11	Box (Palo Pinto)	105,224	82,125	0	0	105,224	82,125	0	0
	Area Total	105,224	82,125	ο	0	105,224	82,125	0	0
12	Taylor County Regular	40,120	29,563	1,020	183	39,100	29,380	0	ů o
	Area Total	40,120	29,563	1,020	183	39,100	29,380	õ	0
13	Clack (Flippen Lime) Taylor County Regular	182 39,139	95 232,199	182 16,564	95 0	0 22,215	0 232,199	0 360	0
	Area Total	39,321	232,294	16,746	95	22,215	232,199	360	0
14	Lake Kirby Taylor County Regular	437 330	735 0	437 330	0	0	735 0	0	0
	Area Total	767	735	767	0	0	735	0	0
15	Taylor County Regular	0	738	0	0	0	0	-	
	Area Total	0	738	0	0	0	0	0	738 738
16	La Gorce (Dothan Sand) Taylor County Regular Thornton (Morris Sand)	2,675 7,710 1,095	29,930 3,400 0	0 7,710 0	0 3,400 0	2,675 0 1,095	29,930 0 0	0 0	0 0
	Area Total	11,480	33,330	7,710	3,400	3,770	29,930	0	0 0
17	Frederickson (Capps) Frederickson (Goen) Inkum, East (Cook)	15,625 1,095 38,653	7,256 0 12,000	14,815 1,095 0	0 0 0	0 0 38,653	7,256 0 12,000	810 0 0	0 0 0

AREA ¹ SHOWN ON		BRI PRODU		DISPO INTO		INJEC WEI		MISCELL	ANEOUS
FIGURE	•	1961	1967	1961	1967	1961	1967	1961	1967
	Inkum, East (Flippen Lime)	5,798	3,650	0	0	5,793	3,650	0	0
	Inkum, East (Goen)	1,001	0	0	0	1,001	0	0	0
	Taylor County Regular	525	0	0	0	0	0	525	0
	View, East (Fry)	379	734	379	0	0	734	0	0
	View Gas Storage	170	0	170	0	0	0	0	0
	View, West (Jennings)	500	0	500	0	0	0	0	0
	Area Total	63,746	23,640	16,959	0	45,452	23,640	1,335	0
18	Taylor County Regular	5,800	0	5,800	0	0	0	0	0
	Area Total	5,800	0	5,800	0	0	0	0	0
19	Black (Flippen)	107	0	0	0	107	0	ο	0
	Black (Hardy Sand)	27	0	0	0	27	0	0	0
	Black (Home Creek)	370	730	0	0	370	730	0	0
	Black (Strawn)	849	0	0	0	849	0	0	0
	Black, South (Canyon)	0	7,300	0	0	0	7,300	0	0
	Davis-Taylor (Cook)	16,900	0	0	0	16,900	0	0	0
	Inkum (Cook Sand)	1,771	0	0	0	1,771	0	0	0
	Inkum, South (Goen)	0	67,525	0	0	0	67,525	0	0
	Inkum, Southeast (Cisco Reef)	10,702	25,915	0	0	10,702	25,915	0	0
	Inkum, Southeast (Upper Flippen)	243	989	243	0	0	989	0	0
	Inkum, Southeast (Lower Flippen)	11,940	400	662	0	11,278	400	0	0
	Inkum, Southeast (Speck Mountain)	5,081	0	0	0	5,081	0	0	0
	Taylor County Regular	46,330	116,425	730	0	45,600	116,425	0	0
	Area Total	94,320	219,284	1,635	0	92,685	219,284	0	0
20	Buffalo Gap (Morris)	1,095	0	1,095	0	0	0	ο	0
	Reid Elliott (Flippen Sand)	13,800	129,000	0	0	13,800	129,000	0	0
	S & D (Flippen Sand)	1,500	24,000	0	0	1,500	24,000	0	0
	Taylor County Regular	7,980	227,395	680	0	7,300	227,395	0	0
	Area Total	24,375	380,395	1,775	0	22,600	380,395	0	0
21	Taylor County Regular	50,196	11,813	15,488	0	34,708	11,813	0	0
	Area Total	5 0 ,196	11,813	15,488	0	34,708	11,813	0	0
22	Taylor County Regular	809	22,832	809	1,400	0	21,432	0	0
	Area Total	809	22,832	809	1,400	0	21,432	0	0
23	Cheatham (Flippen Sand)	739	o	739	0	0	0	0	0
	McGill (Flippen Sand)	3,124	0	0	0	3,124	0	0	0
	Taylor County Regular	60,772	95,455	72	0	60,700	95,455	0	0

Table 9.—Reported Oil-Field Brine Production and Disposal in 1961 and 1967, Taylor County—Continued

AREA ¹ SHOWN C		BR PRODU		DISPO INTO		INJEC WEI		MISCELL	ANEOUS
FIGURE 2	2 FIELD ¹	1961	1967	1961	1967	1961	1967	1961	1967
	Tuscola, North (Flippen Sand)	183,021	168,791	0	0	183,021	168,791	0	0
	Area Total	247,656	264,246	811	0	246,845	264,246	0	0
24	Cedar Gap (Flippen) Taylor County Regular	189,978	276,658	8,940	0	181,038	276,658	0	0
	Area Total	279,465 469,443	284,501 561,159	0 8,940	182 182	279,465 460,503	284,319 560,977	0	0
25	Elm Cove (Dothan)	500	0	500		·		0	0
	Taylor County Regular	118,641	37,911	71,114	0 0	0 47,527	0 37,911	0 0	0 0
	Area Total	119,141	37,911	71,614	0	47,527	37,911	0	0
26	Franklin (Moutray) Potosi (Cook Sand) Taylor County Regular	4,599 11,287 316,585	2,205 360 418,966	365 5,050 2,555	0 0 417	4,234 6,237 314,030	0 360 418,549	0 0 0	2,205 0 0
	Area Total	332,471	421,531	7,970	417	324,501	418,909	0	2,205
27	Potosi (Cook Sand) Potosi (Flippen Sand) Taylor County Regular Area Total	83,900 19,000 324,716	7,104 0 171,935	0 0 5,400	0 0 0	83,900 19,000 319,316	7,104 0 171,935	0 0 0	0 0 0
		427,616	179,039	5,400	0	422,216	179,039	0	0
28	Taylor County Regular Area Total	0	9,125	0	0	0	9,125	0	0
		0	9,125	0	0	0	9,125	0	0
29	Taylor County Regular Tuscola, East (McMillan)	625 2,800	34,128 0	625 0	0 0	0 2,800	34,128 0	0	0
	Area Total	3,425	34,128	625	0	2,800	34,128	0	0
30	Atwood Atwood, West (Gardner) Axelson (Gardner) Bacon (Cross Cut) Bacon (3140' McMillan) Bacon (3170' McMillan) Bradshaw (Gardner) Bull (Gardner) Bull (Gray) Extra Point (Gardner Lime) Extra Point (Gardner Sand) Lake Abilene (Flippen Sand) Landers (Gardner)	12 26,894 2,200 9,800 0 11,500 2,180 1,000 5,351 210 6,139 704	0 0 0 19,374 22,402 0 0 6,337 13,416 10,194	12 3,563 2,200 9,800 0 11,500 2,180 1,000 2,200 0 4,314	0 0 0 0 0 0 0 0 0 0 0 0	0 23,331 0 0 0 0 0 3,151 210 1,825	0 0 18,088 19,297 0 0 6,337 13,416 10,194		0 0 1,286 3,105 0 0 0 0 0 0 0
	Landers (Gardner)	704	10,194	4,314 704	0	1,825 0	10,194 0	0 0	

Table 9.—Reported Oil-Field Brine Production and Disposal in 1961 and 1967, Taylor County—Continued

AREA ¹		BRIN PRODU(DISPO: INTO F		INJEC1 WEL		MISCELL	ANEOUS
SHOWN OF	N1		1967	1961	1967	1961	1967	1961	1967
FIGURE 2	2 FIELD ¹	1961	1907	1901	1307	1001			
		5,206	0	5,206	0	0	0	0	0
	Lawn (Gardner)		ő	135	ō	0	0	0	0
	Lawn (Gardner Sand)	135	49,275	37	ŏ	Ō	49,275	0	0
	Lawn, Southwest	37		2,665	ŏ	ō	4,121	0	0
	Proctor (Gardner)	2,665	4,121	2,885	ŏ	õ	13,455	0	0
	Sabra (Cross Cut)	700	13,455		0	õ	45,125	Ó	0
	Saxon-Guion (Gardner)	0	45,125	0	0	5,110	-0,110	ō	Ō
	Saxon-Guion (McMillan Sand)	5,110	0	0	0	185,887	0	õ	Ō
	Saxon-Guion (Morris)	185,887	0	0	-		544,169	ő	6,730
	Taylor County Regular	12,362	550,899	12,362	0	0		ŏ	0,,00
	Ulander (Cross Cut)	0	1,460	0	0	0	1,460	ő	ő
	Ulander (Gray)	650	0	650	0	0	0	U	U
	Area Total	278,742	736,058	59,228	0	219,514	724,937	0	11,121
			-	4 000	0	4,680	0	0	0
31	Audra (Fry)	5,976	0	1,296	0	3,960	ŏ	ō	0
	Audra, South (Upper Fry)	3,960	0	0	-	3,980	ő	õ	ō
	Drasco (Middle Gardner)	0	1,050	0	1,050	8,232	ő	õ	1,095
	Herber (Cross Cut)	28,613	1,095	20,381	0		0	Ő	0
	Herber (Gray Sand)	14,600	0	14,600	0	0	0	0	ő
	Herber, South (Gray Sand)	4,500	0	4,500	0	0	0	0	ő
	Joni (Upper Fry)	8,021	0	821	Ó	7,200	0	0	ŏ
	Moro (Cross Cut)	4,990	0	4,990	0	0	-	•	o
	New Seven (Gray Sand)	2,900	3,285	0	0	2,900	3,285	0	0
	New Seven (Hope Lime)	12,500	5,872	0	0	12,500	5,872	0	
	Sanrob (Gardner)	1,120	0	1,120	0	0	0	0	0
	Sanrob (Upper Fry)	4,010	3,800	4,010	0	0	3,800	0	0
	Shaffer (Cross Cut Sand)	16,695	61,420	16,695	0	0	61,420	0	0
	Shaffer, West (Upper Fry)	0	7,300	0	0	0	7,300	0	0
		45,562	47,440	8,587	0	36,975	47,440	0	0
	Taylor County Regular	153,447	131,262	77,000	1,050	76,447	129,117	0	1,095
	Area Total	155,447	131,202	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					
32	Goble (Cross Cut)	7,200	0	0	0	7,200	0	0	0
J2	Lail (Canyon Reef)	2,100	77,000	0	0	2,100	77,000	0	-
	Taylor County Regular	21,080	95,000	0	0	21,080	95,000	0	0
	Area Total	30,380	172,000	0	0	30,380	172,000	0	0
33	Bartee (Fry Sand)	1,186	0	1,186	0	0	0	0	0
	Cornett (Upper Fry)	365	0	365	0	0	0	0	0
		0	10,950	0	0	0	10,950	0	0
	Gay Hill (4500' Fry)	183	0	183	0	0	0	0	0
	Grassburr (Gray Sand)	16,875	14,600	14,655	0	2,220	14,600	0	0
	Jocelyn-Varn (Fry)	10,875	14,000	10	Ō	. 0	0	0	0
	Jocelyn-Varn (Middle Fry)	21,521	10,950	3,600	ō	17,921	10,950	0	0
	Jocelyn-Varn (Upper Fry)		10,950	3,000	õ	0	0	4,369	0
	Jocelyn-Varn (Gray)	4,369	0	5	Ŭ	5			

Table 9.—Reported Oil-Field Brine Production and Disposal in 1961 and 1967, Taylor County–Continued

		BRINE PRODUCTION		DISP(INTO			CTION	MISCELI	LANEOUS
AREA ¹ SHOWN ON							CTION		_ANEOUS
FIGURE 22	FIELD	1961	1967	1961	1967	1961	1967	1961	1967
	J. V. (Fry) Kissel (Upper Fry) Shep (Caddo) Shep (Gray Sand) Shep (Upper Fry Sand) Shep, Southwest (Fry Sand) Taylor County Regular Area Tota! Robertson-Griffin (Gray Sand) Area Total	0 26,303 365 35,086 7,422 12,000 0 125,685 3,300	42,340 1,825 5,800 18,360 0 8,300 113,125 1,805	0 23,960 365 12,045 4,745 12,000 0 73,114 3,300	0 0 0 0 0 0 0 0	0 0 16,979 2,677 0 0 39,797	42,340 1,825 0 5,800 18,360 0 8,300 113,125 365	0 2,343 0 6,062 0 0 12,774 0	0 0 0 0 0 0 0 1,440
		3,300	1,805	3,300	0	0	365	0	1,440
	County Total	4,745,183	4,307,897	554,658	32,727	4,154,872	4,254,211	35,653	20,959
Percent of Total	Percent of Total	100.0	100.0	11.7	0.8	87.6	98.7	0.7	0.5

 1 Oil and gas fields as assigned by the Railroad Commission of Texas.

Table 10.-Oil and Gas Tests Selected as Data-Control Points in Taylor County and Adjacent Areas

WELL	OPERATOR	LEASE NAME AND OPERATOR'S WELL NUMBER	COUNTY	SECTION, BLOCK, AND SURVEY
UA-29-39-702	Sojourner et al.	Pace, No. 2	Nolan	Sec. 68, Blk. 20, T & P RR Survey
UA-29-46-805	Fisher and Webb	Campbell, No. 1	Nolan	Sec. 185, Blk. 1-A, H & T RR Survey
XW-29 -48 -301	W. M. and A. P. Fuller	Grady Parmelly, No. 1	Taγlor	Tract 7, Blk. 4, Burr & Caswell Survey
XW-29-48-810	Edgar Davis	Edgar Davis, No. 1	Taylor	NW/4 Sec. 296, Blk. 64, H & TC RR Survey
XW-29-55-301	Star Oil Co.	W. L. Ray, No. 1	Taylor	Sec. 242, Blk. 64, H & TC RR Survey
XW-29-56-111	Condor	Stokes, No. 1	Taylor	NW/4 Sec. 257, Blk. 64, H & TC RR Survey
XW-29-56-112	R, P. Fisher	Elm Cattle Co., No. 1	Taylor	SE/4 Sec. 275, Blk. 64, H & TC RR Survey
XW-29-56-505	Bert Fields	Sears, No. 1	Taylor	SW/4 Sec. 223, BLK. 64, H & TC RR Survey
PY-30-26-801	Sid Katz Exploration and Rockhill Oil Corporation	L. E. McKee, No. 1	Jones	Sec. 22, Blk. 16, T & P RR Survey
XW-30-34-804	Great Lakes Carbon Corporation	Jones, No. 3	Taylor	Wm. Bishop Survey No. 43
XW-30-42-210	Taubert Drilling Co.	M. J. Farr, No. 1	Taylor	W. E. Vaughn Survey No. 54
XW-30-42-802	L. M. Lockhart	J. L. Camp, No. 1	Taylor	Sec. 44, Blk. 1, SP RR Survey
XW-30-43-901	West Central Drilling	W. O. Black, No. 1	Taylor	South part Sec. 3, Blk. 7, SP RR Survey
XW-30-43-902	West Central Drilling	Chrane, No. 3-A	Taylor	NE/4 Sec. 9, Blk. 7, SP RR Survey
XW-30-43-903	Humble Oil	Mrs. J. V. Kemper, No. 2	Taylor	NW/4 Sec. 14, Blk. 7, SP RR Survey
XW-30-49-404	Continental Oil Co.	Frances Sears Shelton, No. 1 G-43	Taylor	Sec. 228, Blk. 64, H & TC RR Survey
XW-30-49-903	Humble Oil	Alton Roberts, No. 1	Taylor	Theo. D. Maltby Survey No. 270
XW-30-50-401	S. C. Herring Drig. Co.	F. A. Boyd, No. 1	Taylor	Sec. 35, Blk. 1, SP RR Survey
XW-30-51-210	J. N. Burnham	Amyz, No. 1	Taylor	SE/4 Sec. 26, Blk. 6, SP RR Survey
XW-30-51-304	West Central Drlg.	TXL, No. 1	Taylor	NE/4 Sec. 23, Blk. 6, SP RR Survey
XW-30-51-603	Robinson-Puckett, Inc.	Addie Bishop Pfleuger, No. 1	Taylor	Sec. 18, Bik. 6, SP RR Survey
BX-30-52-601	Anderson-Pritchard	Tom Windham, No. 1	Callahan	George Hancock Survey No. 369
WP-30-57-501	Robinson-Puckett and W. P. Luse	Frank Johnson, No. 1	Runnels	Jose Espinosa Survey No. 500
XW-30-58-301	Woodley Petroleum Co.	M. G. Reed, No. 1	Taylor	M. P. King Survey No. 434